Hydrogeology and the Distribution of Salinity in the Floridan Aquifer System, Southwestern Florida

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By Ronald S. Reese

Abstract

A study was conducted to establish a detailed hydrogeologic framework in the complex Floridan aquifer system of southwestern Florida. and to evaluate and relate the distribution of salinity found in this system. The Floridan aquifer system consists of the Upper Floridan aquifer, middle confining unit, and Lower Floridan aquifer. The Upper Floridan aquifer extends into a basal unit of the Hawthorn Group; however, a regional unconformity present at the base of this unit generally marks the top of the Floridan aquifer system, as it does in the rest of southern Florida. The basal Hawthorn unit, which is defined at its top by a correlative marker unit, ranges in thickness from 120 to 460 feet. Paleotopography present prior to deposition of the basal Hawthorn unit, which resulted at least in part from erosion, is believed to have caused some of this variation in thickness. However, in some areas where the basal Hawthorn unit is thick, particularly in Lee County, depositional buildup created paleotopographic highs at the top of the unit. In these areas, permeable limestone zones are present in the unit, giving the unit a high transmissivity.

In most of the study area, the Floridan aquifer system can be divided into a brackish-water zone, a salinity transition zone, and a saline-water zone. The brackish-water zone contains water with a dissolved-solids concentration of less than 10,000 milligrams per liter. The saline-water zone has a dissolved-solids concentration of at least 35,000 milligrams per liter and a salinity similar to that of seawater. The salinity transition zone that

separates these two zones is usually 150 feet or less in thickness. The altitude of the base of the brackish-water zone was mapped primarily using geophysical logs; it ranges from as shallow as 565 feet below sea level along the coast to almost 2,200 feet below sea level inland. This mapping indicated that the boundary represents a salinity interface, the depth of which is controlled by head in the brackish-water zone.

Chloride concentrations in the upper part of the brackish-water zone range from 400 to 4,000 milligrams per liter. A large area of relatively low salinity in north-central Collier County and to the northwest, as defined by a 1,200-milligram-per-liter chloride-concentration line, coincides with a high area on the basal contact of the Hawthorn Group. As this contact dips away from this high area to central Hendry and southwestern Collier Counties, chloride concentration increases to 2,000 milligrams per liter or greater. However, the increase in salinity in these areas occurs only in the basal Hawthorn unit or Suwannee Limestone, but not in deeper units. In central Hendry County, the increase occurs only in the basal Hawthorn unit in an area where the unit is well developed and thick. These areas of higher salinity could have resulted from the influx of seawater from southwestern Collier County into zones of higher permeability in the Upper Floridan aquifer during high sea-level stands. The influx may only have occurred in structurally low areas and may have experienced incomplete flushing subsequently by the modern freshwater flow system.

In an area in north-central Collier County, the altitude of the base of the brackish-water zone is anomalously deep given the position of this area relative to the coast. In this area, the base extends as deep as 2,090 feet below sea level, and the salinity transition zone is not present or is poorly defined. The origin of this anomalous area is interpreted to be related to the development of a unit containing thick dolomite and evaporite beds high in the middle confining unit of the Floridan aquifer system. The top of this dolomite-evaporite unit, which probably has very low permeability, occurs at the base of the brackish-water zone in this area. The axis of a high area mapped at the top of the unit trends to the northwest from central Collier County into north-central Lee County. This axis parallels and lies just to the west of the anomalous area, and it could have acted as an impermeable sill, preventing saline water from moving in laterally from the coast to the southwest and up from the Lower Floridan aguifer. Locating a Floridan aquifer system well field in or near this anomalous area could be optimal because of the lack of a salinity interface at depth.

INTRODUCTION

Increasing demand for water from the surficial aquifer system in the highly populated coastal area of southern Florida has prompted a need to find supplemental sources of available water for both public and agricultural use. In 1995, nearly 456 Mgal/d (million gallons per day) were withdrawn from ground-water sources in Collier, Hendry, and Lee Counties (Marella, 1999). Of this amount, 60 percent was obtained from the surficial aquifer system, 38 percent from the intermediate aquifer system, and 2 percent from the Floridan aquifer system (Marella, 1999). Ground-water withdrawals in these three counties increased 107 percent between 1975 and 1995.

The virtually untapped, but well-developed Floridan aquifer system can be used to assist in the need to find supplemental water sources in southern Florida. Because of the generally brackish nature of this ground-water source, its use has been primarily for withdrawal for irrigation.

Two other methods for using the aquifer system are currently being explored: (1) the reverse-osmosis desalination method, and (2) the aquifer storage and retrieval (ASR) method. With the reverse-osmosis

method, high pressure is applied to the water being treated, forcing it through a semipermeable membrane. This process removes the dissolved salts, thus producing pure water (freshwater). Because the salinity of water in the upper part of the Floridan aquifer system is only about 10 percent of that of seawater, the expense of the reverse-osmosis treatment is much less than desalting seawater.

With the ASR method, freshwater from the surface or the surficial aquifer system is temporarily stored in the upper part of the Floridan aquifer system and withdrawn when the water is needed. Before use of the Floridan aquifer system can be implemented on a large scale, its hydrogeologic framework and distribution of salinity in southern Florida need to be characterized and better understood.

To address these information needs, the U.S. Geological Survey (USGS), in cooperation with the South Florida Water Management District (SFWMD), conducted a study from October 1992 through September 1995 to: (1) describe the vertical and areal variations in water quality in the Floridan aquifer system, and (2) relate these variations in water quality to the local hydrogeologic framework of southern Florida. Emphasis in this study was placed on the upper part of the Floridan aquifer system in Collier, Hendry, and Lee Counties, and small parts of Charlotte and Glades Counties to the north; Palm Beach, Broward, and Dade Counties to the east; and Monroe County to the south (fig. 1). The study area is bounded by Lake Okeechobee on the northeast and the Gulf of Mexico on the west. Two similar studies were conducted, one in southeastern Florida encompassing mainly Dade and Broward Counties (Reese, 1994) and the other in Palm Beach County (Reese and Memberg, 1999).

Purpose and Scope

This report delineates the distribution of salinity in relation to the local hydrogeology of southwestern Florida, and assesses the potential processes that might control (or have affected) the distribution of salinity in the Floridan aquifer system. Hydrogeologic sections and maps were prepared showing the altitude of the top of a basal Hawthorn unit in the Hawthorn Group, the altitude of the basal contact of the Hawthorn Group, and the thickness of the basal Hawthorn unit. The basal contact of the Hawthorn Group approximately coincides with the top of the Floridan aquifer

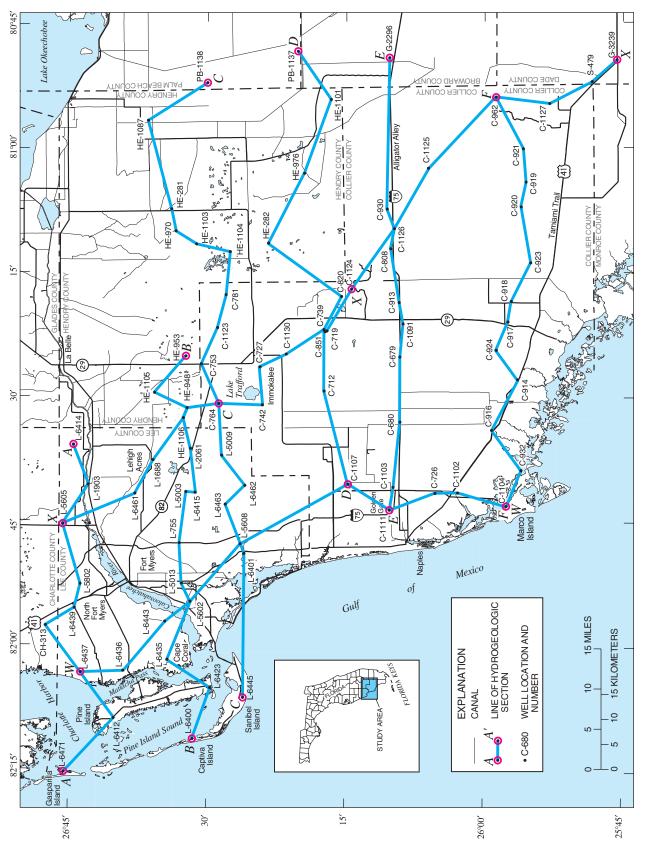


Figure 1. Study area and trace of hydrogeologic section lines.

system. The altitude of a thick dolomite evaporite unit in the middle confining unit of the Floridan aquifer system was also mapped. Lithologic descriptions and borehole geophysical logs were used to correlate geologic units between wells. The principal aquifer systems and their hydrogeologic units in southwestern Florida (the watertable aquifer, lower Tamiami aquifer, sandstone aquifer, mid-Hawthorn aquifer, Upper Floridan aquifer, middle confining unit, and the Lower Floridan aquifer) are described, including their thicknesses, relations to geologic units, and hydraulic properties.

Because the water-quality data available in the study area were not comprehensive enough for a complete water-quality analysis, the analysis in this report deals primarily with salinity (principally chloride and dissolved-solids concentrations). The water-quality data presented in this report consist of 137 analyses, 59 of which were collected and analyzed by the USGS. No water samples were collected specifically for this study.

Borehole geophysical logs, including porosity and resistivity logs, were used to evaluate groundwater (formation water) salinity. The depths of occurrence of threshold salinity values of interest in the Floridan aquifer system were approximated based on resistivity geophysical logs, and the average salinity of particular depth intervals was calculated for a number of wells. These geophysical logs were not run as part of this study, but were available for use. As part of this geophysical log evaluation, relations were developed between chloride and dissolved-solids concentrations, and between chloride concentration and specific conductance based on water-quality data from the Floridan aquifer system. Additionally, relations were developed between sonic log interval transit time and density log porosity, and between formation temperature and well depth.

The Floridan aquifer system has been divided into three salinity zones; in order of increasing depth, they are the brackish-water zone, a salinity transition zone, and the saline-water zone. The boundaries between these zones principally were determined based on borehole geophysical logs. However, they also were determined based on water-quality data, which were collected while drilling or from completed intervals. Maps were prepared that show the altitude of the base of the brackish-water zone and the distribution of chloride and sulfate concentrations in this zone in the study area. One plot was constructed that shows the distribution of chloride concentration in ground

water relative to depth above and below the basal contact of the Hawthorn Group. A plot of chloride and sulfate concentrations in ground water was constructed for comparison with a pure water-seawater mixing line. The influence of gypsum dissolution and seawater mixing was evaluated by plotting the sulfate-to-chloride ratio against sulfate concentration in ground water from the Floridan aquifer system. The description and character of the brackish-water zone are emphasized in this report because of its potential use as a supplemental water-supply source. These maps and plots of the brackish-water zone were useful in determining processes that could control the thickness of the brackish-water zone and the distribution of salinity within it.

Classification and Characterization of Salinity

A classification scheme for water based on dissolved-solids concentrations was used to define salinity in the Floridan aquifer system in southwestern Florida. In this scheme, brackish water contains dissolved-solids concentrations that range from 1,000 to 10,000 mg/L (milligrams per liter), moderately saline water contains concentrations that range from 10,000 to 35,000 mg/L, and saline water contains concentrations from 35,000 to 100,000 mg/L. This scheme is similar to, but differs from, the one defined by Fetter (1988, p. 368) in which the moderately saline water portion does not exist, and saline water has dissolvedsolids concentrations that range from 10,000 to 100,000 mg/L. Seawater has dissolved-solids concentrations of about 36,000 mg/L (Nordstrom and others, 1979). A well-defined relation between dissolvedsolids and chloride concentrations in water produced from the Floridan aquifer system has been established for southeastern Florida (Reese, 1994), allowing for the interchanging of these constituents in the characterization of salinity. Chloride concentration was used in mapping the distribution of salinity in this report.

Water in the Upper Floridan aquifer in southern Florida is brackish with chloride and dissolved-solids concentrations generally greater than 1,000 mg/L (Sprinkle, 1989, pls. 6, 8). The Lower Floridan aquifer contains water with a salinity similar to that of seawater (Meyer, 1989, fig. 3). Parts of the Floridan aquifer system where water has dissolved-solids concentrations less than 10,000 mg/L are protected from contamination by injected wastewater through the Underground Injection Control Program of the Safe Drinking Water Act (Fetter, 1988, p. 459). Underground injection in Florida

is regulated by the Florida Department of Environmental Protection (FDEP), formerly known as the Florida Department of Regulation (1982).

Inventory of Well Data

Data for all wells used in this study are presented in appendix I and include: local well number. other well identifier or owner, site identification number, latitude and longitude, land-net location, altitude of measuring point, well depth, bottom and diameter of casing, and date at end of well construction. The well locations are shown in figures 2 and 3. Data from all wells presented in this report are stored in the USGS Ground Water Site Inventory (GWSI) computer system. Some information on these wells beyond that given in appendix I, such as the drilling contractor's name and the top and bottom of the completed (open) intervals in a well, is stored in the GWSI. A completed interval in a well is defined in this report as an interval open to flow regardless of the type of openings in the interval. Completed intervals are generally isolated from each other and from other parts of the borehole through the use of casing and cement during construction of the well. Most completed intervals in the wells used in this report are open-hole completions. Additional data, including site use, geophysical logs run, and a representative water-quality analysis, are presented in a publication by Smith and others (1982).

Depth in a well, as used in this report, refers to feet below the measuring point. In most instances, the altitude of the measuring point is the same as the elevation of the land surface; however, in some instances, it is higher than the land surface, such as the top of a drilling floor, which can be a number of feet above the land surface. If measurement of a point in a well is referenced to sea level datum in this report, the phrase "altitude, in feet above sea level" or just "feet below sea level" is used.

Many of the wells used in this report were drilled for the purpose of oil exploration or production (67 wells), and several wells were drilled and completed at five wastewater injection system sites (table 1). The oil test wells, generally at least 11,000 ft (feet) deep, are located mostly in an area that extends from north-central Collier County, northwest into western Hendry County (fig. 3). Lithologic sample descriptions were produced and open-hole geophysical logs were run in many of the oil test wells. Although the lithologic descriptions are available, the quality of drill cutting samples from most of the oil test wells often is not good because of the large sampling depth

interval and the use of the mud rotary method for drilling. The geophysical logs that were run in the oil test wells sometimes included both resistivity and porosity logs of good quality. Most of the water-quality data collected from the oil test wells in the study area was accomplished after setting an intermediate casing string and deepening the hole a short distance below the casing.

Nine wells (table 1) were drilled at the following wastewater injection system well sites:

- South States Utilities Marco Island Wastewater Treatment Plant (injection well C-1104 and monitor well C-1105),
- North County Regional Water Treatment Plant (injection well C-1107 and monitor well C-1108),
- Zemel Road Landfill (injection well CH-313 and monitor well CH-314),
- North Fort Myers Utility Wastewater Treatment Plant (injection well L-5802 and monitor well L-5803), and
- Gasparilla Island Wastewater Treatment Plant (injection well L-6471).

At four wastewater injection well sites, monitor wells were drilled adjacent to an injection well. The monitor wells at these sites are located less than 200 ft apart from their companion injection well. Thus, data collected from these wells drilled in close proximity at a site are considered as data collected from one well in this report.

Lithologic sample descriptions were produced and open-hole geophysical logs were run in the wastewater injection wells, as was the case for the oil test wells. The quality of drill cutting samples from these wells generally is good because of the small sampling depth interval (5 or 10 ft) and the use of the reverse-air rotary drilling method. A full suite of geophysical logs is usually run in these wells, including borehole television surveys of open-hole sections before emplacement of the casing. Whole-diameter cores of selected intervals in the Floridan aquifer system were taken and analyzed in a laboratory.

Seven wells used in the study area were continuously cored their entire depth, including: wells L-6400, L-6401, and L-6403 in Lee County; wells C-1090 and C-1091 in Collier County; and wells HE-1084 and HE-1085 in Hendry County (Green and others, 1990). In addition to a detailed lithologic description available for these wells, some geophysical logs were also run. In addition to the seven cored wells, well C-851 was almost continuously cored and had a total depth of 2,056 ft.

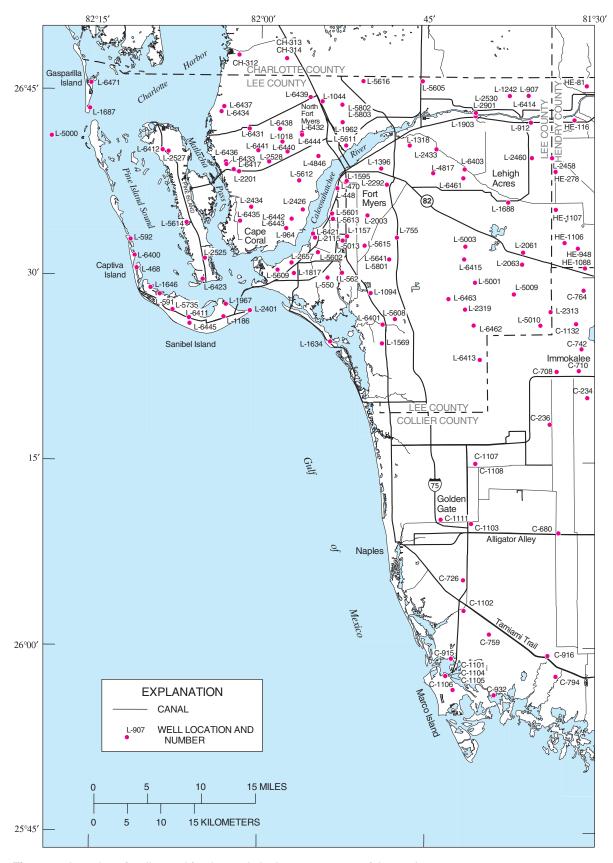


Figure 2. Location of wells used for the study in the western part of the study area.

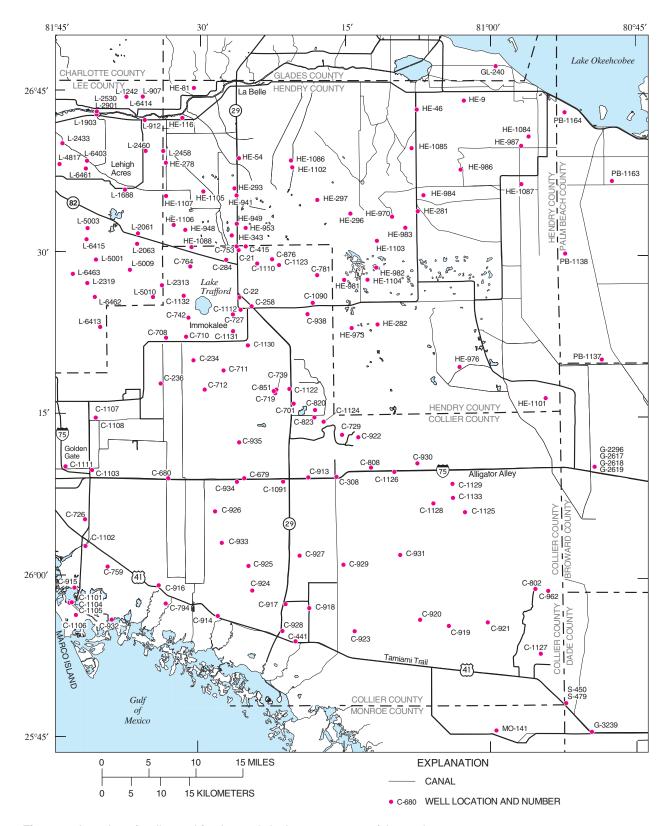


Figure 3. Location of wells used for the study in the eastern part of the study area.

Table 1. List of oil test wells and wastewater injection system wells used in the study

[WWI, wastewater injection well. Asterisk indicates monitor well at the same site as the preceding injection well]

| Well number | Type of well | Well number | Type of well |
|-------------|--------------|-------------|--------------|
| C-324 | Oil test | C-1133 | Oil test |
| C-415 | do. | CH-313 | WWI |
| C-701 | do. | CH-314* | WWI |
| C-708 | do. | L-5000 | Oil test |
| C-710 | do. | L-5001 | do. |
| C-711 | do. | L-5003 | do. |
| C-712 | do. | L-5009 | do. |
| C-719 | do. | L-5010 | do. |
| C-726 | do. | L-5013 | do. |
| C-727 | do. | L-5802 | WWI |
| C-729 | do. | L-5803* | WWI |
| C-739 | do. | L-6415 | Oil test |
| C-742 | do. | L-6461 | do. |
| C-753 | do. | L-6462 | do. |
| C-759 | do. | L-6463 | do. |
| C-764 | do. | L-6471 | WWI |
| C-781 | do. | G-3239 | Oil test |
| C-794 | do. | S-479 | do. |
| C-802 | do. | GL-240 | do. |
| C-808 | do. | HE-282 | do. |
| C-820 | do. | HE-343 | do. |
| C-823 | do. | HE-941 | do. |
| C-962 | do. | HE-948 | do. |
| C-1104 | WWI | HE-949 | do. |
| C-1105* | WWI | HE-953 | do. |
| C-1107 | WWI | HE-970 | do. |
| C-1108* | WWI | HE-973 | do. |
| C-1122 | Oil test | HE-976 | do. |
| C-1123 | do. | HE-1101 | do. |
| C-1124 | do. | HE-1102 | do. |
| C-1125 | do. | HE-1103 | do. |
| C-1126 | do. | HE-1104 | do. |
| C-1127 | do. | HE-1105 | do. |
| C-1128 | do. | HE-1106 | do. |
| C-1129 | do. | HE-1107 | do. |
| C-1130 | do. | MO-141 | do. |
| C-1131 | do. | PB-1137 | do. |
| C-1132 | do. | PB-1138 | do. |

Inventory and Collection of Water-Quality Data

Selected water-quality data from well sampling intervals in the intermediate and Floridan aguifer systems are presented in appendix II. Included in the appendix are 137 water analyses taken from 104 wells, with the analyses listed chronologically by local well identifier. Of the 137 samples, 103 were obtained from completed intervals, 25 were obtained from open-hole intervals by a packer test, and 9 were obtained by the reverse-air rotary method while drilling. Of the 103 samples that were from completed intervals, 15 were obtained as a result of a well-abandonment program conducted by the SFWMD. These water-quality data (along with other data including flow measurements and casing and open-hole condition) were collected from the SFWMD wells just before abandonment and are stored in an SFWMD data storage and retrieval computer system (DATAFLEX).

Of the 137 samples listed in appendix II, 59 were collected and analyzed by the USGS; however, no USGS water samples were collected specifically for this study. Sampling procedures and analytical methods used to determine the value of the constituents given in the appendix for the USGS samples are described by Brown and others (1970). The constituents in appendix II include chloride, sulfate, dissolved solids, and specific conductance. Most of the USGS data are stored in a USGS water-quality data storage and retrieval computer system (QWDATA). The other water samples in appendix II were collected and analyzed by the SFWMD (29 analyses) and private consultants (49 analyses).

Control of water sampling and testing methods for wastewater injection system wells (table 1) is overseen by the FDEP. According to FDEP rules (Florida Department of Environmental Regulation, 1982), the background water quality of the injection and monitoring zone(s) shall be established prior to injection. FDEP permits issued to construct and operate injection well systems include specific testing requirements, one of which is pumping at least three well volumes of fluid from a monitor well before sampling.

Open-hole packer test samples are often more contaminated than water samples from completed intervals due to the small volume of water produced before sampling occurs and the possibility of leakage of drilling fluid around packers. Barite-weighted bentonite drilling mud wafers, instead of saltwater slugs, are used occasionally to control artesian pressure in

the Floridan aquifer system. The use of mud wafers reduces the potential for deep invasion of the formation by drilling fluid.

Wells are commonly drilled in the Floridan aquifer system in southern Florida with the reverse-air rotary method in which air is injected into the drill pipe at a variable depth. This air provides the lift needed to bring fluid and drill cuttings up the drill pipe to the surface (return flow). Water samples of this return flow are collected at regular intervals while drilling. A common problem with this method is that a change in salinity with depth might not be detected. This results if the permeability of the rock being drilled is low so that little of the return flow originates from the rock (formation) at or near the drill bit as expected. Rather, the flow continues to come from a permeable zone higher in the hole between the borehole wall and the drill pipe. For this reason, the top of the sampling interval in each of the nine samples collected by this method (app. II) is at the top of the openhole section being drilled (base of the casing).

Previous Studies

The Regional Aquifer System Analysis (RASA) Program of the USGS provided background information for this report. Final interpretive results of the RASA Program, which began in 1978, are presented in a series of USGS Professional Papers that describe the geology, hydrology, and geochemistry of each regional aquifer system. A series of studies on the Floridan aquifer system that were conducted as part of the RASA program (USGS Professional Paper 1403 series reports) were used for this report.

Meyer (1989) analyzed the hydrogeology, ground-water movement, and subsurface storage of liquid waste and freshwater in the Floridan aquifer system in southern Florida. Miller (1986), who studied the hydrogeologic framework of the Floridan aquifer system in the RASA study area (Florida and parts of Georgia, Alabama, and South Carolina), subdivided the aquifer system into chronostratigraphic units and constructed hydrogeologic sections, isopach maps, and structure maps. Additional studies of the same area were conducted by Bush and Johnston (1988) and Sprinkle (1989). Bush and Johnston (1988) described ground-water hydraulics, regional flow, and changes in the flow system as a result of ground-water development of the Floridan aquifer system. Sprinkle (1989) examined the geochemistry of the Floridan

aquifer system and mapped the concentrations of selected constituents in water from the Upper Floridan aquifer. More recent work done by the USGS on the geochemistry of ground water in the Floridan aquifer system focuses on sources of sulfate in ground water found in the Upper Floridan aquifer in southwestern Florida (Sacks and Tihansky, 1996).

Chen (1965) studied the lithology and stratigraphy of Paleocene and Eocene strata in Florida and made paleogeographic interpretations. The Floridan aquifer system in southern Florida was mostly deposited during Eocene time (Miller, 1986). Puri and Winston (1974) mapped and described high transmissivity zones in southern Florida. Scott (1988) studied the Hawthorn Group, describing its lithologies, stratigraphy, and relation to subjacent and suprajacent units. Recent work on the Tertiary stratigraphy for the Florida Keys and the southern peninsula of Florida has been done by Cunningham and others (1998). This work has resulted in the definition of two new formations of upper Miocene to Pliocene age, and also includes analyses of previously defined formations as old as the Oligocene.

Detailed hydrogeologic mapping and descriptions of the intermediate aquifer system and the Upper Floridan aquifer were done in Lee County by Wedderburn and others (1982), whose work provided important groundwork for this study. Other useful SFWMD reports that deal with the geology, hydrogeology, or ground-water resources in the study area include those by Peacock (1983) covering southern Collier County, Knapp and others (1986) covering western Collier County, and Smith and Adams (1988) covering Hendry County.

Studies of saline ground-water resources and saline-water intrusion in Lee County were conducted by Boggess (1974) and Sproul and others (1972). Hydrogeologic sections of the surficial aquifer system and the upper part of the intermediate aquifer system in Lee County and adjacent areas were constructed by Boggess and others (1981). Missimer and Associates (1991a, b) conducted a hydrogeologic study in southwestern Collier County, which included the drilling of two deep test wells, and a detailed hydrogeologic study in the Cape Coral area of northwestern Lee County, which included water-quality mapping of the intermediate and Floridan aquifer systems.

Acknowledgments

Appreciation is extended to several organizations and individuals who contributed data and helpful suggestions during the course of this study. Invaluable input and data were provided by Robert Caughey of the Florida Geological Survey in Fort Myers, who has many years of experience working with oil test wells and the geology in the study area. George Winston, consulting geologist, provided lithologic descriptions of a number of wells that were used in the hydrogeologic sections as well as useful ideas concerning construction of the hydrogeologic sections. Charles "Buzz" Walker of Missimer International, Inc., was very helpful in providing data collected by Missimer and Associates or related consulting firms. Richard Orth of the FDEP in Fort Myers provided data on deep injection system wells collected by consulting firms. Michael Bennett of the SFWMD was instrumental in providing data collected from wells drilled by SFWMD during the course of this study and in having SFWMD digitize many of the geophysical logs used on the hydrogeologic sections.

A USGS colleague, Richard Kane, contributed much to this study, including some of the analysis of water-quality data and many of the calculations of salinity from geophysical logs. Other USGS colleagues and part-time students who helped with this study are Linda Powell, Michael Byrne, Isaac Segal, Robert Mooney, and Steven Memberg. The large effort involved in the construction of the hydrogeologic sections, including the digitizing of geophysical logs and construction and coding of the lithocolumns, would not have been possible without the help of these individuals. The final drafting of the hydrogeologic sections and the contour maps was all computer generated and produced by USGS scientific illustrator Kimberly Swidarski of the USGS Miami Subdistrict office.

HYDROGEOLOGY OF SOUTHWESTERN FLORIDA

Southern Florida is underlain by rocks of Cenozoic age to a depth of about 5,000 ft (Meyer, 1989, p. G5). These rocks are principally carbonates (limestone and dolostone), with minor amounts of evaporites (gypsum and anhydrite) in the lower part and clastics (sand and clay) in the upper part. The movement of ground water from inland areas to the ocean and the reverse occurs primarily through the carbonate rocks (Meyer, 1989, p. G5). This section of the report

presents a detailed discussion of the geologic framework of the study area, including the lithology, stratigraphy, and structure. Also discussed are the principal aquifer systems and hydrogeologic units of southwestern Florida.

The Floridan aguifer system in southwestern Florida includes (from oldest to youngest) the upper part of the Cedar Keys Formation of Paleocene age, Oldsmar Formation of early Eocene age, Avon Park Formation of middle Eocene age, Ocala Limestone of late Eocene age, and the Suwannee Limestone of early Oligocene age (fig. 4). Overlying the Suwannee Limestone is the Hawthorn Group as defined by Scott (1988), and the lower part of this group is included in the Floridan aquifer system in this report. The Hawthorn Group, which is divided into the Peace River Formation in the upper part and the Arcadia Formation in the lower part, was thought to be all Miocene in age (Miller, 1986; Scott, 1988); however, age-dating of core taken from a well in southwestern Florida has shown that the lowermost part of the Arcadia Formation is as old as early Oligocene in age (Wingard and others, 1994).

To illustrate geologic and hydrologic boundaries and spatial relations in the study area, 10 hydrogeologic sections were constructed (pls. 1-10, in pocket). The locations of the east-west sections (pls. 1-7) and the northwest-southwest sections (pl. 8-10) are shown in figure 1. The depth of these hydrogeologic sections extends from 200 to 2,400 ft below sea level; however, some of the wells on the sections were not drilled as deep as 2,400 ft below sea level. Data presented for each well on the sections include geophysical logs (gamma ray or spontaneous potential and resistivity curves), lithology, and water-quality data. Geologic and salinity zone boundaries, as determined in this study, are also shown on the hydrogeologic sections.

Lithology and Stratigraphy

The Floridan aquifer system in southwestern Florida is composed predominantly of limestone with dolomitic limestone and dolomite being common in the lower part of the aquifer system (fig. 4). Delineation of the geologic units in the study area began with selected wells where the boundaries of the units were determined based on geophysical well logs and/or lithologic sample descriptions. The gamma-ray log was the most useful well log for determining geologic boundaries and making correlations between wells.

| Series | | Geologic Unit | Approximate thickness (feet) | Lithology | Ну | Hydrogeologic unit | Approximate thickness (feet) |
|--------------------|----------|------------------------|------------------------------|---|------------------|----------------------------------|------------------------------|
| HOLOCENE | | UNDIFFERENTIATED | 02-0 | Quartz sand, silt, clay, and shell | | WATER-TABLE AOUIFER | 20 -100 |
| TO | | TAMIAMI | i i | Silt, sandy clay, micritic limestone, sandy, shelly | EK 2A | CONFINING BEDS | 09-0 |
| PLIOCENE | <u> </u> | FORMATION | 6-170 | limestone, calcereous sandstone, and quartz sand | | LOWER TAMIAMI AQUIFER | 25-160 |
| | d | PEACE | | Interhedded sand silt | EEK | CONFINING UNIT | 20-100 |
| MIOCENE | BOU | RIVER | 50-400 | gravel, clay, carbonate, and phosphatic sand | E AQUII | SANDSTONE AQUIFER | 0 -100 |
| ANDIATE | O N | FORMA HON | | | TAIC ITSY | CONFINING UNIT | 10-250 |
| OLIGOCENE | HOB | ARCADIA | | Sandy limestone, shell beds, | | MID-HAWTHORN AQUIFER | 0-130 |
| | LM | FORMATION | 400-550 | and carbonate, sand, silt, | ILNI | CONFINING UNIT | 100-400 |
| | ∀Н | | | and clay | | LOWER HAWTHORN PRODUCING ZONE | 0-300 |
| EARLY OLIGOCENE | | SUWANNEE LIMESTONE | 009-0 | Fossiliferous, calcarenitic limestone | SASTEM | UPPER FLORIDAN | 700-1,200 |
| ATE | | OCALA | 0400 | Chalky to fossiliferous, | | AQUIFER | |
| 1 | | IVIES I OINE | | calcalenno mnesione | EEK | | |
| MIDDLE | | AVON PARK FORMATION | 900-1,200 | Fine-grained, micritic to fossiliferous limestone, | IUQA | MIDDLE CONFINING UNIT | 500-800 |
| STX | | OLDSMAR | 800-1 400 | dolomitic limestone, dense | N | LOWER | 1,400-1,800 |
| .₩∃ | | FORMATION | | dolomic, and gypsum | <u>−</u> WID∀ | FLORIDAN BOULDER AOUIFER ZONE | 400 |
| PAIFOCENE | | CEDAR KEYS | 200-200 | Dolomite and dolomitic limestone | FLC | | |
| | | FORMATION | 1,200? | Massive anhydrite beds | | SUB-FLORIDAN CONFINING UNIT | 1,200? |

Figure 4. Generalized geology and hydrogeology of southwestern Florida.

Lithologic sample descriptions used in determining the geologic boundaries came from a variety of sources including the Florida Geological Survey, the SFWMD, private consultants, and individuals. Most of the descriptions done by the Florida Geological Survey were obtained from a computer data base known as GeoSys/4G (GeoSys, Inc.), in which lithologic data are coded. Depths to the tops of geologic units, as determined in this study, are given in appendix III.

Avon Park Formation

The deepest unit in the Floridan aquifer system dealt with in this report is the Avon Park Formation of middle Eocene age. Determination of the top of the underlying Oldsmar Formation can be arbitrary and difficult, and thus was not done for this study. According to Winston (1993), the Oldsmar Formation in southern Florida is not identifiable. The lower part of the Avon Park Formation, as discussed and shown in this report, could be placed in the Oldsmar Formation as defined by other investigators, such as Meyer (1989).

The top of the Avon Park Formation is often marked by a zone of thinly bedded, light-brown, finely crystalline to fossiliferous dolomite or dolomitic limestone that is about 50 ft in thickness. The predominant lithology in the Avon Park Formation is fine-grained, micritic to fossiliferous limestone. Dolomitic limestone, dense dolomite, and gypsum can also be present and abundant. Dolomite, dolomitic limestone, and recrystallized limestone become more common in the Avon Park Formation in Lee County and western Collier County, with dolomite often occurring in the lower part of the formation as thick interbeds (30 ft or greater in thickness). Foraminifera characteristic of the Avon Park Formation are Dictyconus cookei and Dictyconus americanus. The thickness of the Avon Park Formation (rocks of middle Eocene age) ranges from 900 to 1,200 ft in southwestern Florida (Miller, 1986, pl. 7).

The east-west hydrogeologic sections (C'-C", D-D', E-E', and F-F'), which extend to the eastern boundary of the study area (pls. 4-7), show that the Avon Park Formation generally thickens to the east as its top rises in this direction. Correlation between wells based on geophysical logs in this study has shown that this eastward thickening of the Avon Park Formation in the eastern part of the study area is due, at least in part, to a facies change between the formation and the overlying formation. This interpre-

tation is in agreement with Winston (1993; 1995), who found evidence for facies changes and interfingering between the Avon Park Formation, Ocala Limestone, and Suwannee Limestone.

Ocala Limestone

The lithology of the Ocala Limestone varies from micritic or chalky limestone, to a mediumgrained calcarenitic limestone, to a coquinoid limestone. The Ocala Limestone is characterized by abundant larger benthic foraminifera, such as Operculinoides sp., Camerina sp., and Lepidocyclina sp. (Peacock, 1983). The presence of these foraminifera aids in distinguishing this geologic unit from the overlying Suwannee Limestone and the underlying Avon Park Formation. Gamma-ray log activity is characteristically low, but the upper and lower boundaries of the Ocala Limestone usually are marked by an increase in gamma-ray activity. The thickness of the Ocala Limestone ranges from 0 to more than 400 ft in the study area (fig. 4). It thins toward the east (pls. 4-7) and disappears toward the southeast (pl. 10). The Ocala Limestone is absent southeast of the study area in most of Dade County (Miller, 1986, pl. 9).

Suwannee Limestone

The dominant lithology of the Suwannee Limestone in the study area is pale-orange to tan, fossiliferous, medium-grained calcarenite with minor amounts of quartz sand. Phosphatic mineral grains are rare. Limestone in the lower part of the unit is similar to that in the upper part, but typically contains more finegrained, phosphatic, clastic material and interbeds of micrite and clay. Because of these interbeds, gammaray activity in the Suwannee Limestone often increases downward below the upper part, which has low activity similar to that found in the Ocala Limestone.

The top of the Suwannee Limestone is often well defined on gamma-ray logs because of the much higher levels of natural radioactivity associated with the lower Hawthorn Group as compared to the Suwannee Limestone. However, in some wells this contact appears gradational, with sandy limestone or calcareous sandstone of relatively low gamma-ray response above the contact. The thickness of the Suwannee Limestone ranges from 0 to more than 600 ft (generally becoming thicker from east to west) and is commonly 300 to 400 ft in Lee and western Collier Counties. Thickness can vary rapidly, particularly in

Lee County, because of the relief on top of the Suwannee Limestone. Some of this relief might be erosional in nature. The Suwannee Limestone thins (pls. 7 and 10) and sometimes disappears (pls. 4-6) toward the east. Farther to the east in Dade County, the base of the Hawthorn Group as mapped by Scott (1988, figs. 41 and 42) is at an altitude similar to the top of the rocks of Ecoene age (Reese, 1994, fig. 6), suggesting that the Suwannee Limestone is not present.

Hawthorn Group

The Hawthorn Group is a heterogeneous unit that generally consists of interbedded siliclastics (quartz sand, silts, and clays) and carbonate rocks. The distinguishing characteristics of the Hawthorn Group are its high and variable siliclastic and phosphatic content; its color, which can be green, olive-gray, or lightgray; and its gamma-ray log response. Intervals high in phosphate sand or gravel, typically 30 to 100 ft in thickness, are present in places and have high gamma-ray activity with peaks of 100 to 200 API units (American Petroleum Institute standard units) or more. Phosphate mineral grain content as high as 15 percent is not uncommon.

The Hawthorn Group is subdivided into the Peace River and Arcadia Formations (Scott, 1988). The upper part of the Hawthorn Group, the Peace River Formation, primarily consists of siliclastic material with occasional carbonate and phosphate-rich beds and ranges from 50 to 400 ft in thickness (Scott, 1988, figs. 42 and 43). The lower part of the Hawthorn Group, the Arcadia Formation, predominantly consists of carbonate rocks and ranges from 400 to 550 ft in thickness in the study area (fig. 4). The top of the Arcadia Formation was determined to be 410 ft below sea level in well C-1107 (pl. 5).

The lower part of the Arcadia Formation is referred to as the basal Hawthorn unit in this report, and this unit ranges from about 120 to 460 ft in thickness in the study area. The basal Hawthorn unit is emphasized throughout this report because of its hydrologic significance. The top of the basal Hawthorn unit is defined by a sequence of sediments referred to as the marker unit. The top of the marker unit, also the top of the basal Hawthorn unit, is often marked by two high gamma-ray activity peaks as shown in well C-914 in southwestern Collier County (fig. 5). The top of the marker unit also was determined by examination and comparison of resistivity logs when no gamma-ray logs were run. The thickness

of the marker unit generally decreases from about 100 ft in the southeastern part of the study area to about 50 ft in the northwestern part (pls. 9 and 10).

The lithology of the marker unit at the top of the basal Hawthorn unit generally consists of limestone and calcilutite with low phosphorite and quartz sand content. The marker unit corresponds relatively well with unit H-2 defined in the Hawthorn Group in southern Collier County where the benthic foraminifera *Miogypsina sp.* was found (Peacock, 1983, p. 17). The lithology of the marker unit is overlain and underlain by phosphatic dolomite in much of southern Collier County (pls. 6 and 7). To the west along the coast in Collier and Lee Counties, the bounding beds are often dolomitic to calcareous, phosphatic clay. Specifically, this clay is present in wells C-916 (pl. 7), C-1103 (pl. 6), C-1107 (pl. 5), and L-6445 on Sanibel Island (pl. 3).

The upper and lower boundaries of the marker unit at the top of the basal Hawthorn unit are defined by thin beds with high gamma-ray activity, and these beds could be synchronous in their deposition over large areas. The gamma-ray curve of the marker unit and its bounding beds has a characteristic pattern (fig. 5), which remains consistent over large areas as shown by the hydrogeologic sections (pls. 1-10). The thin bounding beds with high gamma-ray activity are high in phosphatic material and are composed of finegrained sediment. They could have been deposited during high stands of sea level when the Florida platform became flooded, and sedimentation was mostly limited to the settling out of fine material from suspension.

The lithology of the basal Hawthorn unit below the marker unit is variable. The phosphate content ranges from low to high (greater than 5 or 10 percent). In Lee County, the basal Hawthorn unit is thick and consists of white to light-gray, quartz sandy, micritic limestone containing minor amounts of phosphate grains and some beds of abundant fragments of mollusk and gastropods shells and other fossils. These shelly beds can have high moldic porosity. The gamma-ray response of this lithology in Lee County is usually intermediate between that found higher in the Hawthorn Group and that in the upper part of the Suwannee Limestone. Dolomite or dolomitic limestone is commonly present, particularly in the lower part of the basal Hawthorn unit and in southern Collier County. This dolomitic lithology can also contain quartz sand and often is characterized by thin beds

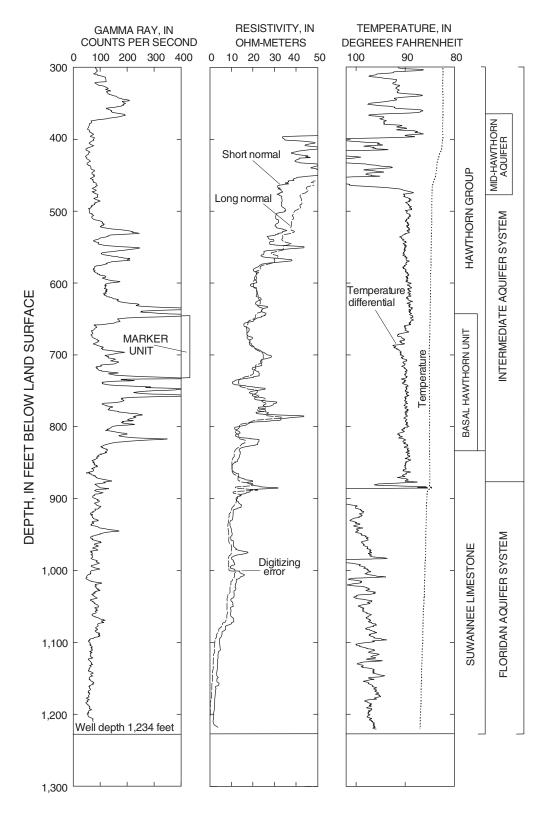


Figure 5. Geophysical logs, geologic units, and hydrogeologic units for well C-914 in southwestern Collier County. Temperature log shows major flow zone at 880 feet, which is below the top of Suwannee Limestone.

with high resistivity (resistivity peaks). Quartz sandrich limestone and dolomite and thick sand or sandstone beds are present in central Hendry County, where the basal Hawthorn unit is thick (pl. 4, wells HE-1103 and HE-1104).

Unconformity

Regional unconformities in peninsular Florida are present at the top of the rocks of late or middle Ecoene age (Ocala Limestone or Avon Park Formation if no Ocala Limestone is present) and rocks of Oligocene age (Suwannee Limestone) according to Miller (1986, pl. 2). Zones of dissolution occur in association with these unconformities in southern Florida (Meyer, 1989, p. 49). In southeastern Florida, the most important unconformity in terms of erosion and dissolution is at the top of the rocks of Eocene age (Reese, 1994); whereas in southwestern Florida, the most important unconformity is the one at the top of the Suwannee Limestone as found in this study and by Wedderburn and others (1982). The unconformity at the top of the Suwannee Limestone and the post-Ecoene unconformity would coincide in southeastern Florida, if as previously suggested, the Suwannee Limestone is absent in this area.

Additional evidence that the Suwannee Limestone is absent or much thinner in southeastern Florida than in southwestern Florida comes from correlation of gamma-ray logs. A correlation line at the top of a phosphatic zone shown on three geologic sections in southeastern Florida (Reese, 1994, figs. 3-5) correlates with the base of the marker unit at the top of the basal Hawthorn unit in this study. The thickness of the interval between the top of the phosphatic zone and the top of the rocks of Eocene age in southeastern Florida is similar to the thickness of the basal Hawthorn unit below the marker unit in the eastern part of this study area.

Continuous core taken from a well at Long Key in the Florida Keys, about 70 mi south-southeast of the study area, shows that a subaerial erosion surface is present at the contact between the Hawthorn Group and the Suwannee Limestone, and that this contact represents a depositional sequence boundary (Cunningham and Rupert, 1996). The unconformity could have formed during a major low stand in sea level that occurred between the early and late Oligocene (Haq and others, 1988).

Structure

Three maps were constructed that show the altitude of the top of the basal Hawthorn unit, the altitude

of the basal contact of the Hawthorn Group, and the thickness of the basal Hawthorn unit in the study area. The base of the Hawthorn Group (base of the basal Hawthorn unit) represents the top of the Suwannee Limestone in most of the study area, but it represents the top of the subjacent Ocala Limestone in some of the eastern part of the study area.

Because of the continuity of the marker unit at the top of the basal Hawthorn unit and the probability that its top surface is isochronous, a map was constructed showing the altitude of the top of the basal Hawthorn unit (fig. 6). Overall, the surface dips from northwest to southeast, ranging from about 400 or 500 ft below sea level in northern Lee County to more than 800 ft below sea level in extreme southeastern Collier County. A major northwest-southeast trending trough or structural sag extends from eastern Lee County into north-central Collier County (fig. 6). This trough has relief of at least 200 ft in eastern Lee County over a distance of only 2 mi (miles), with less pronounced relief in Collier County. An inferred fault has been mapped which parallels this trough and roughly coincides with the high area along its southwest side (Winston, 1996, fig. 19). The trough could be related to this fault. The trace of the fault (fig. 6) is a projection of the "North Port" fault, which was established to the northwest of the study area. In the study area, its presence is indicated by missing Eocene-aged section in one well (C-729) and a thick Eocene-aged section in which the borehole wall collapsed due to fracturing in another well (Winston, 1996, p. 27). The well with wall collapse is an injection well (CH-313) in south-central Charlotte County (fig. 1).

Structure in central to southeastern Lee County is the most complex in the study area (fig. 6). Two closely spaced troughs trending east-northeast are located southeast of the Caloosahatchee River, with pronounced relief of 200 ft or more for both troughs over a distance of 2 or 3 mi. The altitude of the top of the basal Hawthorn unit at the bottom of the two troughs is similar, being about 600 ft below sea level. These troughs could be fault related. The vertical displacement (200 ft) of the basal Hawthorn unit between wells L-6443 and L-5602 (pl. 8) suggests a fault. This fault lies along the northwestern boundary of the northernmost trough, adjacent to and paralleling the Caloosahatchee River. The north block is upthrown. Evidence was found for faults displacing the Hawthorn Group and older sediments in an area southwest of Fort Myers in Lee County along the southeastern bank of the Caloosahatchee River (Sproul and others, 1972, fig. 4). Vertical displacement along these faults is about 50 to 100 ft, and their trend is west-northwest.

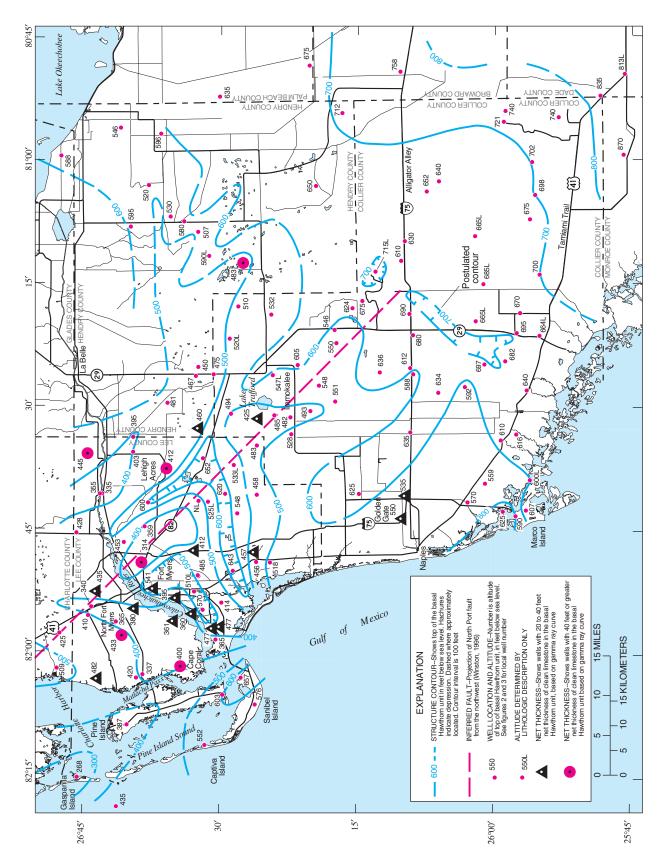


Figure 6. Altitude of the top of the basal Hawthorn unit in the study area.

Indications of faulting exist elsewhere in the study area. In southwestern Collier and central Hendry Counties, contours suggest structural features trending northwest-southeast, parallel to the projection of the North Port fault (fig. 6). Additionally, a narrow low area extends across central Collier County trending northeast-southwest, with the top of the basal Hawthorn unit possibly as low as 700 ft below sea level.

The altitude of the basal contact of the Hawthorn Group ranges from 500 or 600 ft below sea level in northern Lee County to greater than 1,000 ft below sea level in the extreme southeastern part of the study area (fig. 7). A broad, high area as shallow as 600 ft below sea level is present in central and northern Collier County and extends to the northwest through eastern Lee County. Separating this high from another high area in eastern Hendry County is a northwest-southeast trending trough, extending through western Hendry County in which the altitude of the surface is as deep as 1,000 ft below sea level.

Some of the relief shown by the map of basal contact of the Hawthorn Group (fig. 7) probably results from erosion and solution prior to deposition of the Hawthorn Group. To better understand this relief, a map was constructed showing the thickness of the basal Hawthorn unit (fig. 8). Because of the characteristics and continuity of the marker unit at the top of the basal Hawthorn unit, as previously discussed, the thickness of the basal Hawthorn unit could, in part, indicate paleotopography just before or during deposition of this unit. Therefore, areas of the basal Hawthorn unit where the interval is thick would represent paleotopographic lows and areas where the interval is thin would represent paleotopographic highs. A salient feature of this map (fig. 8) is a thin area, which could have been a paleo-ridge, where the interval is 200 ft thick or less extending northwest through central Collier County and eastern Lee County. Areas where the basal Hawthorn unit is thick (300-400 ft or greater), which could have been paleotopographic lows, are located in central and western Hendry County, northeastern Lee County, and the Cape Coral peninsula area of Lee County. The hydrogeologic sections constructed for this study clearly show that a large part of the relief on the basal contact of the Hawthorn Group (fig. 7) is compensated by the thickening and thinning of the basal Hawthorn unit; for example, between wells L-6412 and L-6437 in northwestern Lee County and between wells L-1903 and L-6414 in northeastern Lee County (pl. 1).

The thickening of the basal Hawthorn unit in some areas could be caused by depositional buildup during deposition of the basal Hawthorn unit. One of these features is evident in the Cape Coral peninsula area, centered on well L-6435 (pl. 2), and a thick limestone unit is present from about 500 to 620 ft below sea level in the well. This limestone unit could be related to the buildup if deposition of the limestone unit was biohermal in nature. A similar buildup within the basal Hawthorn unit is evident at wells L-5608 and (pl. 8) and L-1688 (pl. 9).

The net thickness of "clean" (low in clay and phosphate) limestone in the basal Hawthorn unit was determined in wells in which a gamma-ray log was run. This was accomplished by adding all intervals in which the gamma-ray activity was low; that is, at a level similar to the activity in the limestone below the basal contact of the Hawthorn Group. These intervals are present in the middle to upper parts of the basal Hawthorn unit. Wells with 20 to 40 ft and 40 ft or greater net thickness of "clean limestone" are shown in figures 6 and 8. The two wells with the greatest net thickness in the study area are L-6435 (pl. 2) and L-6414 (pl. 1) with 100 and 70 ft of net thickness, respectively.

The depositional buildups previously identified on the hydrogeologic sections at wells L-6435, L-5608, and L-1688 are located where the top of the basal Hawthorn unit is high (fig. 6), where the basal Hawthorn unit is thick (fig. 8), and where there is at least 20 ft of net thickness of "clean" limestone within the basal Hawthorn unit (figs. 6 and 8). Of 21 wells in which there is 20 ft or greater net thickness of "clean" limestone in the basal Hawthorn unit, 20 wells are located where the top of the unit is high relative to surrounding areas, and 18 of these 21 wells are located where the top of the basal Hawthorn unit is 500 ft below sea level or shallower (fig. 6). However, this "clean" limestone unit is not developed in all wells located where the top of the basal Hawthorn unit is high.

Principal Aquifer Systems and Hydrogeologic Units

The Floridan aquifer system is one of three principal aquifer systems in southwestern Florida. The other two are the surficial and intermediate aquifer systems. The major hydrogeologic units that underlie the study area, their stratigraphic equivalents, and approximate thicknesses are shown in figure 4.

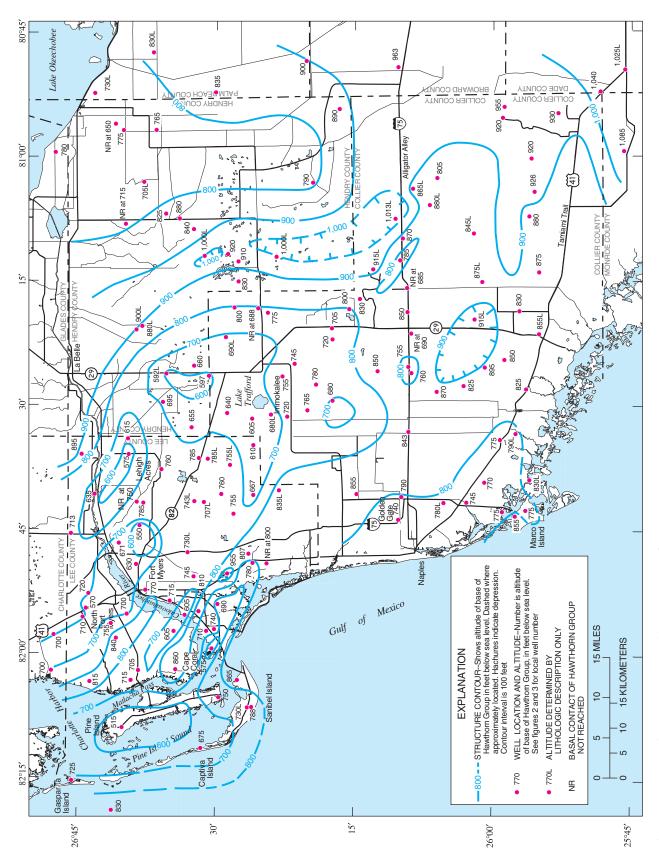


Figure 7. Altitude of the basal contact of the Hawthorn Group in the study area.

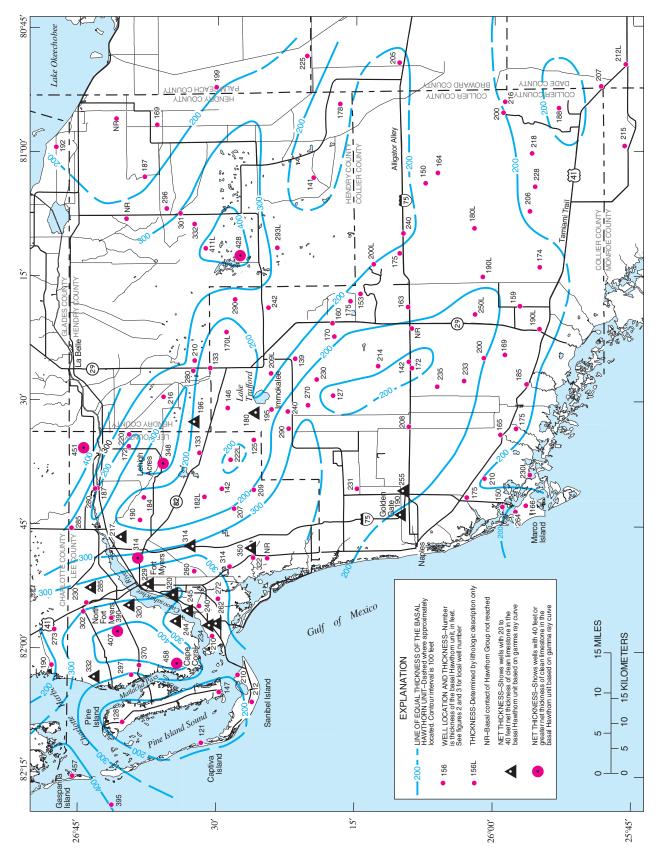


Figure 8. Thickness of the basal Hawthorn unit in the study area.

Although the Floridan aquifer system is the primary focus of this report, the surficial and intermediate aquifer systems are discussed to provide background information on the hydrogeology of southwestern Florida. The nomenclature used in this report for the various water-bearing and confining units of the aquifer systems is compared to that of previous reports in figure 9.

Surficial Aquifer System

The surficial aquifer system consists of the water-table aquifer and hydraulically connected units above the top of the first occurrence of laterally extensive and vertically persistent beds of much lower permeability (Southeastern Geological Society Ad Hoc Committee on Florida Hydrostratigraphic Unit Defini-

| Sproul and others (1972) | Wec | Wedderburn and others (1982) | Boggess and others (1981) | | tioner sint | 0 |
|---------------------------|----------------------|---|--------------------------------------|---------------------------------|--|---|
| | | Lee County | Lee, Hendry, and Collier Counties | | | Selles |
| WATER-TABLE AQUIFER | SURFICIAL AQUIFER | WATER TABLE CONFINING BEDS TAMIAMI PRODUCING ZONE | SURFICIAL AQUIFER | SYSTEM SYSTEM SYSTEM | WATER-TABLE AQUIFER CONFINING BEDS LOWER TAMIAMI AQUIFER | HOLOCENE, PLEISTOCENE, AND PLIOCENE |
| | 8 | UPPER HAWTHORN CONFINING ZONE | | ME | CONFINING UNIT | |
| SANDSTONE AQUIFER | AQUIFEI | SANDSTONE AQUIFER MID-HAWTHORN CONFINING ZONE | TAMIAMI AQUIFER | ER SYSTE | SANDSTONE AQUIFER CONFINING UNIT | |
| UPPER HAWTHORN AQUIFER | SYST | MID-HAWTHORN AQUIFER | UPPER HAWTHORN AQUIFER | AQUIF | MID-HAWTHORN AQUIFER | MIOCENE |
| | ΓWΑΗ | LOWER HAWTHORN CONFINING ZONE | | KMEDIATE. | CONFINING UNIT | AND 1.ATF |
| LOWER HAWTHORN AQUIFER |] | LOWER HAWTHORN/ TAMPA PRODUCING ZONE | | INLE | LOWER HAWTHORN PRODUCING ZONE | OLIGOCENE |
| | SLEW | CONFINING BEDS | | | CONFINING UNIT? | |
| | DIAN AQUIFER SY | SUWANNEE AQUIFER | | | PRODUCING ZONES WITHIN THE SUWANNEE LIMESTONE | EARLY |
| | FLORIE | DEEPER AQUIFER | | UPPER FLORIDIAN FLORIDAN AQU | PRODUCING ZONES WITHIN THE OCALA LIMESTONE AND AVON PARK FORMATION | AND |

Figure 9. Aquifer nomenclature for southwestern Florida used in previous studies and in this report.

tion, 1986). In southwestern Florida, the surficial aquifer system includes the water-table aquifer and the lower Tamiami aquifer (fig. 4). Generally, the watertable aguifer occurs in the undifferentiated deposits and the upper part of the Tamiami Formation; however, in some areas no undifferentiated deposits are present, and the water-table aguifer occurs in the Tamiami Formation. The lower Tamiami aquifer mostly consists of sandy, shelly limestone and calcareous sandstone that occurs in the lower part of the Tamiami Formation; commonly, the thickness is less than 60 ft. However, in some areas, the lower Tamiami aquifer extends down into unconsolidated coarse siliciclastics (quartz sand with grain size up to very coarse or granule size) that occur at the top of the Hawthorn Group. The aguifer can be much thicker in these areas (Knapp and others, 1986; Smith and Adams, 1988).

Intermediate Aquifer System

Aquifers that lie beneath the surficial aquifer system and above the Floridan aquifer system in southwestern Florida are grouped within the intermediate aquifer system (Southeastern Geological Society Ad Hoc Committee on Florida Hydrostratigraphic Unit Definition, 1986). The intermediate aquifer system does not crop out and contains water under confined conditions (Miller, 1986). The intermediate aquifer system lies within the Hawthorn Group and includes, in descending order, the sandstone aquifer and the mid-Hawthorn aquifer. The two aquifers tend to be thin in comparison to the thickness of confining units above and below (fig. 4).

The sandstone aquifer in Lee County generally is 50 to 100 ft in thickness, with the top of the aquifer ranging from 21 to 167 ft below sea level (Wedderburn and others, 1982). In Hendry County, the sandstone aquifer is divided into clastic and carbonate zones, and mapping of these zones shows that the aquifer does not extend east of the north-south boundary between Collier and Hendry Counties (Smith and Adams, 1988). Mapping of this aquifer in western Collier County shows that at about State Road 84 (Alligator Alley) the top of the aquifer lies at 250 ft below sea level and that south of this road it is absent (Knapp and others, 1986).

The mid-Hawthorn aquifer has been referred to as the upper Hawthorn aquifer by some previous investigators in southwestern Florida (fig. 9). The thickness of the mid-Hawthorn aquifer in Lee County rarely exceeds 80 ft, and the aquifer has low transmissivity. The altitude of the top of the mid-Hawthorn aquifer ranges from 100 to more than 300 ft below sea level, deepening to the east and south (Wedderburn and others, 1982). The aquifer terminates close to the Lee-Hendry County line and is not present in most of Hendry County (Boggess and others, 1981; Smith and Adams, 1988). In western Collier County, the top of the aquifer occurs at 300 to 400 ft below sea level, and the thickness averages 100 ft (Knapp and others, 1986). The geophysical log expression of the mid-Hawthorn aquifer is shown by logs run in well C-914 in southern Collier County (fig. 3 and pl. 7). This aquifer can be traced through much of the study area based on the hydrogeologic sections (pls. 1-10).

Floridan Aquifer System

The Floridan aquifer system is defined as a vertically continuous sequence of permeable carbonate rocks that are hydraulically connected in various degrees, and whose permeability is generally several orders of magnitude greater than that of the rocks bounding the system above and below (Miller, 1986). It is divided into three units; namely, the Upper Floridan aquifer, middle confining unit, and Lower Floridan aquifer. This section presents a detailed description of these units and their boundaries, thickness, and transmissivity. Also included is a description of some subunits within these three major units (fig. 4).

Upper Floridan Aquifer

The Upper Floridan aguifer includes the lower part of the Hawthorn Group, Suwannee Limestone, Ocala Limestone, and upper part of the Avon Park Formation (fig. 4). Production zones in the lower part of the Hawthorn Group and the upper part of the Avon Park Formation might or might not be present. Production zones in the lower part of the Hawthorn Group, if present, are collectively referred to as the lower Hawthorn producing zone (LHPZ) in this report, and they occur in the basal Hawthorn unit, from the base of the marker unit to the basal contact of the Hawthorn Group. The Upper Floridan aguifer in the study area generally consists of several thin water-bearing zones of high permeability interlayered with thick zones of much lower permeability, which is similar to what is found in southeastern Florida (Reese, 1994). The Suwannee Limestone in parts of Lee County can be an exception to this tendency because of the generally

coarser size and good sorting of the carbonate grains contained within the formation.

The top of the Floridan aquifer system, as defined by the Southeastern Geological Society Ad Hoc Committee on Florida Hydrostratigraphic Unit Definition (1986), coincides with the top of the vertically persistent permeable carbonate section. According to this definition, the LHPZ can be placed in the Floridan aquifer system in the study area, at least in Lee County; however, important sources of data for determining where the top of the system should be placed are geophysical logs, such as temperature and flowmeter logs, head data, and zones of lost circulation or lost returns.

Water in the Upper Floridan aquifer exists under flowing artesian conditions, so permeable zones (or flow zones) can be defined in a well based on flowmeter and temperature logs. Anomalous changes of temperature with depth (shown by large fluctuations on a temperature differential curve) or a pronounced change in the temperature gradient can help in identifying permeable zones. The vertical distribution of head can help in defining the top of the Floridan aguifer system. Potentiometric-surface maps of the Upper Floridan aquifer show a particular head or range of head values expected for an area. If this level of head has not been reached at a particular depth, the top of the aquifer would then be expected to be deeper; the Upper Floridan aquifer has a higher head than all of the aquifers above. Without detailed data in a well, including flowmeter and temperature logs or the vertical distribution of head, the top of the aquifer could be difficult to determine, particularly if the top is not defined by a lithologic change, such as the one often found at the basal contact of the Hawthorn Group.

In Lee County, the "lower Hawthorn/Tampa producing zone" (fig. 9, a unit equivalent to the LHPZ) is placed in the Floridan aquifer system where it ranges from 80 to 275 ft in thickness (Wedderburn and others, 1982). The major zone of production was found to occur near the top of the LHPZ (Wedderburn and others, 1982, p. 52). Potentiometric-surface maps for this zone (Wedderburn and others, 1982, pls. 27 and 28) show head values that are similar to those expected for the Upper Floridan aquifer in Lee County (Bush and Johnston, 1988, pl. 5). These head values range from 50 ft above sea level in eastern or northeastern Lee County to 20 or 30 ft above sea level along the coast.

Head data indicate some confinement between the LHPZ and the Suwannee Limestone of the Upper Floridan aquifer and good confinement between the mid-Hawthorn aquifer and the Suwannee Limestone. The original head in the Suwannee Limestone was about 5 ft higher than head in the LHPZ in central Lee County as estimated by Sproul and others (1972, p. 10). In the study by Sproul and others (1972), head in the "upper Hawthorn aquifer" (fig. 9, referred to as the mid-Hawthorn aquifer in this report) was estimated to be as much as 20 to 25 ft above sea level before development. Original head in the Suwannee Limestone in the area was estimated to range from 35 to 40 ft above sea level.

The basal contact of the Hawthorn Group (fig. 7) is an unconformity that probably approximates an important hydrogeologic boundary in most of the study area. Even though the top of the Floridan aquifer system is placed higher than this geologic contact, the most permeable flow zone in the Upper Floridan aquifer probably is at or near this contact in most areas. Permeable beds that are developed in the middle to upper part of the basal Hawthorn unit are not laterally continuous and are not present in much of the study area.

The top of the Floridan aquifer system can be placed based on the depth at which zones of lost circulation or lost returns are encountered. Where noted in lithologic descriptions, the tops of these zones are identified on the hydrogeologic sections (pls. 1-10). These zones generally are delimited by intervals of missing sample. The highly permeable or vuggy nature of rock in these zones results in loss of drilling fluid during mud rotary drilling, and the cutting samples that normally are brought up by the mud are lost. The hydrogeologic sections generally show that these zones first occur in the lower part of the basal Hawthorn unit or at the basal contact of the Hawthorn Group, for example, as shown by wells C-1124, C-1125, and C-1126 in Collier County (pl. 10).

In well C-1107 in western Collier County, the top of the Floridan aquifer system can be placed in the upper part of the basal Hawthorn unit (pl. 5). The top of the basal Hawthorn unit in this well is at a depth of 640 ft, and the top of the LHPZ is at 740 ft, which is the top of the first major flow zone, as indicated by the temperature log. The top of the Suwannee Limestone was placed at 870 ft based on gamma-ray log response and lithology. An anomaly on the spontaneous potential curve, recorded on the dual-induction resistivity log, occurs in association with the contact at the top of

the Suwannee Limestone. This anomaly consists of a large negative deflection, 40 mV (millivolts), at a depth of between 860 and 895 ft, which could indicate enhanced permeability associated with a flow zone at this contact.

A temperature log run on well C-914 in southwestern Collier County indicated little flow from the basal Hawthorn unit (fig. 5 and pl. 7). Apparently, the LHPZ is not developed in this well. The top of the Floridan aguifer system was placed at the top of the first significant flow zone, 880 ft deep, as indicated by the temperature log. The presence of this major flow zone is confirmed by the lithologic log of well C-914 (Knapp and others, 1986, p. I-54). Lost circulation and large cavities were encountered from 880 to 900 ft with no sample recovery. Based solely on the gammaray and resistivity logs, the top of the Floridan aquifer system in this well would have been placed at or just above the top of the Suwannee Limestone, which is at 830 ft. This example illustrates that in wells without additional logs, such as the temperature log, the top of the Floridan aquifer system can be placed at a depth that is too shallow.

In well L-6414 in northeastern Lee County, the basal Hawthorn unit is thick and the LHPZ is well developed (fig. 10 and pl. 1). The first major flow zone occurs at 620 ft, which is almost 300 ft above the top of the Suwannee Limestone. A number of other discrete flow zones occur in this well in the LHPZ and Suwannee Limestone as shown by the temperature differential curve.

The depth to the base of the Upper Floridan aguifer is variable, and the base is difficult to define. Miller (1986) defines the base using a change in vertical hydraulic conductivity of two orders of magnitude. However, the permeability data required to define the base using this definition is rarely present in the study area. Additionally, the nature of the Upper Floridan aquifer can make the use of this definition difficult because much of the aguifer in the study area consists of thick intervals of relatively low permeability. Miller (1986, pl. 29) places the base of the Upper Floridan aguifer at 2,000 to 2,100 ft below sea level in most of the study area; that is, at the top of a confining unit. This confining unit contains gypsiferous dolomite and is located in the Avon Park and Oldsmar Formations. However, the base of the Upper Floridan aguifer has been placed by others (consulting firms) at shallower depths ranging from 1,500 to 1,800 ft below land surface. Using the latter depths for the base, the thickness

of the Upper Floridan aquifer ranges from 700 to 1,200 ft (fig. 4).

In western Collier County in well C-1107, Viro-Group, Inc./Missimer Division (1993) placed the base of the Upper Floridan aguifer in the lower part of the Ocala Limestone at a depth of 1,460 ft (pl. 5). Good confinement was shown to be present below a depth of 1,800 ft in well L-5802 (pl. 1) in northern Lee County at the North Fort Myers wastewater injection well site (Post, Buckley, Schuh, and Jernigan, Inc., 1988). In well L-5802, most of the interval from 1,180 to 1,550 ft in the lower Suwannee Limestone, Ocala Limestone, and upper part of the Avon Park Formation is also interpreted to have relatively low permeability (Post, Buckley, Schuh, and Jernigan, Inc., 1988, fig. 2-10). This interpretation is based, in part, on core permeability measurements at depths of 1,341 and 1,443 ft (Post, Buckley, Schuh, and Jernigan, Inc., 1988, table 7-3). The measured specific horizontal permeability to water at these two depths, converted to hydraulic conductivity, was 0.007 and 0.024 ft/d (foot per day), respectively.

Bush and Johnston (1988, pl. 2) mapped the transmissivity of the Upper Floridan aquifer in all of Florida. Transmissivity ranges from more than 100,000 ft²/d (feet squared per day) in northern Lee and Hendry Counties to less than 50,000 ft²/d in the southern part of the study area, including most of Collier County. However, the map shows only one aquifer test site within the study area, so most of the interpretation is based on geology and simulation.

Tests to determine the transmissivity of various zones in the Upper Floridan aguifer have recently been conducted in the study area. The transmissivities of several intervals were estimated in well C-1102 (pl. 8) in southwestern Collier County based on step-drawdown data collected from open-hole packer tests (Missimer and Associates, 1991a). The total estimated transmissivity from four intervals with a combined thickness of 471 ft was 33,000 ft²/d. These intervals were included in an overall interval from 680 to 1,606 ft in depth and are referred to as the lower Hawthorn/upper Suwannee, lower Suwannee, Ocala, and Avon Park aguifers (Missimer and Associates, 1991a). The highest hydraulic conductivity was from the 80-ft thick lower Hawthorn/upper Suwannee aguifer interval; estimated transmissivity for the interval was 15,000 ft²/d. The four intervals selected probably did not cover all of the permeable parts of the Upper Floridan aquifer at the site.

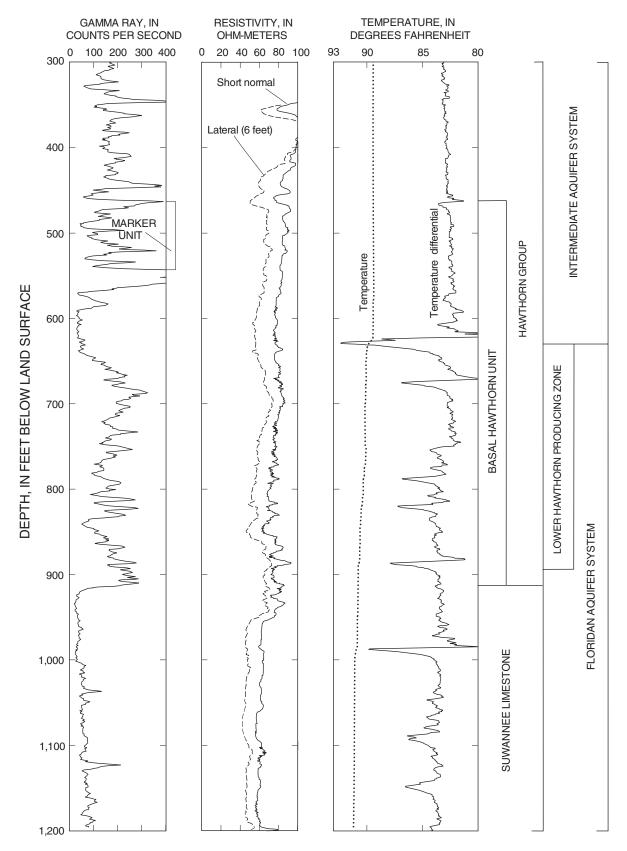


Figure 10. Geophysical logs, geologic units, and hydrogeologic units for well L-6414 in northeastern Lee County.

Three straddle packer tests were conducted in the Ocala Limestone and Avon Park Formation in well L-6471 on Gasparilla Island in northwestern Lee County (pl. 1). The three intervals that were tested (each 51 ft thick) were located in the overall interval of 1,058 to 1,543 ft. Hydraulic conductivity determined from these tests was low, ranging from 0.028 to 0.14 ft/d (Geraghty and Miller, 1986, table 2).

Transmissivity values were determined from aquifer tests in an area extending across western Lee County (Missimer and Associates, 1991b, table 4-1). Tests of the LHPZ at seven sites in the area gave a transmissivity range of between 1,800 and 12,300 ft²/d, with a corresponding range in hydraulic conductivities of between 12 and 53 ft/d. Tests of the intervals in the Suwannee Limestone or of its upper part at four sites gave a transmissivity range of between 4,400 and 9,100 ft²/d, and limited packer testing of intervals in the Ocala Limestone within the area indicated a transmissivity range of between 300 and 4,000 ft²/d (Missimer and Associates, 1991b, p. 87).

The transmissivity of the LHPZ is related to the thickness of the basal Hawthorn unit (fig. 8). When temperature logs were run, the top of the first major flow zone was near the top of the basal Hawthorn unit where the unit is thick, and near the bottom of the unit or in the Suwannee Limestone where the unit is thin (pls. 1-10). In western Lee County, the highest transmissivity of the LHPZ (12,300 ft²/d) was found in a well (Missimer and Associates, 1991b, fig. 4-12) located about 1 mi east of well L-6435 (pl. 2). The transmissivity of the LHPZ in a well on Sanibel Island near well L-6445 in Lee County (pl. 3) was measured to be only 4,000 ft²/d. High permeability in at least the upper part of the basal Hawthorn unit of well HE-1104 in central Hendry County is apparent based on lithology, the gamma-ray curve, and the separation between shallow and deep resistivity curves (pl. 4). In comparison to these values or estimates of transmissivity, the thickness of the basal Hawthorn unit in wells L-6435, L-6445, and HE-1104 is 458, 212, and 428 ft, respectively.

Another consideration in defining the transmissivity of the basal Hawthorn unit is the structure on top of this unit (fig. 6). As discussed earlier, there is evidence that some of the high areas on top of the basal Hawthorn unit, particularly those in Lee County, coincide with paleotopographic high areas created by sedimentation. Additionally, the zones of "clean" limestone developed in these paleotopographic high

areas in the middle and upper parts of the basal Hawthorn unit (figs. 6 and 8) are indicated by temperature logs to contain important flow zones. Wells with major flow zones, as shown by temperature logs, in these limestone zones are L-5608 (pl. 8), L-1688 (pl. 9), and L-6414 (pl. 1 and fig. 10). All of these wells have at least 20 ft of net thickness of "clean" limestone in the basal Hawthorn unit, and wells L-1688 and L-6414 have at least 40 ft.

Middle Confining Unit

The base of the middle confining unit of the Floridan aguifer system (fig. 4) ranges from 2,300 to 2,500 ft below sea level over most of the study area (Miller, 1986, pl. 31). The lower boundary of the middle confining unit in well C-1107 in western Collier County was placed at a depth of 2,300 ft at the top of a transmissive dolomite. The base of the unit was placed at a depth of at least 2,300 ft in three other wells, including wells C-1104 (Marco Island), L-5802 (North Fort Myers), and CH-313 (Zemel Road Landfill in southern Charlotte County). However, some wells showed evidence of transmissive dolomite or dolomitic limestone zones developed at depths less than 2,300 ft. In well L-6471 on Gasparilla Island in northwestern Lee County (pl. 1), an interval of dolomite with fractures and solution cavities occurs at a depth of 1,742 to 1,845 ft, and this interval was used for injection of wastewater (Geraghty and Miller, 1986, p. 20). Based mostly on drilling characteristics and cores, evidence suggests that zones of high transmissivity exist (Puri and Winston, 1974, fig. 24) at a depth of 2,000 ft or shallower in north-central Collier County (well C-851) and western Hendry County (well HE-343). The approximate thickness of the middle confining unit ranges from about 500 to 800 ft, as determined in this study.

Hydraulic conductivity was estimated for the middle confining unit from packer test and core data from well C-1107 in western Collier County (pl. 5). Hydraulic conductivity values from two packer test depth intervals (1,990-2,022 and 2,050-2,090 ft) ranged from 0.25 to 0.40 ft/d (ViroGroup, Inc./Missimer Division, 1993, table 13). Horizontal permeability to air was measured in six core plugs taken from a depth of between 2,013 and 2,259 ft in well C-1107. The range in values measured in these plugs was 0.01 to 55 millidarcies, which can be converted to an equivalent range in hydraulic conductivity of 3 x 10⁻⁵ to 0.15 ft/d. Specific horizontal permeability to water

was measured in three core plugs at a depth of between 1,880 and 2,261 ft in well L-5802 (pl. 1) in northern Lee County (Post, Buckley, Schuh, and Jernigan, Inc., 1988, table 7-3). The range in values measured in these plugs was converted to a range in hydraulic conductivity of 1 x 10⁻⁵ to 0.033 ft/d. By relating sonic log transit time to core permeability measurements in well L-5802, the overall vertical hydraulic conductivity for the middle confining unit was calculated for depth intervals of 1,820 to 2,150 ft and 2,150 to 2,340 ft, giving values of 0.013 and 4 x 10⁻⁴ ft/d, respectively (Post, Buckley, Schuh, and Jernigan, Inc., 1988, p. 9-7).

Among the most impermeable rock in the middle confining unit is dense, unfractured dolomite. The occurrence of gypsum or anhydrite as bedded deposits or in a disseminated form within the dolomite probably further reduces the overall vertical permeability. Gypsum occurs as interbeds as thick as 40 ft in well C-851 (pl. 5) and nearby oil wells of the Sunniland oil field in north-central Collier County (Puri and Winston, 1974, fig. 18). Based on continuous core, sample description, and geophysical well logs, these gypsum interbeds occur in well C-719 (located 0.3 mi from well C-851) from a depth of about 1,830 ft down to 2,300 ft (pl. 5). An area in western and north-central Collier County contains 50 percent or more anhydrite in the middle one-third portion of the Eocene age section (Puri and Winston, 1974, fig. 13). The thick interval containing dolomite and/or gypsum or anhydrite is referred to as the dolomite-evaporite unit in this report.

The altitude of the top of the dolomite-evaporite unit was mapped in the study area and ranges from 1,530 to 2,540 ft below sea level (fig. 11). The top of the unit was selected at the top of a sequence containing thick beds of dolomite or dolomite and evaporite minerals (gypsum and anhydrite). Beds of dolomite, 30 ft or greater in thickness, often occur in this unit and might be dense and impermeable. However, evaporite, particularly bedded evaporite, probably is not present in appreciable quantities in this unit in much of the study area, such as in eastern Hendry and Collier Counties. The most prominent feature present on the map on top of this unit is a high area trending to the northwest, beginning in central Collier County and extending into north-central Lee County (fig. 11). The top in this area is as much as 400 or 500 ft higher than in adjacent areas in central Collier County, and this high area could coincide with, or be related to, areas of maximum gypsum deposition. Hydrogeologic section

D-D' (pl. 5) extends across the axis of this high area where it is well developed; the top of the dolomiteevaporite unit is at 1,728 ft below sea level in well C-712 and decreases to 2,260 ft below sea level in well HE-282 to the west of the high area. The top of the dolomite-evaporite unit probably represents an important hydrologic boundary when thick beds of dense dolomite or evaporite of low vertical permeability are present. This top could be considered to be the top of the middle confining unit in some of the study area, particularly in areas where the top of the dolomiteevaporite unit is high. However, in eastern Hendry and Collier Counties where the top of the unit is 2,000 ft below sea level or deeper and little if any evaporite is present, dolomite in the unit can be highly permeable and the unit can be included in the Lower Floridan aquifer.

Lower Floridan Aquifer

The altitude of the base of the Lower Floridan aguifer ranges from 3,700 to 4,100 ft below sea level in the study area (Miller, 1986, pl. 33). This aquifer includes the highly transmissive Boulder zone, which contains massively bedded, cavernous, or fractured dolomite of high permeability. The altitude of the top of the Boulder zone ranges from about 2,900 to 3,100 ft below sea level in the study area, and the zone has a thickness of about 400 ft in Collier County (Miller, 1986, figs. 21 and 23). The base of the Lower Floridan aquifer extends below the Boulder zone into permeable carbonates of the upper part of the Cedar Keys Formation, below which are massive, impermeable beds of anhydrite. Previous measurements of transmissivity of the Boulder zone in southern Florida were found to be extremely high, $3.2 \times 10^6 \text{ ft}^2/\text{d}$ (Meyer, 1974) and 24.6 $\times 10^6 \text{ ft}^2/\text{d}$ (Singh and others, 1983).

In an east-west cross section of southern Florida extending through Collier County, Meyer (1989, fig. 3) shows that an upper dolostone unit and a middle dolostone unit are present in the Lower Floridan aquifer above the lower dolostone Boulder zone. These overlying dolostone units have transmissivity, which probably is an order of magnitude less than that of the Boulder zone (Meyer, 1989, p. 10).

Evidence obtained from drilling deep wells for injection of wastewater or brine into the Lower Floridan aquifer indicates that zones similar to the Boulder zone are developed higher in the section. A highly permeable "Boulder zone" extends from 2,560 to 3,330 ft below land surface in well C-1107 in

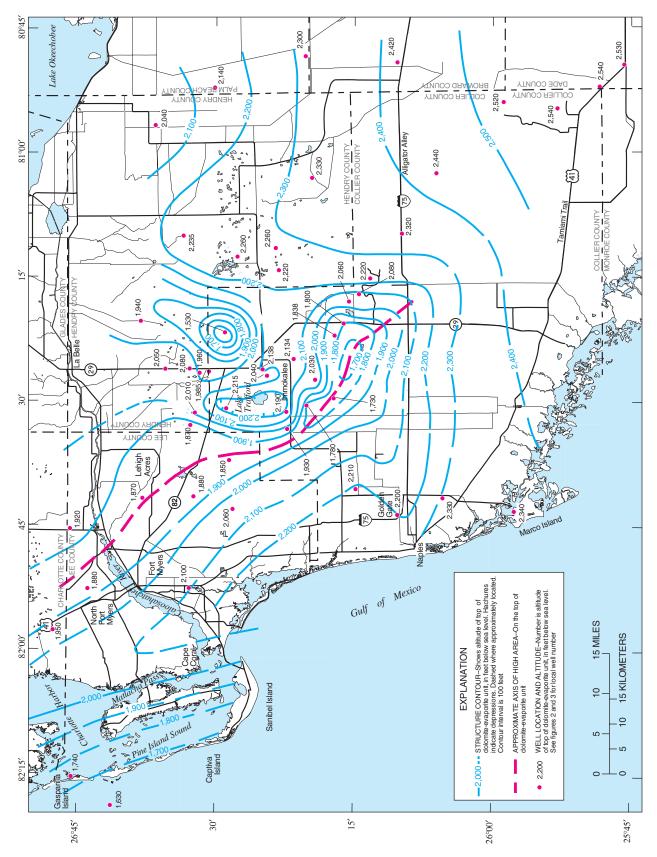


Figure 11. Altitude of the top of the dolomite-evaporite unit in the middle confining unit of the Floridan aquifer system in the study area.

western Collier County as determined by ViroGroup, Inc./Missimer Division (1993, p. 13). This depth interval consists of permeable units alternating with impermeable units, and the thickness of the permeable units ranges from 20 to 130 ft (ViroGroup, Inc./Missimer Division, 1993, p. 14). The depth interval completed for wastewater injection in well C-1107 was 2,497 to 3,390 ft. A depth interval containing cavernous dolomite was found in well L-5802 in northern Lee County, extending from 2,340 to 2,600 ft (Post, Buckley, Schuh, and Jernigan, Inc., 1988, p. 9-1). This same depth interval was completed for wastewater injection in well L-5802, and the transmissivity for the interval was determined to be 67,000 ft²/d. In well C-820, drilled for the disposal of brine produced in an oil field in north-central Collier County, the depth interval completed for injection was 2,004 to 2,500 ft.

DISTRIBUTION OF SALINITY IN THE FLORIDAN AQUIFER SYSTEM

An investigation of the distribution of salinity in the Floridan aquifer system in southwestern Florida indicated that the system could be divided into the same three salinity zones based on geophysical log responses, as was done in an earlier study in southeastern Florida (Reese, 1994, p. 30). These zones, in order of increasing depth, are a brackish-water zone, a transition zone containing moderately saline water (the salinity transition zone), and a saline-water zone. Salinity increases rapidly with depth in the salinity transition zone. This zone was defined based on a salinity equivalent to a dissolved-solids concentration of 10,000 mg/L (a chloride concentration of about 5,240 mg/L) at its top and 35,000 mg/L (a chloride concentration of about 18,900 mg/L) at its base. The concentration used at its base is a salinity value similar to that of seawater. The boundaries of these three zones were determined in all wells with either geophysical logs or water-quality data or both.

The section includes an evaluation of formation water salinity based on borehole resistivity logs, estimates of porosity, formation temperature, and the empirical cementation factor, *m*. Several types of resistivity tools were used in the study and are described in this report. This section also defines and maps the brackish-water, salinity transition, and saline-water zones; describes the distribution of salinity by salinity zone; and maps the distribution of sulfate. Sulfate can be a significant part of the dissolved solids in ground water from the Floridan aquifer system in southwestern Florida.

Evaluation of Formation Water Salinity Based on Geophysical Logs

Two threshold salinity values of interest in the Floridan aquifer system are dissolved-solids concentrations of 10,000 and 35,000 mg/L. As previously defined, a dissolved-solids concentration of 10,000 mg/L separates brackish and moderately saline water, and a dissolved-solids concentration of 35,000 mg/L separates moderately saline water and saline water. Depths to the tops of zones in the Floridan aquifer system that contain water with these threshold salinity values or greater can be approximated based on borehole geophysical logs (Reese, 1994). Additionally, the salinity of formation water at a particular depth, or an average over a depth interval, can be estimated.

Use of the term "formation" in this report refers to the bulk rock or sediment including the contained water under ambient conditions, and "formation water" is equivalent to the term "ground water." The salinity of formation water is directly proportional to resistivity of the water. If this water resistivity and the formation porosity are known, the resistivity of the formation containing this water can be determined.

Determination of Formation Resistivity

The resistivity of a nonshaley, water-bearing formation is related to the porosity and resistivity of the formation water according to the following equation (Archie, 1942):

where

 R_o is the water-saturated formation resistivity, in ohm-meters,

a is an empirical constant,

Ø is total or bulk formation porosity as a fraction,

m is the cementation factor, an empirical number that increases with compaction and cementation, and

 R_w is the formation water resistivity, in ohmmeters

The values of R_o and R_w are at formation temperature.

Equation 1 was applied to the Floridan aquifer system in southeastern Florida by Reese (1994, p. 20) and is used in this study as well. The predominant lithology of the Floridan aquifer system in both areas is similar, with fine-grained to micritic limestone and high intergranular and intraparticle primary porosity. Based on microscopic examination of cuttings, this porosity has not undergone loss to any great extent through sealing by secondary calcite or diagenesis. Oolitic or fragmental limestone that has not been sealed by secondary calcite generally can be analyzed as though it were a clastic rock (MacCary, 1983, p. 335), and clastic rocks are analyzed based on equation 1. Equation 1 was not used for intervals containing dolomite in the Floridan aquifer system because of the difficulty in determining or predicting porosity in dolomite. These dolomite intervals have high potential for the development of extensive secondary porosity (fracture, intercrystalline, and vugular), and this porosity can be highly variable.

A borehole-compensated neutron-density log used to determine porosity was run on well C-962 in eastern Collier County (Reese, 1994, p. 20). Logderived porosity, an average of the responses from the two devices, ranged from 20 to 45 percent in the upper 1,200 ft of the Floridan aquifer system and from 30 to 40 percent throughout most of this interval (fig. 12). A general tendency for porosity to decrease with increasing depth was observed. Responses from the neutrondensity log give a measure of total porosity (eq. 1) rather than effective porosity. Because porosity responses from the density and neutron devices were usually in close agreement and because the neutron device is more affected by borehole conditions (such as hole enlargement), only the density device response from this log and other neutron-density logs run in the study area were used in the determination of porosity in this study.

Determination of porosity from the sonic log was made by calibration of its response to the density porosity response in wells in which both neutron-density and sonic logs were run. For example, both logs were run in well BF-3, which was drilled by the SFWMD in eastern Broward County (outside of the study area). Well BF-3 was drilled into the Floridan aquifer system, reaching the Avon Park Formation at a depth of 1,034 ft. Average responses for the density and sonic logs were determined over 25 zones (each 3 to 10 ft thick), within a depth

interval of 1.050 to 2.046 ft. The well was drilled through this interval with a 10.75-in. (inch) diameter bit, and because of this large initial hole size and enlargement of the hole after drilling and before logging, density porosity values were corrected for the hole size as shown by a caliper curve based on a correction chart (Schlumberger Educational Services, 1988, chart Por-15a). An interpreted linear fit was made for data from depths greater than 1,250 ft based on a matrix transit time of 43.5 µs/ft (microseconds per foot) (fig. 13A). This value for matrix transit time is a minimum value for limestone with zero porosity; the range of this parameter is from 43.5 to 47.6 µs/ft (Schlumberger Educational Services, 1988, chart Por-3). The relation for the linear fit (fig. 13A) is:

Density porosity = (sonic transit time \times 0.60) – 26.0 (2)

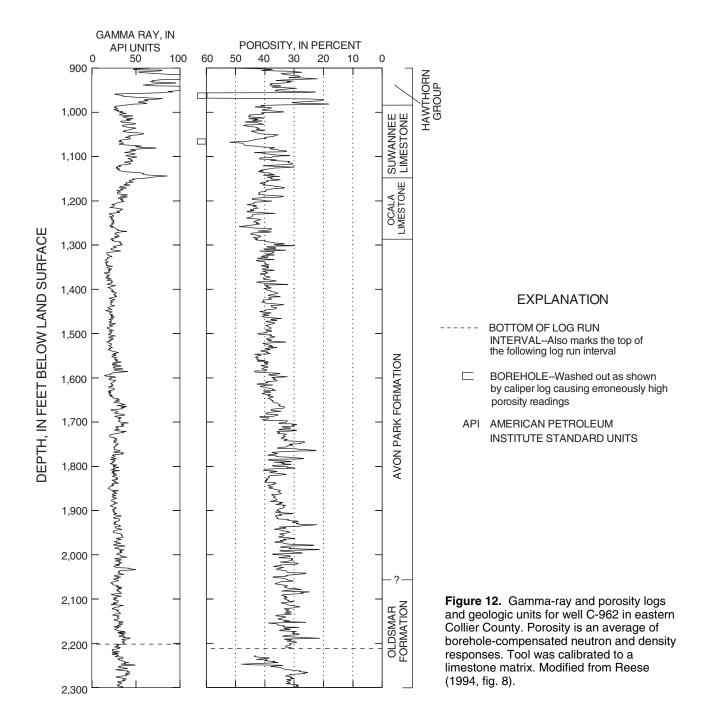
where density porosity is in percent, and sonic transit time is in microseconds per foot. Data from a depth of less than 1,250 ft do not fall on the trend of deeper data points in figure 13A, probably because the formation is less compacted at shallower depths than implied in equation 2, resulting in a transit time that is longer than that predicted for a given porosity.

Both neutron-density and sonic logs were run in well HE-1104 in central Hendry County, and responses were determined in 10 zones within a depth interval of 964 to 1,240 ft (fig. 13B). The tops of the Suwannee and Ocala Limestones in this well are at depths of 960 and 1,060 ft, respectively. Well HE-1104 was drilled with a large diameter bit of 17.5 in., and density porosity values were corrected for the hole size (Schlumberger Educational Services, 1988, chart Por-15a). An interpreted linear fit was made for the data from wells HE-1104 and BF-3 (at depths of 1,250 ft or less) based on a matrix transit time of 43.5 $\mu s/ft$ (fig. 13B). The relation for this fit is:

Density porosity = (sonic transit time \times 0.55) – 23.9 (3)

where density porosity is in percent and sonic transit time is in microseconds per foot.

Values of a and m (eq. 1), 1.0 and 2.0, respectively, are recommended for chalky limestone (Schlumberger Educational Services, 1972, p. 2). The constant a also is assumed to be equal to 1 in this study. The value of m ranges from 1.6 to 1.8 for Tertiary clean "platform type" limestones in the Southeastern Coastal Plains of the United States (Kwader, 1986).



This range for *m* could be low in comparison to the range expected in southeastern Florida in the Floridan aquifer system because of the likelihood of less compaction and cementation in the area of the Coastal Plains that excludes peninsular Florida. The depths of the Tertiary section worked within the Coastal Plains area are less than 1,000 ft (Kwader, 1986, fig. 1).

Values used for *m* have been determined from analyses of whole diameter core samples in the study

area. This parameter ranged from 1.84 to 2.30 and averaged 2.02 based on the analyses of 13 limestone core samples collected from well CH-313 in southern Charlotte County within the depth interval of 1,325 to 2,116 ft (Post, Buckley, Schuh, and Jernigan, Inc., 1992, table 7-4). The value of *m* ranged from 1.53 to 2.13 and averaged 1.92 based on the analyses of six limestone core samples collected from well L-5802 in northern Lee County within the depth interval of 1,341 to 2,261 ft (Post, Buckley, Schuh, and Jernigan, Inc.,

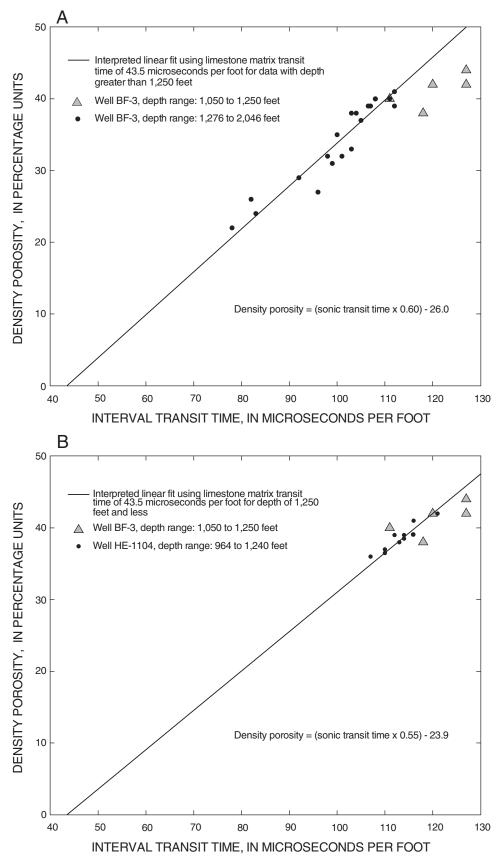


Figure 13. Plots showing relation between sonic log interval transit time and density log porosity for well BF-3 in eastern Broward County and well HE-1104 in central Hendry County. Graph A shows interpreted linear fit for depths greater than 1,250 feet, and graph B shows the fit for depths of 1,250 feet and less.

1988, figs. 7-3 to 7-8). In these analyses, m was calculated based on laboratory measured values for porosity, brine-saturated core sample resistivity, and brine resistivity. Formation water was simulated by the brine solutions used in these measurements; the solutions were synthesized based on analyses of formation water samples collected from straddle packer testing of intervals from which the core samples were taken. The value of a was constrained to be 1.0 in these calculations. The values used for m ranged from 1.8 to 2.1 in the Floridan aguifer system in southeastern Florida, which was based, in part, on core analysis (Reese, 1994, p. 22). Because of increasing compaction and cementation with depth in the Floridan aquifer system, the cementation factor, m, generally increases with depth. Average values of m used in the present study are 1.8 at depths less than 1,250 ft and 2.0 at depths greater than 1,250 ft. Use of 1,250 ft as a depth for change in the value of m is supported by the change at

that depth in the relation between sonic and density log responses (figs. 13A and 13B).

Determination of Formation Water Resistivity from Water Analysis

The formation water resistivity, R_w , for a given salinity of water in the Floridan aquifer system, as defined by dissolved-solids concentration, can be determined from water analysis. Chloride concentration can be calculated for a given dissolved-solids concentration, then by relating chloride concentration to specific conductance, water resistivity can be determined. This resistivity is corrected based on formation temperature to give R_{wr} .

Linear regression relations were developed between dissolved-solids and chloride concentrations and between chloride concentration and specific conductance of water samples collected from the Floridan aquifer system in southeastern Florida (Reese, 1994, eqs. 2-4) where water is of a sodium chloride type.

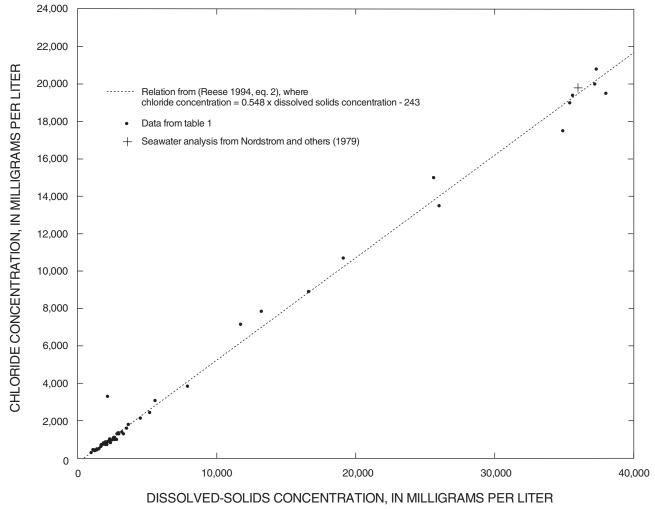


Figure 14. Relation between dissolved-solids and chloride concentrations for 54 water samples from the Floridan aquifer system in the study area.

These relations were applied to the present study of southwestern Florida where water is also a sodium chloride type (Sprinkle, 1989, pl. 9).

A plot of concentrations of dissolved solids and chloride for 54 water samples collected from the Floridan aquifer system is shown in figure 14, and a plot of chloride concentrations and specific conductance for 71 water samples is shown in figure 15. Only selected data from appendix II were used in producing figures 14 and 15 because either a constituent was not determined or the analysis was in error. Comparison of the data from appendix II with plots of lines generated based on equations 2, 3, and 4 from Reese (1994) show that these equations can be used to fit the data in the present study (figs. 14 and 15).

The resistivity of sample water, in ohm-meters, can be calculated from specific conductance, in microsiemens per centimeter at 77 degrees Fahrenheit (25 degrees Celsius), by use of the following expression:

Resistivity =
$$10,000/\text{specific conductance}$$
 (4)

The resistivity of Floridan aquifer system formation water for the two threshold salinity values, dissolved-solids concentrations of 10,000 and 35,000 mg/L, was

Table 2. Computations of the resistivity of Floridan aquifer system formation water for two salinities as defined by dissolved-solids concentration

[mg/L, milligrams per liter; µS/cm, microsiemens per centimeter at 77 degrees Fahrenheit; ohm-m, ohm-meters at 77 degrees Fahrenheit]

| Dissolved-solids concentration (mg/L) | Chloride concentration (mg/L) | Specific conductance (µS/cm) | Resistivity (ohm-m) |
|---|-------------------------------------|------------------------------------|------------------------|
| 10,000 | 5,240 | 14,800 | 0.675 |
| 35,000 | 18,900 | 48,000 | .208 |

calculated and the results are given in table 2. Chloride concentration was calculated based on equation 2 from Reese (1994) and specific conductance was calculated based on equation 3 from Reese (1994), which is the relation for chloride concentrations up to 22,000 mg/L.

The resistivity of water that is a sodium chloride type can be adjusted for a change in temperature based on a resistivity chart for sodium chloride solutions (Schlumberger Educational Services, 1988, chart Gen-9). The calculated resistivity of Floridan aquifer system formation water for the two salinity values of

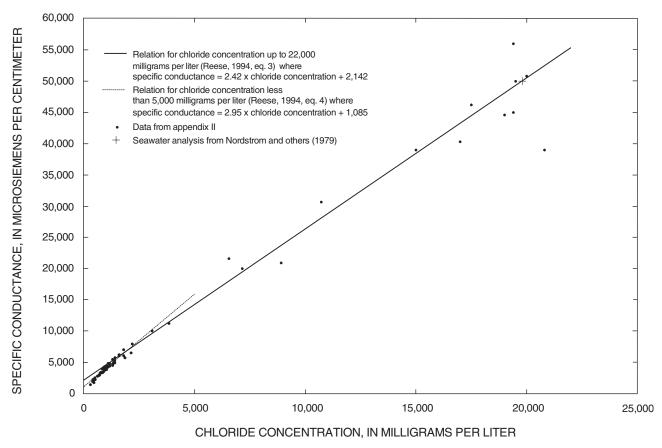


Figure 15. Relation between chloride concentrations and specific conductance for 71 water samples from the Floridan aquifer system in the study area.

interest can be adjusted from 77 degrees Fahrenheit to the formation temperature to give R_{w} .

Formation temperature in southwestern Florida in the Floridan aquifer system is higher and more variable than in southeastern Florida (Reese, 1994, p. 26). Temperature data from 18 wells were plotted against depth, in feet below land surface, as shown in figure 16. All of these data came from below the basal contact of the Hawthorn Group. Most of the data (17 measurements) came from the maximum temperature recorded during logging by a thermometer placed on a logging tool, and the remaining 7 data points came from 4 wells logged with a temperature log. For the maximum recorded temperature data, the temperature was assumed to have been set at the bottom of the logged open-hole section. A linear regression fit shows that a normal geothermal gradient generally

exists in the study area (fig. 16). However, three data points from three wells at a depth greater than 2,000 ft plot well below the linear fit (lower-than-expected temperature for their depth). These three wells are located in southeastern Collier County (wells C-962, C-1126, and C-1127), and these anomalous temperatures could result from the cooling effect of cold deep seawater that probably enters the Boulder zone along the southeastern coast of Florida in the Straits of Florida (Meyer, 1989, fig. 24). Additionally, four data points from four wells (L-6462, C-781, C-820, and HE-1106) within or just outside northern Collier County plot well above the linear fit, and all but one have a temperature of 100 degrees Fahrenheit or higher. This indicates a higher geothermal gradient in northern Collier County than the rest of the study area.

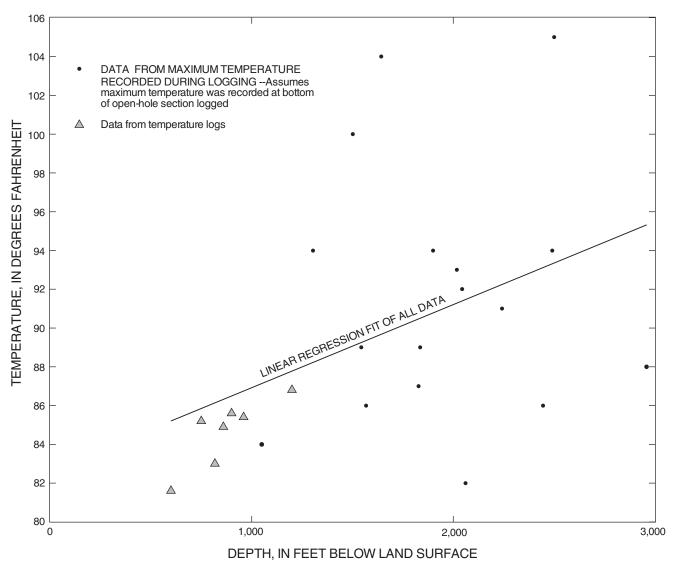


Figure 16. Relation between well depth and formation temperature for 24 water samples from 18 wells in the study area.

Table 3. Computations of formation resistivity for the Floridan aquifer system at a salinity of 10,000 milligrams per liter of dissolved-solids concentration for ranges in porosity and formation temperature

[Values used for the cementation factor, m, were 1.8 and 2.0; the value used for the constant, a, was 1.0]

| | | Format | ion resistivit | y (R _o), in ohm | n-meters |
|---------------------|-------------------|-----------------------------|-----------------------------|------------------------------|------------------------------|
| Percent porosity | <i>m</i> value | 80 degrees Fahrenheit | 90 degrees Fahrenheit | 100 degrees Fahrenheit | 110 degrees Fahrenheit |
| 20 | 1.8 | 11.8 | 10.6 | 9.6 | 8.8 |
| | 2.0 | 16.3 | 14.6 | 13.3 | 12.1 |
| 25 | 1.8 | 7.9 | 7.1 | 6.4 | 5.9 |
| | 2.0 | 10.4 | 9.4 | 8.5 | 7.8 |
| 30 | 1.8 | 5.7 | 5.1 | 4.6 | 4.2 |
| | 2.0 | 7.2 | 6.5 | 5.9 | 5.4 |
| 35 | 1.8 | 4.3 | 3.9 | 3.5 | 3.2 |
| | 2.0 | 5.3 | 4.8 | 4.3 | 4.0 |
| 40 | 1.8 | 3.4 | 3.0 | 2.8 | 2.5 |
| | 2.0 | 4.1 | 3.7 | 3.3 | 3.0 |
| 45 | 1.8 | 2.7 | 2.5 | 2.2 | 2.0 |
| | 2.0 | 3.2 | 2.9 | 2.6 | 2.4 |

Computation of Formation Resistivity for Two Threshold Salinity Values

The formation resistivity (R_o) was computed for the two threshold salinity values based on equation 1 for the expected ranges of values in porosity (\emptyset) , the cementation factor (m), and the formation temperature (tables 3 and 4). The values used for formation water resistivity at 77 degrees Fahrenheit came from table 2. These computations indicate that variation in porosity produces the greatest uncertainty in R_o . As salinity increases or decreases with depth in the Floridan aquifer system, an approximate depth at which salinity equals dissolved-solids concentrations of 10,000 or 35,000 mg/L can be determined based on the results given in tables 3 and 4, if the variation of true formation resistivity with depth is known, and the porosity and formation temperature are also known or can be estimated.

Determination of Formation Resistivity and Salinity Based on Geophysical Logs

Several borehole geophysical resistivity tools were used in this study to determine formation resistivity and salinity. These included conventional tools, such as the 16-in. normal, 64-in. normal, and 18-ft 8-in. lateral (electrical log); tools with focusing electrode devices, such as the spherically focused device, laterologs, and guard or focused log; and tools

Table 4. Computations of formation resistivity for the Floridan aquifer system at a salinity of 35,000 milligrams per liter of dissolved-solids concentration for ranges in porosity and formation temperature

[Values used for the cementation factor, m, were 1.8 and 2.0; the value used for the constant, a, was 1.0]

| | | Formati | on resistivity | / (R _o), in ohn | n-meters |
|---------------------|-------------------|-----------------------------|-----------------------------|------------------------------|------------------------------|
| Percent porosity | <i>m</i> value | 80 degrees Fahrenheit | 90 degrees Fahrenheit | 100 degrees Fahrenheit | 110 degrees Fahrenheit |
| 20 | 1.8 | 3.6 | 3.3 | 3.0 | 2.7 |
| | 2.0 | 5.0 | 4.5 | 4.1 | 3.7 |
| 25 | 1.8 | 2.4 | 2.2 | 2.0 | 1.8 |
| | 2.0 | 3.2 | 2.9 | 2.6 | 2.4 |
| 30 | 1.8 | 1.8 | 1.6 | 1.4 | 1.3 |
| | 2.0 | 2.2 | 2.0 | 1.8 | 1.7 |
| 35 | 1.8 | 1.3 | 1.2 | 1.1 | 1.0 |
| | 2.0 | 1.6 | 1.5 | 1.3 | 1.2 |
| 40 | 1.8 | 1.1 | .9 | .9 | .8 |
| | 2.0 | 1.3 | 1.1 | 1.0 | .9 |
| 45 | 1.8 | .9 | .8 | .7 | .6 |
| | 2.0 | 1.0 | .9 | .8 | .7 |

with induction devices, such as the medium and deep induction. Generally, the induction devices give the best representation of true formation resistivity.

Devices with shallow and deep depths of investigation are run on a single logging tool to estimate the depth of invasion of borehole fluid into the formation. If the depth of invasion of borehole fluid is minimal, the device with the greatest depth of investigation can be used as an approximation of true formation resistivity. If the invasion is moderate, an estimate of the true formation resistivity can be made based on correction charts when a dual induction log (medium and deep induction devices with a shallow penetrating focusing electrode device) is run. For example, with invasion of drilling fluid that contains a salinity lower than that of the formation fluid, an estimate of the true formation resistivity can be made with the dual induction log as long as the diameter of invasion is less than 70 or 80 in. (Schlumberger Educational Services, 1988, p. 90, chart Rint-2b). If the invasion is extensive, which can occur when saltwater slugs are used to control artesian pressure during drilling in the Upper Floridan aquifer, the resistivity log cannot be used. Many of the wells used for geophysical log evaluation in the study area were drilled over the section of interest with a fresh gel mud system. In these wells, invasion was minimal as indicated by the dual induction logs that were run, and the deep induction curve could be used to determine formation resistivity.

Calculation of Salinity Data

Average values of specific conductance and chloride concentration in formation water for depth intervals ranging from 50 to 300 ft in thickness were calculated for wells in which both resistivity and porosity geophysical logs were run. In a depth interval of interest for a given well, 5 to 10 zones, each 3 to 10 ft thick, were selected based on the porosity log curve (10 zones usually were selected for the thicker intervals). These zones were selected so that an average value for density porosity or sonic transit time could be easily determined. Average values of resistivity for the same zones were then determined based on the resistivity log. Based on equations 1, 2, and 3, R_w was calculated for each zone. The value of the cementation factor, m, and the relation between sonic and density porosity (eqs. 2 or 3) depended on the depth of the interval as previously discussed. The R_w values for all of the zones in the interval were averaged, and after conversion of the average R_w at formation temperature to an R_w at 77 degrees Fahrenheit, the specific conductance and chloride concentration were calculated based on equation 4 in this report and equation 3 or 4 from Reese (1994). If not measured, formation temperature was calculated based on the relation determined between depth and formation temperature in the study area (fig. 16). If formation temperature for the well was available, but not for the interval of interest, temperature was determined by interpolating between the known temperature in the well and the values shown in figure 16.

Water-quality data calculated from geophysical logs for 21 depth intervals in 17 wells are presented in table 5. Calculated chloride concentration and specific conductance for each depth interval is given. All of these depth intervals, except for four, are in the Suwannee Limestone. The depth interval in well C-962 extends down into the Ocala Limestone, and only the Ocala Limestone is included in the deeper interval calculated in well CH-313. Two other intervals, which are the deeper intervals calculated in wells C-1124 and HE-1105, are in the Avon Park Formation or deeper. For one depth interval, from 810 to 1,033 ft in well C-820, the resistivity values and calculated porosity and chloride concentration values for each of 10 zones were plotted (fig. 17).

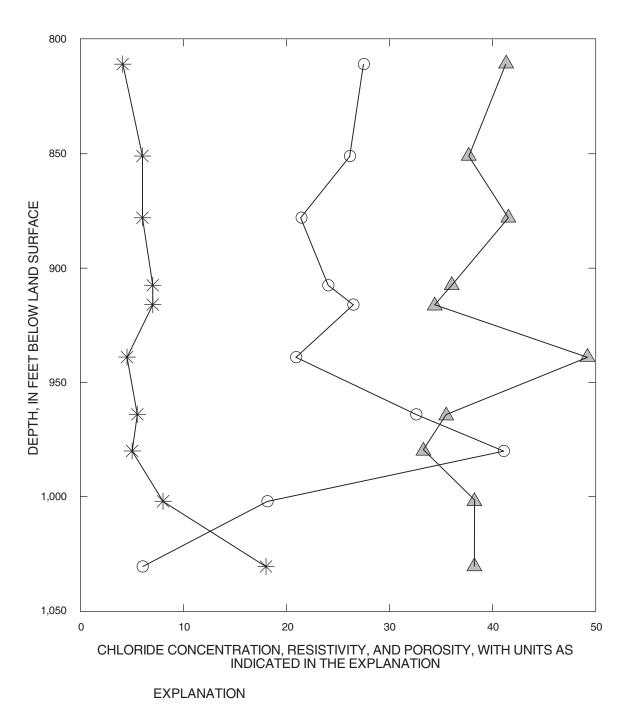
Table 5. Water-quality data calculated from geophysical logs

[Abbreviated units: ft, feet; mg/L, milligrams per liter; µS/cm, microsiemens per centimeter at 77 degrees Fahrenheit; Type of resistivity log used: DIL, deep induction, medium induction, and shallow investigation curves (dual induction); IES, deep induction and short normal curves. Asterisk indicates hole badly washed out which could result in porosity from sonic log being too high and calculated chloride concentration being too low. Depth intervals are from measuring point given in appendix I]

| Local well identifier | Depth interval analyzed (ft) | Chloride concentra- tion (mg/L) | Specific conduct- ance (µS/cm) | Type of resistivity and porosity log used |
|-----------------------|---------------------------------------|--|---|---|
| C-820 | 810-1,033 | 2,000 | 7,100 | DIL and sonic |
| C-962 | 990-1,300 | 630 | 2,900 | DIL and density |
| C-1104* | 1,046-1,092 | 13,000 | 33,000 | DIL and sonic |
| C-1107 | 896-998 | 1,900 | 6,600 | DIL and sonic |
| C-1124 | 870-1,074 | 2,600 | 8,800 | DIL and densiy |
| 0 112 1 | 1,870-1,913 | 3,100 | 10,000 | DIL and density |
| C-1125 | 854-1,038 | 610 | 2,900 | DIL and density |
| C-1126 | 919-1,038 | 630 | 2,900 | DIL and density |
| C-1130 | 800-1,080 | 1,000 | 4,200 | DIL and density |
| HE-949 | 800-1,008 | 580 | 2,800 | IES and sonic |
| HE-1104 | 964-1,060 | 680 | 3,100 | DIL and density |
| HE-1105 | 750-997 | 850 | 3,600 | DIL and density |
| ПЕ-1103 | 1,506-1,538 | 910 | 3,800 | DIL and density |
| HE-1106 | 772-1,050 | 570 | 2,800 | DIL and density |
| L-6461 | 828-1,030 | 450 | 2,400 | DIL and sonic |
| L-6462 | 710-1,010 | 1,200 | 4,700 | DIL and sonic |
| L-6463 | 810-1,120 | 630 | 2,900 | DIL and density |
| L-6471 | 730-753 | 7,600 | 20,000 | DIL and sonic |
| L-04/I | 890-940 | 19,000 | 49,000 | DIL and sonic |
| CH-313 | 728-1,016 | 560 | 2,700 | DIL and sonic |
| C11-313 | 1,350-1,410 | 840 | 3,600 | DIL and sonic |

Comparison of Calculated Values with Water-Quality Data

To help determine the accuracy of the calculated salinity data, a comparison of water-quality data calculated from geophysical logs with water samples collected from the same well (at different but proximal depth intervals) or nearby wells was made, and the results are presented in table 6. The "twin" wells given in table 6 (sequential well identifier) represent an injection (geophysical log analysis) and monitor (water analysis) well, respectively. Wells C-1125 and C-1133, although not twin wells, are located only 2 mi apart. For well L-6471, the comparison was made by assuming, based on the overall level of resistivity in the well below 765 ft, that the depth interval analyzed from 890 to 940 ft was in the saline-water zone. Salinity in the saline-water zone is similar to that of seawater (Reese, 1994), and the threshold resistivity used to define the top of the saline zone is that calculated for formation containing water with a dissolved-solids concentration of 35,000 mg/L (table 4).



Resistivity, in ohm-meters, from dual induction log Calculated chloride concentration divided by 100, in milligrams per liter Calculated porosity, in percent, derived from sonic log

Figure 17. Depth profiles of chloride concentration, resistivity, and porosity for well C-820 in northern Collier County. Each of the 10 data points represents a zone which is 3 to 8 feet thick and is plotted using a midpoint depth for the zone.

Table 6. Comparison of water-quality data calculated from geophysical logs with water samples from same well or nearby well

[Data source: SL, calculated using a sonic log; WA, water analysis; DL, calculated using a density log; SA, seawater analysis from Hem (1985). Abbreviated units or acronyms: ft, feet; mg/L, milligrams per liter; μ S/cm, microsiemens per centimeter at 77 degrees Fahrenheit; in., inches; SWZ, saline-water zone below 765 feet. Depth intervals (column 2) are from measuring point given in appendix I]

| Local well identifier | Depth interval computed or sampled (ft) | Data source | Chloride concen- tration (mg/L) | Specific conduc- tance (μS/cm) | Percent error based on chloride concen- tration | Borehole size from caliper log (in.) |
|-----------------------|--|----------------|--|---|---|---|
| C-1104 C-1105 | 1,046-1,092 1,000-1,089 | SL WA | 13,000 15,000 | 33,000 39,000 | -13 | 30 |
| C-1107 C-1108 | 896-998 900-995 | SL WA | 1,900 2,100 | 6,000 7,100 | -10 | 18 |
| C-1124 | 1,870-1,913 1,840-1,890 | DL WA | 3,100 2,440 | 10,000 | +26 | 13-15 |
| C-1125 C-1133 | 854-1,038 229-1,084 | DL WA | 610 770 | 2,900 | -21 | 18 |
| HE-1105 | 1,506-1,538 1,578-1,598 | DL WA | 910 730 | 3,800 | +25 | 18 |
| L-6471 | 890-940 SWZ | SL SA | 19,000 19,000 | 49,000 50,000 | 0 | 13 |
| CH-313 CH-314 | 1,350-1,410 1,340-1,415 | SL WA | 840 925 | 3,600 4,100 | -9 | 15 |

Average percent error based on chloride concentration = 15

The percent error of calculated chloride concentration values, assuming that the chloride concentration from the water analysis is the true value, is presented in table 6. This error ranges from 0 to 26 percent and averages 15 percent. A likely source for this error is the porosity determination based on sonic logs. If the porosity were too high, the chloride concentration would be too low, which is the case for all of the comparisons involving sonic logs except one. Density porosity was corrected for the hole size in large-diameter boreholes by lowering the porosity (Schlumberger, 1988, chart Por-15a), but no correction chart was available for the sonic log.

Large-diameter boreholes can cause an increase in the transit time measured by sonic logs, which can increase calculated porosity (Schlumberger Educational Services, 1987, p. 34). Logging tools generally are designed for 8- to 10-in. diameter boreholes, but the wells in this analysis tend to have a much larger borehole size. The borehole size was determined for the intervals calculated in table 6 based on caliper logs run at the same time as the porosity logs, with the size ranging from 13 to 30 in. (table 6). These large borehole sizes result not only from the use of large-diameter drilling bits, but also

from hole enlargement as the well is drilled deeper before casing is set. The upper part of the Floridan aquifer system is especially prone to hole enlargement because of the soft and friable nature of the limestone. Some of the error associated with sonic log readings in large-diameter boreholes is accounted for in equations 2 and 3 because these relations were determined in wells with large-diameter boreholes in which the density porosity was corrected for hole size.

Another likely source for the error between calculated and measured waterquality data in table 6 is the value used for the cementation factor, m. For well C-1124 at a depth of 1,870 to 1,913 ft (table 6), a chloride concentration of 2,600 mg/L is computed if a value for m of 1.9 is used instead of 2.0, and the percent error between calculated and measured values decreases from 26 to 8 percent. Although a value of m of 2.0 was used for all calculations of depth intervals greater than 1,250 ft in table 5, this value could be as low as 1.8.

Sensitivity of Calculated Salinity for Common Formation Resistivity Values

The sensitivity of a calculated chloride concentration in the Floridan aquifer system to porosity and the cementation factor was determined for two commonly occurring values – 10 and 20 ohm-m (ohmmeters) – of formation resistivity (fig. 18). A formation temperature of 88 degrees Fahrenheit, which is common in the Upper Floridan aquifer and the middle confining unit (fig. 16), and cementation factors of 1.8, 1.9, and 2.0 were used in the calculations from which the curves shown in figure 18 were generated. These curves show that the error in calculating a chloride concentration due to uncertainty in porosity becomes greater as the porosity decreases.

The errors between the calculated and measured water-quality data in table 6 are not large when viewed in the context of the range of variation in salinity commonly found in the Floridan aquifer system in the study area, as will be shown in the next section. The results given in table 5 are considered accurate enough to use in helping to define the distribution of salinity in the Floridan aquifer system.

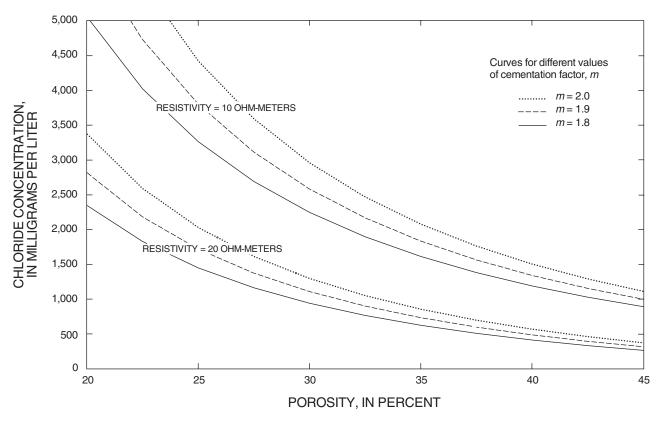


Figure 18. Calculated chloride concentration for formation resistivities of 10 and 20 ohm-meters and a range of porosity and the cementation factor, m, in the Floridan aquifer system. A value for formation temperature of 88 degrees Fahrenheit was used.

Determination of the Salinity Zone Boundaries

Geophysical logs, water-quality data collected from known intervals (completed and packer test), and water-quality data collected while drilling were used to determine the boundaries of the salinity zones in the study area. A total of 60 wells are presented in table 7; however, not enough data were available for the exact determination of the depth of one or both zone boundaries for some of the wells. The depths of the salinity zone boundaries in the Floridan aquifer system were mostly determined based on geophysical logs, with an induction resistivity device available for use in 27 wells (table 7). A porosity log (density or sonic) and a resistivity log were used to define the boundaries in 17 wells.

If only a resistivity log was run, an average porosity was used. Determination of the salinity zone boundaries in wells in which both porosity and resistivity logs were run indicated that an average porosity of 30 percent could be used when no porosity log was available. Based on this porosity and assuming a for-

mation temperature of 90 degrees Fahrenheit and a cementation factor, m, of 2.0 gives formation resistivity values of 6.5 and 2.0 ohm-m for formation water containing dissolved-solids concentrations of 10,000 mg/L and 35,000 mg/L, respectively (tables 3 and 4). These threshold formation resistivity values were used to determine salinity zone boundaries when no porosity log was run.

Water-quality data were exclusively used for nine wells to determine the boundaries of the salinity zones in the study area (table 7). However, use of water-quality data alone is probably not the most ideal means to accurately determine a salinity zone boundary in a well because of unknown depth intervals, very thick depth intervals, and/or limited number of depth intervals sampled. For water-quality data collected during drilling by the reverse-air rotary method, the depth determined for a boundary should be considered the maximum depth. This is because an increase in salinity of formation water with depth can go undetected if the formation being drilled is of low permeability.

Table 7. Depths to salinity zone boundaries in the Floridan aquifer system as determined in this study

[Methods: E, conventional electrical log (normal and lateral devices); IES, deep induction and short normal devices; DIL, dual-induction log (deep and medium induction and shallow focusing electrode devices); LL, focusing electrode devices, such as laterologs; density, porosity from density device; sonic, porosity from sonic device; QW, water-quality data (samples from known intervals); DQW, water-quality data (samples taken while drilling by reverse-air rotary method). Methods are listed in order of importance in determining boundaries for each well. Other annotations: BBZ, base of brackish-water zone; TSZ, top of saline-water zone; ?, depth of boundary or thickness of zone is uncertain; *, depth of boundary is uncertain because of dolomite interbeds; --, no data; >, greater than the value; <, less than the value. Depths are from measuring point given in appendix I]

| Local well identifier | Depth to base of brackish-water zone (feet) | Depth to top of saline- water zone (feet) | Thickness of salinity transition zone (feet) | Method |
|-----------------------|--|---|--|--------------------------------|
| C-234 | Not reached at 1,820 | Not found | | Е |
| C-708 | 1,510 to 1,960 | Not found | | Е |
| C-710 | 2,130 | Not found | | Е |
| C-711 | 1,930 | Not found | | Е |
| C-712 | 1,660 | Not found | | Е |
| C-719 | Not reached at 1,830 | Not found | | Е |
| C-726 | 1,120? | 1,740? | 620? | E (top at 1,030) |
| C-727 | Not reached at 2,080 | Not found | | E |
| C-729 | 2,050 | 2,120 | 70 | IES |
| C-820 | 2,030 | 2,365* | 335? | DIL-sonic for BBZ; DIL for TSZ |
| C-823 | 2,040 | 2,190 | 150 | DIL-sonic |
| C-914 | 1,070 | 1,110 | 40 | E |
| C-916 | Not reached at 880 | Not reached | | QW |
| C-962 | 2,155 | 2,270 | 115 | DIL-density |
| C-1102 | 900? | 1,100? | 200? | QW and DQW |
| C-1103 | 1,200 | Not reached at 1,620 | >420 | QW and DQW |
| C-1104 | 760 from well C-1101 | 910 or shallower | <150 | DQW, DIL (top at 910) |
| C-1106 | 780 (at top of Suwannee Limestone) | Not reached | | DQW |
| C-1107 | 1,200 | 1,760 | 560 | DIL-sonic |
| C-1111 | 950 | 1,280 | 330 | DIL and QW |
| C-1112 | 1,968 | 2,030 | 62 | DIL |
| C-1124 | 2,010 | 2,220* | 210? | DIL-density |
| C-1125 | 2,070 | 2,220 | 150 | DIL-density |
| C-1126 | 1,940 | 2,070 | 130 | DIL-density |
| C-1127 | Not reached at 2,060 (projected at 2,070 to 2,100) | No log | | DIL (bottom at 2,061) |
| C-1130 | Not reached at 1,830 | No log | | DIL (bottom at 1,836) |
| CH-313 | 1,560 | 1,730 | 170 | DIL-sonic |
| G-2296 | 2,175 | 2,230 | 55 | E |
| G-3239 | 1,960 | 2,070 | 110 | Е |
| HE-282 | 2,060 | 2,260 | 200 | Е |
| HE-343 | 1,920 | 2,070 | 150 | IES-sonic |

Table 7. Depths to salinity zone boundaries in the Floridan aquifer system as determined in this study--(Continued)

[Methods: E, conventional electrical log (normal and lateral devices); IES, deep induction and short normal devices; DIL, dual-induction log (deep and medium induction and shallow focusing electrode devices); LL, focusing electrode devices, such as laterologs; density, porosity from density device; sonic, porosity from sonic device; QW, water-quality data (samples from known intervals); DQW, water-quality data (samples taken while drilling by reverse-air rotary method). Methods are listed in order of importance in determining boundaries for each well. Other annotations: BBZ, base of brackish-water zone; TSZ, top of saline-water zone; ?, depth of boundary or thickness of zone is uncertain; *, depth of boundary is uncertain because of dolomite interbeds; --, no data; >, greater than the value; <, less than the value. Depths are from measuring point given in appendix I]

| Local well identifier | Depth to base of brackish-water zone (feet) | Depth to top of saline- water zone (feet) | Thickness of salinity transition zone (feet) | Method |
|-----------------------|---|---|--|-----------------------------------|
| HE-941 | <1,943 | 2,030 | >87 | E (top at 1,943) |
| HE-948 | 1,860 | 2,010 | 150 | DIL |
| HE-949 | 1,995 | 2,070 | 75 | IES-sonic |
| HE-970 | 2,084 | 2,214 | 130 | DIL |
| HE-973 | 2,000 | 2,160 | 160 | Е |
| HE-1087 | 2,070? | No log | | DIL (bottom at 2,082); QW |
| HE-1104 | 2,010 | No log | | DIL-density (bottom at 2,018); QW |
| HE-1105 | 1,840 | 1,900 | 60 | DIL-density |
| L-2657 | Not reached at 916 | | | E (bottom at 916) |
| L-4846 | 1,000? | Not reached | | E (bottom at 1,010) |
| L-5000 | All saline | | | LL |
| L-5003 | 1,690 | 1,790? | 100? | Е |
| L-5009 | >1,685 | Not found | | LL |
| L-5013 | 1,500 | 1,580 | 80 | Е |
| L-5602 | Not reached at 960 | | | E (bottom at 960) |
| L-5605 | 1,640 | 1,716 | 76 | LL-sonic |
| L-5802 | 1,560 | 1,655 | 95 | E for BBZ; DIL-sonic for TSZ |
| L-6412 | 570 | 592 | 22 | E |
| L-6423 | 1,085 | 1,130 | 45 | Е |
| L-6435 | 1,060 | | | DQW |
| L-6436 | 900 | | | DQW |
| L-6437 | 1,070 | | | DQW |
| L-6445 | 900 | | | DQW |
| L-6461 | 1,680 | 1,745 | 65 | DIL-sonic |
| L-6462 | Not reached at 1,300 | | | DIL (bottom at 1,310) |
| L-6463 | 1,530 | Not reached at 1,544 | | DIL (bottom at 1,544) |
| L-6471 | <730 | 765 | | DIL-sonic |
| PB-1137 | 2,220 | 2,540* | 320? | E |
| PB-1138 | 2,030 | 2,160 | 130 | DIL-sonic |

Geophysical logs of well L-6461 in eastern Lee County provide an ideal example in determining the boundaries of the brackish-water zone, salinity transition zone, and saline-water zone (fig. 19). The threshold formation resistivity values used for defining the salinity boundaries in this well were determined based

on porosity as calculated from a sonic log run in the well (eq. 2) and calculated formation resistivity values (tables 3 and 4). For the base of the brackish-water zone, a resistivity value of 6.2 ohm-m was determined with a calculated porosity of about 30 percent and a formation temperature of 95 degrees Fahrenheit. For

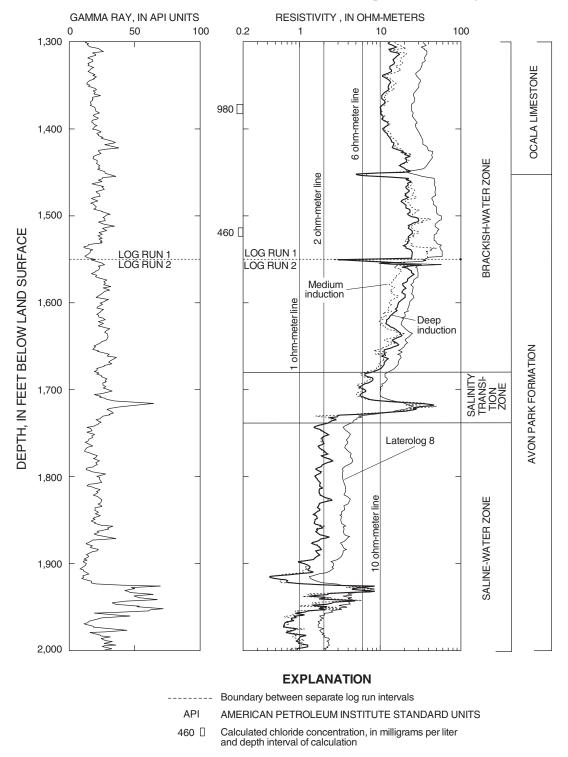


Figure 19. Geophysical logs, calculated chloride concentration, salinity zones, and geologic units for well L-6461 in eastern Lee County in the Floridan aquifer system.

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the top of the saline-water zone, a value of 1.7 ohm-m was determined with a calculated porosity of 33 percent and the same temperature.

Chloride concentrations were calculated based on geophysical logs in the brackish-water zone of well L-6461 at three depth intervals, and results indicate that salinity (at least in this well) does not greatly vary in this zone. The chloride concentration was calculated to be 450 mg/L (table 5) in the upper part of the brackish-water zone in the Suwannee Limestone at a depth of 828 to 1,030 ft. The two other depth intervals, 1,376

to 1,385 ft and 1,514 to 1,522 ft, were selected deeper in the brackish-water zone where resistivity was low (10 ohm-m) and high (22.5 ohm-m), respectively, as shown in figure 19. The calculated chloride concentrations were 980 and 460 mg/L, respectively, in these two depth intervals. No water samples were collected from well L-6461.

Salinity boundaries could not be determined in many of the wells in north-central Collier County because the salinity transition zone is either not present, which was the case for well C-727 (pl. 9 and fig. 20), or is poorly developed. Limestone is predomi-

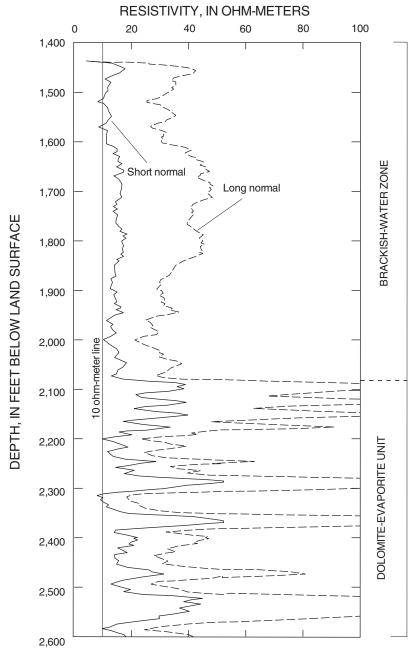


Figure 20. Resistivity geophysical log and salinity zones for well C-727 in northern Collier County. Salinity transition zone is not present.

nant in well C-727 to a depth of 2,080 ft, and thick beds of evaporite occur between 2,080 and 2,190 ft deep. The brackish-water zone extends down to the lithologic contact at 2,080 ft, which is the top of the dolomite-evaporite unit (fig. 11). The very low permeability sediments that are present below this contact probably prevent the development of the salinity transition zone.

The transition zone is not present or is poorly defined in well C-708 in northern Collier County based on a conventional electrical log (fig. 21). The base of the brackish-water zone could be present as high as 1,510 ft based on the increase in resistivity above this depth; however, the resistivity of about 8 ohm-m (medium normal) at this depth is higher than the 6.5 ohm-m value that normally is used to define the base of the brackish-water zone. Additionally, resistivity in the depth interval of 1,510 to 1,960 ft does not sharply decrease, and resistivity recorded by the medium normal device ranges from 6 to 10 ohmm. The depth of investigation for the three devices on this log increases from the short normal to the medium normal to the long lateral. The resistivity profile with distance away from the borehole shown by the curves recorded from these three devices (fig. 21) indicates invasion by saline borehole fluid. Therefore, true formation resistivity is indicated to be higher than that shown by the medium normal, and could even be higher than that shown by the long lateral curve. The long lateral curve has the greatest depth of investigation in well C-708 and is no lower than 8 ohm-m in the depth interval from 1,510 to 1,960 ft. Thus, the brackish-water zone could extend to 1,960 ft, which is the depth of the top of the dolomite-evaporite unit.

Depth to the Base of the Brackish-Water Zone

The approximate depth to the base of the brackish-water zone was determined for each well in the study area in which adequate data were available (table 7). Difficulties in determining salinity zone boundaries based on geophysical logs and waterquality data were previously described. A map showing the altitude of the base of the brackish-water zone is shown in figure 22. The base of the brackish-water zone ranges from about 565 ft below sea level in northwestern Lee County on Pine Island (well L-6412)

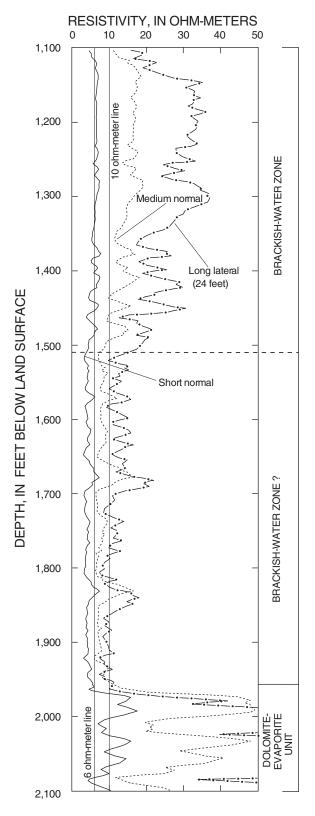


Figure 21. Resistivity geophysical log and salinity zones for well C-708 in northern Collier County. Brackish-water zone extends down to at least 1,510 feet and could extend down to 1,960 feet.

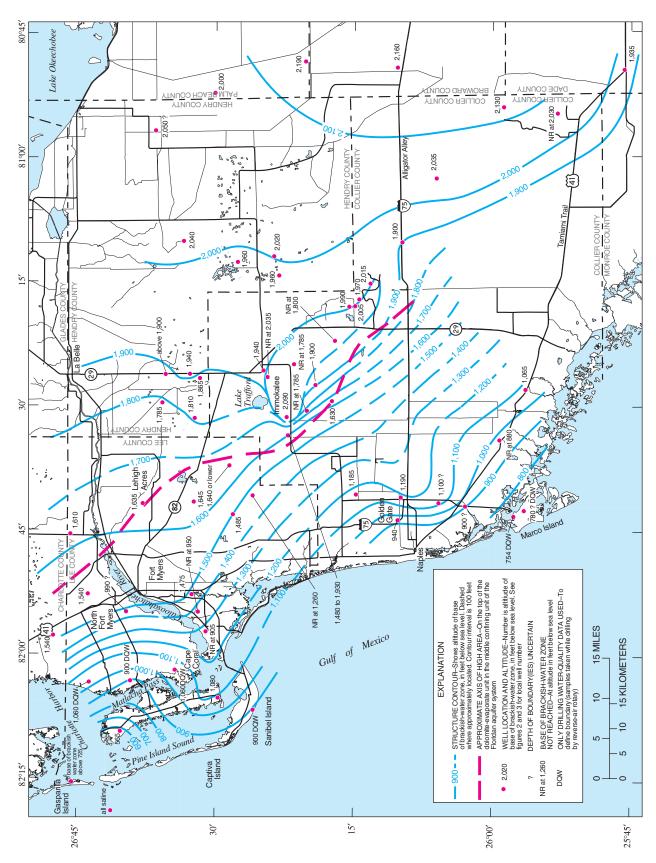


Figure 22. Altitude of the base of the brackish-water zone in the study area.

to about 2,200 ft below sea level in southwestern Palm Beach County (well PB-1137). The mapped surface, in general, rises gently to the west in most of Hendry County and far eastern Collier County and rises more rapidly to the west upon approaching the coast. The direction of the dip is opposite to that of the potentiometric surface of the Upper Floridan aquifer (Bush and Johnston, 1988, pl. 5), supporting the interpretation that the salinity transition zone represents a diffuse salinity interface, the depth of which is controlled by head in the brackish-water zone. This interpretation also is supported by the location of potentiometricsurface contours in Lee County, an area where they are well defined (Bush and Johnston, 1988, pl 5). The dip of the potentiometric surface to the west increases at a position in central Lee County that coincides with where the dip of the base of the brackish-water zone to the east increases (fig. 22).

The base of the brackish-water zone occurs near the basal contact of the Hawthorn Group in several wells within the study area. Because of the lithologic and hydrologic changes that often occur here, determination of the base of the brackish-water zone when it is near or above this contact is uncertain. Marco Island in southwestern Collier County is one area in which the base occurs at or near the top of the Suwannee Limestone. In well C-1104 on Marco Island (pl. 7), the base of the brackish-water zone was located above the basal contact of the Hawthorn Group as shown by water-quality data collected from well C-1101 (app. II), which is collocated with well C-1104 (fig. 3).

A thin zone of brackish or moderately saline water at the top of the Upper Floridan aquifer could extend farther out toward the coast than predicted based on the altitude of the base of the brackish-water zone (fig. 22). In well L-6471 on Gasparilla Island in northwestern Lee County (pl. 1), the top of the salinewater zone is at a depth of 765 ft (table 7) with the top of the Suwannee Limestone present at 730 ft (app. III). The presence of a thin zone of moderately saline water (salinity transition zone) in well L-6471 from 730 to 765 ft, as opposed to saline water, is supported by a chloride concentration of 7,600 mg/L which was calculated based on geophysical logs at a depth interval from 730 to 753 ft (table 5). The presence of this thin salinity transition zone in well L-6471 would not have been expected based on the contours shown in figure 22.

Areas of Anomalous Altitude of the Base of the Brackish-Water Zone

An anomalous low area at the base of the brackish-water zone is present in north-central Collier County (fig. 22). The brackish-water zone in this area extends deeper than expected, by as much as 300 ft. The base is at least as deep as 2,090 ft below sea level (well C-710), and the salinity transition zone is either not present or is poorly defined (figs. 20 and 21, wells C-727 and C-708). Additionally, the base of the brackish-water zone seems to rise very rapidly on the west side of the anomalous area. This is apparent in the area around wells C-711 and C-712, between which the surface rises almost 300 ft in about 3 mi, and between wells C-1107 and C-712 on hydrogeologic section D-D' (pl. 5), which extend across the anomalous area from west to east.

The origin of this anomalous area is probably related to the permeability of the sediments in the underlying middle confining unit of the Floridan aquifer system. As discussed earlier, gypsum or anhydrite is present in this unit in north-central and western Collier County at a depth as shallow as 1,800 ft, and its presence (together with dense dolomite) could substantially reduce the vertical permeability of the unit. Impermeable beds in the middle confining unit could result in a major hydrologic boundary, preventing the movement of brackish water below the top of the beds. These beds could also prevent the establishment of a normal salinity transition zone above, if this process is dependent on the upward movement of saline water from below, such as from the Boulder zone. Upward movement of saline water from the Boulder zone due to geothermal heating under the Floridan Plateau was proposed by Kohout (1965). Evidence in support of this theory is found by the presence of temperature anomalies in the Upper Floridan aquifer and warm saline-water springs located in western Lee County and north of the study area along the west coast (Meyer 1989, fig. 25).

Comparison of the location of the brackish-water zone anomalous area with the map showing the altitude of the top of the dolomite-evaporite unit (fig. 11) suggests an origin for the anomalous area. The axis of the high area on top of the dolomite-evaporite unit that trends to the northwest, starting in central Collier County, lies adjacent to the anomalous area and parallels its southwestern side (fig. 22). This high area could be acting as an impermeable sill, preventing more dense saline water from moving laterally from the

coast to the southwest and beneath the anomalous area, displacing water in the lower part of the brackish-water zone. Additionally, during the rise in sea level since the end of the Pleistocene Epoch, this sill and the dolomite-evaporite unit beneath the anomalous area could have prevented the upward adjustment of the salinity interface in the anomalous area, an adjustment which probably occurred in most other areas.

Another anomalous low area at the base of the brackish-water zone is in western Collier County to the southwest of the area described above (fig. 22). Also in this area, the base of the brackish-water zone is deeper than expected as shown by well C-726 (base at 1,100 ft below sea level), and the salinity transition zone is not well developed as shown by well C-1103, where the thickness of this zone is 420 ft or greater (table 7). Gypsum or anhydrite might also be present in the middle confining unit of the Floridan aquifer system in this area, reducing its permeability and possibly preventing the development of a brackish-water/saline-water interface at equilibrium because of retardation of the upward movement of saline water.

Distribution of Salinity by Zone

Water-quality data used to describe salinity in the Floridan aquifer system in this report were selected from data collected as early as 1941. In most of the study area, conditions are not believed to have changed enough to have significantly affected predevelopment water quality. This is because development of the Floridan aguifer system in southwestern Florida, as in the rest of southern Florida, has been minimal. One exception could be the area along the Caloosahatchee River in Lee County where the potentiometric surface in the LHPZ and Suwannee Limestone portion of the Upper Floridan aquifer declined as much as 8 ft from the 1944-50 to the 1966-73 period (Boggess, 1974, fig. 5). This area extends 4 to 5 mi away from the river on both sides. However, as will be shown based on the data in appendix II, salinity even in this area has not increased relative to surrounding areas. Decline of the estimated predevelopment potentiometric surface of the Upper Floridan aguifer in all of southern Florida was less than 10 ft in May 1980 (Bush and Johnston, 1988, pl. 6).

Many of the wells completed in the Floridan aquifer system in the study area, particularly in Lee County, were short cased, such that either the sandstone aquifer or mid-Hawthorn aquifer of the interme-

diate aquifer system or both are open for production in addition to the LHPZ of the Upper Floridan aquifer. Samples in appendix II were selected to show waterquality data from the LHPZ or deeper and to avoid wells open in at least the sandstone aquifer. In Lee County an attempt was made to select samples for which the top depth of the interval sampled was at a minimum depth of 300 ft, and the bottom of the sample interval was deeper than about 200 ft above the basal contact of the Hawthorn Group as determined by figure 7. The value of 200 ft is related to the thickness of the LHPZ.

Brackish-Water Zone

Because many wells are open to more than one producing zone, few water-quality data were available to map the distribution of salinity by zone or formation in the upper part of the brackish-water zone; therefore, this was not done for the study. However, if the basal contact of the Hawthorn Group marks a major hydrologic boundary, such as the top of the Floridan aquifer system, a significant change in salinity across the contact could be present. A total of 39 water samples from 38 wells (app. II) were identified where the sampled depth interval did not overlap the basal contact of the Hawthorn Group but was still above the base of the brackish-water zone. The interval was located above the contact for 21 of these samples and was located below the contact for 18 of these samples. A plot of the midpoint depth of the sample interval and chloride concentration for each sample was made with points distinguished by this grouping (fig. 23). This plot shows that salinity does not change substantially between the sampled intervals above and below the basal contact of the Hawthorn Group.

A decrease in salinity with depth can occur across the basal contact of the Hawthorn Group in inland areas. For example, in western Broward County, well G-2296 and monitor tube G-2618 (pl. 6), within the same well, were completed above and below the basal contact of the Hawthorn Group, which is at a depth of 980 ft. Depths of completed intervals sampled were 811 to 816 ft in well G-2296 and 1,104 to 1,164 ft in monitor tube G-2618; chloride concentrations of recovered water samples were 1,600 and 620 mg/L, respectively (app. II).

A map showing the distribution of chloride concentration in the upper part of the brackish-water zone (fig. 24) was constructed based on selected water sample analyses (app. II) and water-quality data calcu-

lated from geophysical logs (table 5). The geologic units analyzed include the LHPZ, Suwannee Limestone, Ocala Limestone, and the Avon Park Formation, although only one well has a depth interval in the Avon Park Formation (well HE-1107 from 1,546 to 1,579 ft; app II). Emphasis is on the LHPZ and Suwannee Limestone with all but six of the water analyses from intervals with a bottom depth of about 1,100 ft or less, and all but one log analysis with the depth interval located only in the Suwannee Limestone.

Chloride concentrations in the upper part of the brackish-water zone range from about 400 to 4,000 mg/L (fig. 24). Concentrations are low in three large areas as generally defined by the 400- and 800-mg/L contours shown in figure 24. One of these areas is along the northern side of the Caloosahatchee River in Lee County, extending to the southwest across Pine and Captiva Islands; the second area is in southeastern Lee County, extending southeast into north-central Collier County; and the third area is in eastern Hendry and Collier Counties.

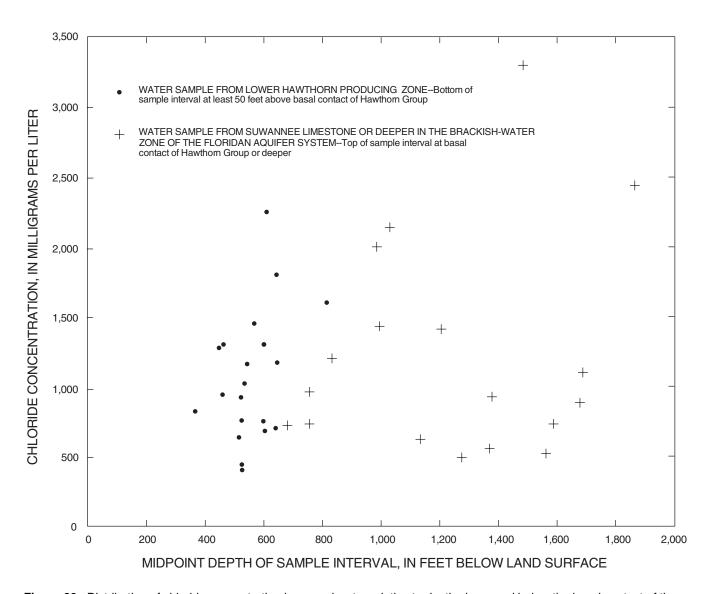


Figure 23. Distribution of chloride concentration in ground water relative to depth above and below the basal contact of the Hawthorn Group.

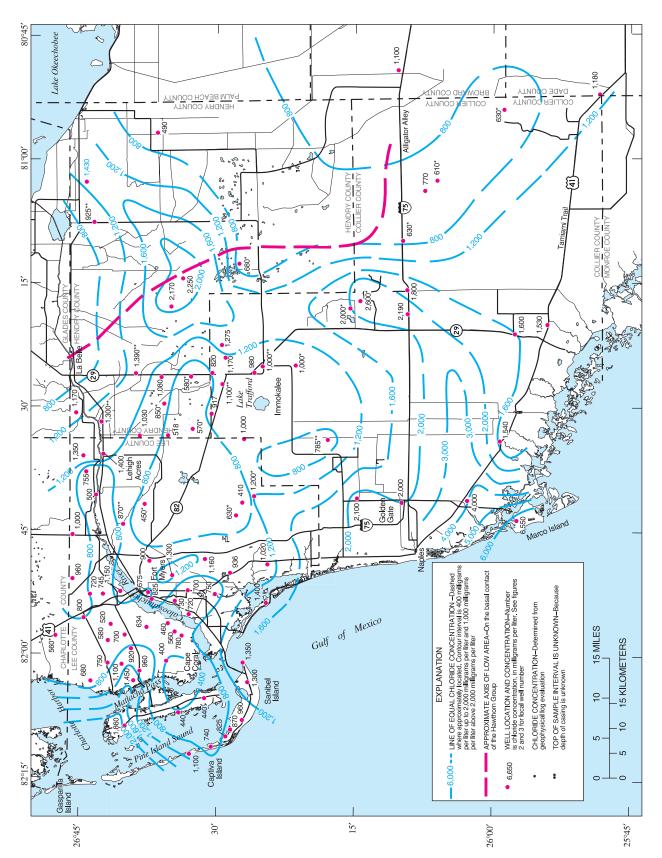


Figure 24. Lines of equal chloride concentration in ground water from the upper part of the brackish-water zone in the Floridan aquifer system in the study area.

A review of the chloride concentrations was made for the area along the Caloosahatchee River in which Boggess (1974, fig. 5) found significant drawdown in the potentiometric surface of the LHPZ and Suwannee Limestone portion of the Upper Floridan aquifer. A matching area of high salinity, which could have resulted from this drawdown due to upward movement of saline water from the salinewater zone, was not found (fig. 24). Well L-5611, located close to the north bank of the river in North Fort Myers, was the only well that had higher-thanexpected salinity in this area of drawdown, with a chloride concentration of 1,150 mg/L (app. II). In well L-4846, also located along the northern bank of the river near North Fort Myers, the base of the brackish-water zone occurred at a depth of about 1,000 ft (table 7), which was much shallower than expected based on the altitude of the base of the brackish-water zone in the area (fig. 22).

If the area of low salinity in southeastern Lee County extending into north-central Collier County, as defined by the 800-mg/L line of equal chloride concentration in figure 24, is expanded to include the area defined by the 1,200-mg/L line, this area coincides with an area of high altitude at the basal contact of the Hawthorn Group (fig. 7). The surface mapped at the basal contact of the Hawthorn Group dips away in all directions from this area of relatively low salinity, except to the northwest, and continues to dip down to the east until a low area is reached in western Hendry County, as shown by the axis of low altitude of the basal contact of the Hawthorn Group (fig. 24).

The increase in salinity in central and northwestern Hendry County coincides with the development of a thick basal Hawthorn unit, with higher salinity in this unit than in the underlying formations. Wells HE-296 and HE-297 completed only in the LHPZ are in this area where the unit is thick (fig. 8). The produced water from these wells has a chloride concentration greater than 2,000 mg/L (fig. 24). In well HE-1104 (figs. 1 and 8, pl. 4) also in this area of thick basal Hawthorn unit, salinity in the basal Hawthorn unit is high, as indicated by the low level of resistivity recorded by the deep induction resistivity curve. The resistivity in much of the basal Hawthorn unit in this well is significantly less than 10 ohm-m, whereas in most other areas, resistivity in the unit is higher than 10 ohm-m (pl. 2). The resistivity in the brackish-water zone below the basal Hawthorn unit in well HE-1104 is 20 ohm-m or greater, which indicates relatively low salinity (pl. 4).

The increase in salinity in central Collier County results from a salinity increase in the lower part of the basal Hawthorn unit and the Suwannee Limestone, but not necessarily in deeper units. For example, geophysical log evaluation shows that the calculated chloride concentration in the Suwannee Limestone in well C-820 averages more than 2,000 mg/L over a depth interval of 810 to 1,033 ft (fig. 17); however, the calculated chloride concentration in individual zones within this interval decreases to less than 1.000 mg/L at 1,030 ft, which is toward the base of the Suwannee Limestone (fig. 17). Resistivity in the lower part of the Suwannee Limestone and the upper part of the Ocala Limestone in well C-820 is 10 ohm-m or greater (pl. 5). Additionally, salinity is higher in the Suwannee Limestone than in underlying formations in well C-1124 (near well C-820) as shown by high values on the deep induction resistivity curve (pl. 10).

The areas of higher salinity discussed above in central and northwestern Hendry County and central Collier County have common characteristics and could have a similar origin. In these areas, the higher salinity is within the basal Hawthorn unit or Suwannee Limestone only. Additionally, the basal contact of the Hawthorn Group is relatively deep in these areas. The higher salinity in these areas could have resulted from the influx of seawater into zones of higher permeability in structurally low areas during high sea-level stands of the Pleistocene Epoch. The influx of seawater could have come from the area to the southwest of well C-820 in southwestern Collier County. A similar origin for areas of high salinity in the Upper Floridan aquifer near or along the coast in southeastern Florida was proposed by Reese (1994, p. 45). Flushing of these areas by fresher water after the high stand due to the lowering of sea level and the buildup of head in the Upper Floridan aquifer has not been complete.

The origin of the area of high salinity that extends from southwestern Collier County into central Collier County could also be related to structure and tectonic movements. As previously discussed, a narrow low area trending northeast-southwest at the top of the basal Hawthorn unit is present in this area (fig. 6), and the origin of this low area could be related to possible faults that bound it, particularly along its northwest side. If such faulting does exist, it could have resulted in permeability enhancement in a direction parallel to the faulting due to fracturing and dissolution in the Upper Floridan aquifer, and this enhanced permeability could have allowed the movement of saline water from the southwest.

High salinity occurs in some areas along the coast in the upper part of the brackish-water zone because the base of the brackish-water zone (fig. 22) rises up close to or above the basal contact of the Hawthorn Group (fig. 7). This occurs in the Marco Island area of southwestern Collier County (fig. 24). A water sample collected from well C-1101 had a chloride concentration of 6,550 mg/L at a depth of 800 ft while drilling in the basal Hawthorn unit (app. II). The base of the brackish-water zone extends above the basal contact of the Hawthorn Group in the Marco Island area (pls. 7 and 8, well C-1104). Another area of high salinity along the coast occurs on islands in far northwestern Lee County (fig. 24). The base of the brackish-water zone also rises up to the basal contact of the Hawthorn Group and higher in this area (pl. 1 and fig. 22).

Salinity Transition Zone

The salinity transition zone is an interface that forms because of equilibrium between two water masses of contrasting density. A salinity transition zone with a thickness of 150 ft or less was found in most of the study area (table 7), indicating that a brackish-water/saline-water interface has developed similar to what was found in southeastern Florida (Reese, 1994, p 43). The thickness of the transition zone in southeastern Florida in 10 of the 18 wells in which it was measured was 124 ft or less (Reese, 1994, p. 40). However, the thickness of the transition zone in southwestern Florida can be much greater than 150 ft. In the anomalous area on the surface at the base of the brackish-water zone in western Collier County, the thickness of the salinity transition zone is 560 ft in well C-1107 and possibly as much as 620 ft in well C-726 (table 7).

Saline-Water Zone

Variability in salinity is minor in the salinewater zone as shown, for example, by the low variability in resistivity (at least down to 1,910 ft) in well L-6461 (fig. 19). Depth intervals below 1,910 ft with resistivity less than 1 ohm-m, such as the one from 1,910 to 1,925 ft where resistivity is as low as 0.5 ohm-m, probably are where the borehole is greatly enlarged because of the collapse of fractured dolomite or the presence of cavernous features. Assuming a salinity similar to a dissolved-solids concentration of 35,000 mg/L and a porosity at this depth of not greater than 40 percent, a formation resistivity of at least 1 ohm-m is expected (table 4). The presence of an enlarged borehole in these intervals is confirmed by a

caliper curve recorded with the sonic log in well L-6461. If dolomite is present, the resistivity would be expected to be high because of the low porosity characteristic of dolomite; dolomite beds are present from 1,920 to 1,960 ft in well L-6461 as indicated by the high resistivity and gamma-ray spikes (fig. 19).

Although the salinity of water in the salinewater zone is similar to seawater, there is some variability. Based on wells in which the depth to the top of the saline-water zone was determined (table 7), 13 results of analyses in appendix II were found to be from intervals in the saline-water zone. Of these, considering only the analyses from completed intervals, the minimum and maximum values for chloride concentration were 17,500 and 20,800 mg/L, respectively. In comparison, two analyses of seawater give chloride concentrations of 19,000 mg/L (Hem, 1985, table 2) and 19,800 mg/L (Nordstrom and others, 1979). Water samples collected from the Boulder zone of the Lower Floridan aguifer were not used in this report, but the average dissolved-solids concentration of Boulder zone water from eight wells in southeastern Florida was 37,000 mg/L, which is slightly higher than that normally found in seawater (Reese, 1994, p. 40).

Distribution of Sulfate

The influence of gypsum dissolution and mixing with seawater on the concentration of sulfate in water from the Floridan aquifer system can be evaluated by plotting the sulfate-to-chloride equivalent ratio against sulfate concentration (Rightmire and others, 1974). Based on 60 water analyses from appendix II, a plot was constructed showing that sulfate in water from the Floridan aquifer system generally comes from the mixing of dilute ground water with seawater (fig. 25). However, the position of much of the data on the plot indicates that a small portion of the sulfate was derived from gypsum dissolution.

A plot of chloride and sulfate concentrations of the same data used in figure 25 shows that the three salinity zones, as defined in this study, plot in different positions in relation to a pure water-seawater mixing line (fig. 26). The salinity zone from which each water sample came was determined for all of the data points in figure 26 based on determined salinity zone boundaries (table 7). All of the data points with chloride concentrations less than 4,000 mg/L are from water samples collected in the brackish-water zone, and most of these plot above the mixing line. The points that have intermediate chloride concentrations from 7,150 to 17,000 mg/L are from the salinity transition

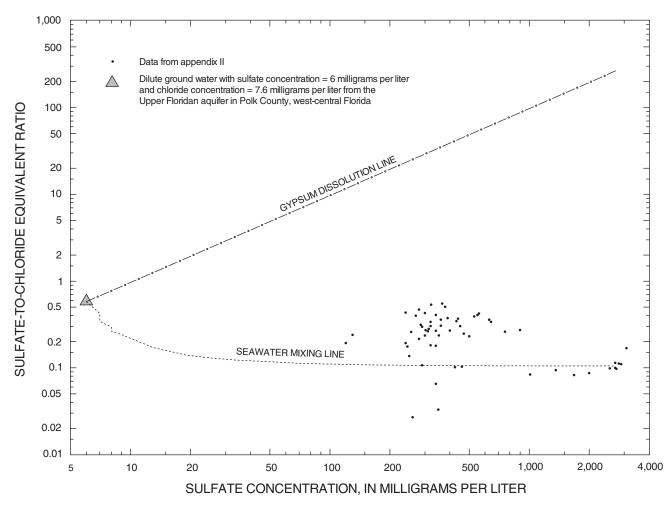


Figure 25. Sulfate concentration and sulfate-to-chloride equivalent ratio for 60 water samples from the Floridan aquifer system with relation to the gypsum dissolution and seawater mixing lines. (Modified from Rightmire and others, 1974.)

zone, and all but one plot below the mixing line. The six points that have chloride concentrations more than 17,000 mg/L plot close to the mixing line, and all of these samples were collected from the saline-water zone. The depletion of sulfate that apparently occurs in the salinity transition zone probably is the result of sulfate reduction. This process commonly occurs in the Upper Floridan aquifer in Florida (Katz, 1992, fig. 22).

The one data point from the salinity transition zone that plots well above the pure water-seawater mixing line in figure 26 has chloride and sulfate concentrations of 13,500 and 3,080 mg/L, respectively. These concentrations were measured in well C-820 in north-central Collier County at a depth interval of 1,998 to 2,500 ft (app. II). Although most of this sampled interval is in the salinity transition zone, the bottom 135 ft could be in the saline-water zone

(table 7 and pl. 5). The high sulfate concentration in this water sample can be explained by the occurrence of gypsum or anhydrite at these depths.

Thirty-nine analyses from appendix II were used to map the distribution of sulfate in the brackish-water zone in southwestern Florida (fig. 27). In the interval sampled, five analyses came from the lower part of the brackish-water zone, and the remaining analyses came from the upper part of the brackish-water zone. The area with the highest concentration of sulfate lies in north-central and western Collier County where, for example, 900 mg/L was determined in well C-1124. Another smaller area where the sulfate concentration is relatively high (greater than 300 mg/L) is in north-central Lee County and south-central Charlotte County. The area with the lowest concentration of sulfate (120-300 mg/L) occurs in western Lee County to the west of the Caloosahatchee River.

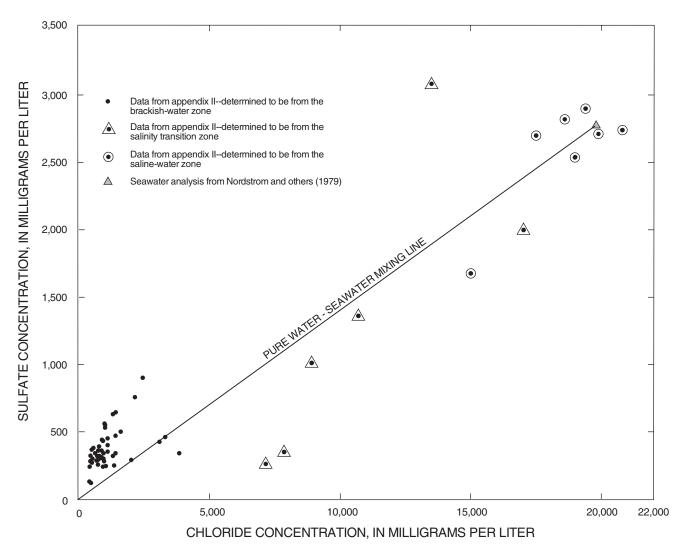


Figure 26. Distribution of chloride and sulfate concentrations in ground water from the Floridan aquifer system relative to a pure water-seawater mixing line. Data showing grouping relative to mixing line by salinity zone.

The area of high sulfate concentration in north-central and western Collier County coincides with the area of gypsum or anhydrite occurrence in the middle confining unit of the Floridan aquifer system, suggesting that the higher sulfate concentration in the brackish-water zone is probably related to this occurrence. Gypsum in the middle confining unit probably also occurs in the other area of higher sulfate concentration in north-central Lee and south-central Charlotte Counties. This is supported by the northwest-trending high area at the top of the dolomite-evaporite unit in the middle confining unit (fig. 11), which probably resulted from gypsum deposition. The axis of this high area passes near or through these two areas of higher sulfate concentration.

High sulfate concentration occurs in the Upper Floridan aquifer in southwestern Florida just to the

north of the study area. Geochemical modeling indicates that these elevated sulfate concentrations result from the upwelling of deeply circulating ground water within the freshwater flow system of the Upper Floridan aquifer, with the source of the sulfate being gypsum dissolution in the lower part of the flow system (Sacks and Tihansky, 1996). In all of the area studied in this report, the Upper Floridan aquifer is confined with only the possibility of discharge occurring (Bush and Johnston, 1988). Therefore, some upwelling of deeply circulating ground water could also be occurring in the brackish-water zone in the study area. This upwelling could help to explain the areas of high sulfate concentration (fig. 27) and explain why these higher values are found in the upper part of the brackish-water zone where gypsum is not known to occur.

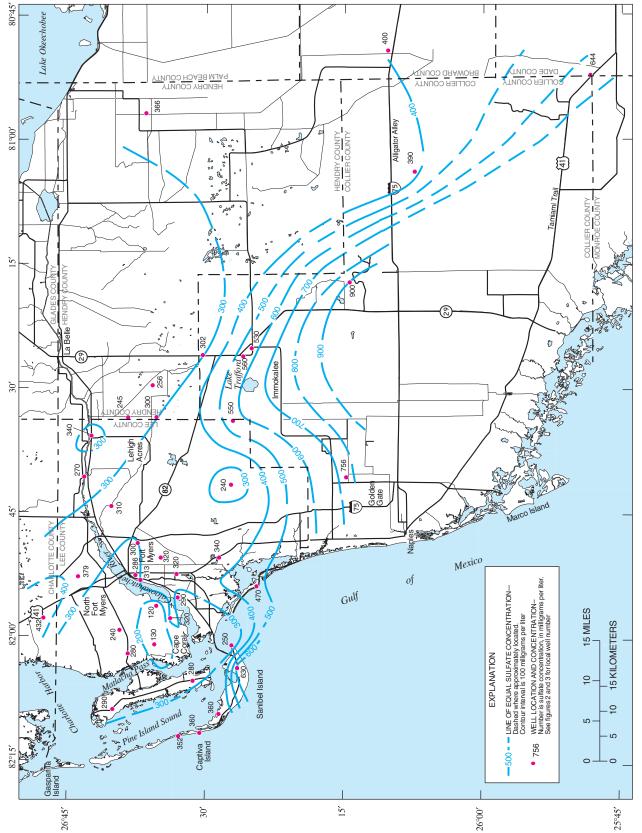


Figure 27. Lines of equal sulfate concentration in ground water from the brackish-water zone of the Floridan aquifer system in the study area.

SUMMARY AND CONCLUSIONS

The Floridan aquifer system is considered to be a valuable supplemental source for public-water supply in southwestern Florida even though it contains only brackish water. Aquifers in shallower aquifer systems in this area are limited by comparison or have been seriously impacted by pumpage or saltwater intrusion. The primary purpose of this study was to establish and describe the hydrogeologic framework, describe and evaluate the distribution of salinity in the aquifer system, and relate the distribution of salinity to the hydrogeologic framework thereby allowing for increased understanding of processes that control this distribution.

The Floridan aquifer system consists primarily of limestone and dolomite of Oligocene and Eocene age. The principal geologic units in the system are the lower part of the Hawthorn Group, Suwannee Limestone, Ocala Limestone, Avon Park Formation, and Oldsmar Formation. A basal portion of the Hawthorn Group, referred to as the basal Hawthorn unit, was defined based on a regionally extensive and correlative marker unit at its top.

The base of the basal Hawthorn unit (basal contact of the Hawthorn Group) usually coincides with the top of the Suwannee Limestone, but also coincides with the top of the Ocala Limestone in the eastern part of the study area; the altitude of this basal surface ranges from about 500 to more than 1,000 ft below sea level. This contact is probably a regionally extensive unconformity that could have formed during a major low stand in sea level occurring at the boundary between early to late Oligocene time. Correlation of this unconformity between southwestern and southeastern Florida in the stratigraphic section indicates that it occurs at the same position as the one mapped on top of rocks of Eocene age in southeastern Florida.

The basal Hawthorn unit ranges from about 120 to 460 ft in thickness in the study area. Its variation in thickness probably relates in most of the study area to the paleotopography prior to its deposition. This paleotopography could have been created by solution and erosion of the underlying limestone. However, in some areas of Lee County where the basal Hawthorn unit is thick, paleotopographic highs formed at the top of the unit due to depositional buildup. A marker bed, which defines the top of the unit, corroborates the depositional origin of these highs. In these high areas, zones of permeable limestone are present in the upper and

middle parts of the basal Hawthorn unit and have characteristic gamma-ray log patterns.

The major hydrogeologic units in southwestern Florida are the surficial aquifer, intermediate aquifer system, and Floridan aquifer system. The surficial aquifer generally is unconfined, and its base is defined by the first occurrence of laterally extensive and vertically persistent beds of much lower permeability. These beds are within the intermediate aquifer system. The Floridan aquifer system is confined by beds of low permeability in the intermediate aquifer system. The Floridan aquifer system consists of the Upper Floridan aquifer, middle confining unit, and Lower Floridan aquifer. This report principally deals with the Upper Floridan aquifer and middle confining unit.

The top of the Upper Floridan aquifer was determined based on head data, zones of lost circulation or returns, and temperature and spontaneous potential logs, which indicate the occurrence of flow zones. Over most of the study area, these data show that the top of the aquifer occurs approximately at the unconformity at the base of the basal Hawthorn unit. However, the lower 10 to 40 ft of the basal Hawthorn unit is often permeable, and if so, is included in the Upper Floridan aquifer. Additionally, where the basal Hawthorn unit is thick, such as in some areas of Lee County, significant flow zones in the Upper Floridan aquifer occur in the middle and upper parts of the unit.

Based on limited measurements of hydraulic conductivity and transmissivity, the base of the Upper Floridan aquifer ranges from about 1,500 to 1,800 ft in depth (giving an approximate range of 700 to 1,200 ft for the thickness of the aquifer). The highest transmissivity value of the Upper Floridan aquifer (33,000 ft²/d) occurs in southwestern Collier County. The transmissivity of the basal Hawthorn unit is related to the thickness of the unit. For example, in the Cape Coral area in west-central Lee County where the unit is thick, the transmissivity of the unit is the highest measured (12,300 ft²/d).

The base of the middle confining unit usually extends down to at least 2,300 ft in the study area; its thickness ranges from 500 to 800 ft, and its hydraulic conductivity is as low as 1 x 10⁻⁵ ft/d. The top of a sequence in the middle confining unit containing thick beds of dolomite and evaporite minerals, referred to as the dolomite-evaporite unit, was mapped. The altitude of the top of this unit, which ranges from about 1,700 to more than 2,500 ft below sea level, is probably an important hydrologic boundary in much of the study

area because of the very low permeability beds in the unit; in areas where the altitude is high, it could mark the base of the Upper Floridan aquifer. Mapping of the top of this unit shows that a prominent feature of higher altitudes is present in central Collier County, which extends to the northwest into north-central Lee County. This feature could have resulted from heavy, localized deposition of gypsum. The top of the unit in this area is as much as 400 to 500 ft higher than in adjacent areas to the east and west in Collier County.

Salinity in the Floridan aquifer system, as defined by chloride and dissolved-solids concentrations, was calculated based on geophysical logs of formation resistivity, porosity, and temperature. Porosity was determined based on sonic and density logs. Relations between sonic log response and density porosity were determined in wells where both logs were run over the same intervals in the Floridan aquifer system below the Hawthorn Group. Calculated values of formation water resistivity were converted to an equivalent chloride concentration based on relations previously derived in southeastern Florida, which are based on analyses of water samples from the Floridan aquifer system. Chloride concentrations were calculated for 21 intervals in 17 wells in which both resistivity and porosity logs were run, and these results were used to help define the distribution of salinity in the Floridan aquifer system. Seven of these intervals had associated water-quality data which could be used for comparisons, and the average difference between the calculated and measured values, expressed as a percent error, was 15 percent. This error is not large in view of the large variation in salinity found in the Floridan aguifer system in the study area.

In much of the study area, the Floridan aquifer system can be divided into three salinity zones. These zones, defined using the threshold salinity values equivalent to dissolved-solids concentrations of 10,000 and 35,000 mg/L are, in order of increasing depth, the brackish-water zone, salinity transition zone, and saline-water zone with the salinity in the saline-water zone similar to that of seawater. These two salinity values equate to chloride concentrations of about 5,240 and 18,900 mg/L, respectively, in the Floridan aquifer system. The base of the brackish-water zone and the top of the saline-water zone were defined in numerous wells in the study area mostly using geophysical logs.

The altitude of the base of the brackish-water zone ranges from 565 ft below sea level along the

coast in Lee County to almost 2,200 ft below sea level far inland in Palm Beach County. The direction of dip and shape of this surface reflect the distribution of hydraulic head in the Upper Floridan aquifer, supporting the interpretation that the salinity transition zone represents a salinity interface, the depth of which is controlled by head in the brackish-water zone.

The base of the brackish-water zone is deeper than expected (as much as 300 ft) in north-central Collier County. The base is as deep as 2,090 ft below sea level, and the salinity transition zone is not present or is poorly defined in this area. The origin of this anomalous area is interpreted to be related to the development of the dolomite-evaporite unit in the middle confining unit of the Floridan aquifer system. The top of this impermeable unit occurs at the base of the brackish-water zone in this area, and the axis of a high area at the top of the unit, which trends to the northwest in Collier and Lee Counties, parallels and lies just to the west of the anomalous area. This high area could be acting as an impermeable sill, preventing saline water from moving in laterally from the coast to the southwest and up from the Boulder zone below in the Lower Floridan aquifer. Locating a Floridan aquifer system well field in or near this anomalous area could be optimal. Increases in salinity with time during withdrawal of ground water from the Upper Floridan aquifer could be minimal because of the thickness of the brackish-water zone, lack of a salinity transition zone, and the occurrence of the impermeable beds at depth.

The salinity transition zone is 150 ft or less in thickness in most of the study area. However, in another area where the base of the brackish-water zone is deeper than expected, the zone apparently is very thick (as much as 500 to 600 ft). The underlying saline-water zone extends to the base of the Floridan aquifer system, and variation of salinity within it is small. The chloride concentration of water samples collected from the completed intervals in the saline-water zone ranged from 17,500 to 20,800 mg/L.

In the brackish-water zone, comparison of analyses of water samples collected from depth intervals above the basal contact of the Hawthorn Group with water samples collected from depth intervals located below this contact indicates that chloride concentration generally does not vary across this contact. The distribution of salinity in the upper part of the brackish-water zone, including the basal Hawthorn unit, was mapped. Chloride concentrations range from

400 to 4,000 mg/L, but range from 800 to 2,000 mg/L in most of the study area. Three large areas contain chloride concentrations less than 800 mg/L; two are in Lee County and one is in eastern Collier County and southeastern Hendry County. Increases in chloride concentration generally were not found in a large area of ground-water withdrawal in Lee County over the last 50 years even though there was drawdown of head.

A large area of relatively low salinity, with chloride concentrations ranging from 500 to 1,200 mg/L, in the upper part of the brackish-water zone in southeastern Lee and north-central Collier Counties coincides with an area of high altitude at the basal contact of the Hawthorn Group. As the altitude of this surface decreases away from this area to the northeast, east, southeast, south, and southwest, salinity increases to a chloride concentration of 2,000 mg/L or more. The increase in salinity to the northeast and east coincides with development of the thick basal Hawthorn unit in central Hendry County, with higher salinity in this zone than in the underlying units. To the southeast in central Collier County, the increase occurs only in the basal Hawthorn unit and Suwannee Limestone, but not in deeper formations. These areas of higher salinity could have resulted from the influx of seawater from the southwest into structurally low areas and into units of higher permeability near the top of the Upper Floridan aquifer. This could have occurred during high sealevel stands, with subsequent lower sea levels and incomplete flushing by the modern freshwater flow system.

Comparison of chloride and sulfate concentrations from water samples obtained from the Floridan aquifer system indicates that most of the sulfate is derived from mixing of dilute ground water with seawater; however, a minor portion of the sulfate in water samples from the brackish-water zone comes from gypsum dissolution. Additionally, the concentration of sulfate was compared to that expected for a particular chloride concentration based on a pure water-seawater mixing line, and this showed that sulfate is depleted in water samples obtained from the salinity transition zone.

The concentration of sulfate in the brackishwater zone ranges from 120 to 900 mg/L in the study area. Areas of higher sulfate concentration coincide with the northwest-trending high area at the top of the dolomite-evaporite unit in the middle confining unit and with areas where gypsum is present in the middle confining unit. This indicates that the higher sulfate concentration present in these areas could result from gypsum dissolution occurring near the base of the brackish-water zone. Upwelling of deeply circulating ground water could explain why this higher sulfate concentration is present in the upper part of the brackish-water zone where gypsum is not thought to be present.

REFERENCES CITED

- Archie, G.E., 1942, The electrical resistivity log as an aid in determining some reservoir characteristics: Journal of Petroleum Technology, v. 5, no. 1.
- Boggess, D.H., 1974, Saline ground-water resources of Lee County, Florida: U.S. Geological Survey Open-File Report 74-247, 62 p.
- Boggess, D.H., Missimer, T.M., and O'Donnell, T.H., 1981, Hydrogeologic sections through Lee County and adjacent areas of Hendry and Collier Counties, Florida: U.S. Geological Survey Water-Resources Investigations Open-File Report 81-638, 7 p.
- Brown, Eugene, Skougstad, M.W., and Fishman, M.J., 1970, Methods for collection and analysis of water samples for dissolved minerals and gases: U.S. Geological Survey Techniques of Water Resources Investigations, book 5, chap. A1, 160 p.
- Bush, P.W., and Johnston, R.H., 1988, Ground-water hydraulics, regional flow, and ground-water development of the Floridan aquifer system in Florida and in parts of Georgia, South Carolina, and Alabama: U.S. Geological Survey Professional Paper 1403-C, 80 p., 17 pls.
- Chen, C.S., 1965, The regional lithostratigraphic analysis of Paleocene and Eocene rocks of Florida: Florida Geological Survey Bulletin 45, 105 p.
- Cunningham, K.J., McNeill, D.F., Guertin, L.A., and others, 1998, New Tertiary stratigraphy for the Florida Keys and southern peninsula of Florida: Geological Society of America Bulletin, v. 110, p. 231-258.
- Cunningham, K.J., and Rupert, F.R., 1996, A new guide fossil (*Miogypsina sp.*) for the lower to middle Arcadia Formation in the Florida Keys: Miami Geological Society, Short Contributions to Florida Geology no. 8, 2 p.
- Fetter, C.W., 1988, Applied hydrogeology (2d ed.): Columbia, Merrill Publishing Company, 592 p.
- Florida Department of Environmental Regulation, 1982, Underground injection control: Chapter 17-28 in Florida Administrative Code.
- Geraghty and Miller, Inc., 1986, Construction and testing of the injection and monitor wells at the Gasparilla Island Water Association wastewater treatment plant: Boca Grande, Florida, 28 p.

- Green, R.C., Campbell, K.M., and Scott, T.M., 1990, Core drilling project: Lee, Hendry and Collier Counties: Florida Geological Survey Open-File Report 37, 44 p.
- Haq, B.U., Hardenbol, J., and Vail, P.R. 1988, Mesozoic and Cenozoic chronostratigraphy and cycles of sea-level change; *in* C.K. Wilgus and others, eds., Sea-Level Changes—An Integrated Approach: SEPM Special Publication 42, p. 72-108.
- Hem, J.D., 1985, Study and interpretation of the chemical characteristics of natural water, 3rd ed.: U.S. Geological Survey Water-Supply Paper 2254, 263 p.
- Katz, B.G., 1992, Hydrogeochemistry of the Upper Floridan aquifer, Florida: U.S. Geological Survey Water-Resources Investigations Report 91-4196, 37 p., 10 pls.
- Knapp, M.S., Burns, W.S., and Sharp, T.S., 1986, Preliminary assessment of the ground water resources of western Collier County, Florida: South Florida Water Management District Technical Publication 86-1, pts. 1 and 2, 142 p.
- Kohout, F.A., 1965, A hypothesis concerning cyclic flow of salt water related to geothermal heating in the Floridan aquifer: New York Academy of Sciences Transactions, ser. 2, v. 28, no. 2, p. 249-271.
- Kwader, Thomas, 1986, The use of geophysical logs for determining formation water quality: Ground Water, v. 24, no. 1, p. 11-15.
- Marella, R.L., 1999, Water withdrawals, use, discharge, and trends in Florida, 1995: U.S. Geological Survey Water-Resources Investigations Report 99-4002, 90 p.
- MacCary, L.M., 1983, Geophysical logging in carbonate aquifers: Ground Water, v. 21, no. 3, p. 334-342.
- Meyer, F.W., 1974, Evaluation of hydraulic characteristics of a deep artesian aquifer from natural water-level fluctuations, Miami, Florida: Florida Bureau of Geology Report of Investigations 75, 32 p.
- ———1989, Hydrogeology, ground-water movement, and subsurface storage in the Floridan aquifer system in southern Florida: U.S. Geological Survey Professional Paper 1403-G, 59 p.
- Miller, J.A., 1986, Hydrogeologic framework of the Floridan aquifer system in Florida, and in parts of Georgia, Alabama, and South Carolina: U.S. Geological Survey Professional Paper 1403-B, 91 p.
- Missimer and Associates, 1991a, Phase I Deep aquifer hydrogeologic study, Collier County, Florida: Report prepared for Collier County Utilities Division, Water and Wastewater Services, April 1991, 61 p.
- ——— 1991b, Hydrogeology and hydraulic solute transport modeling of the upper Floridan aquifer system beneath Cape Coral, Florida: City of Cape Coral master water supply plan phase II report, January 1991, pts. I, II, and III, 131 p.
- Nordstrom, D.K., Plummer, L.N., Wigley, T.M.L., and others, 1979, A comparison of computerized chemical models for equilibrium calculations in aqueous

- systems; *in* E.A. Jenne, ed., Chemical Modeling in Aqueous Systems: Speciation, Sorption, Solubility, and Kinetics: Washington, D.C., American Chemical Society Symposium Series 93, p. 857-892.
- Parker, G.G., Ferguson, G.E., Love, S.K., and others, 1955, Water resources of southeastern Florida: U.S. Geological Survey Water-Supply Paper 1255, 965 p.
- Peacock, Roland, 1983, The post Eocene stratigraphy of southern Collier County, Florida: South Florida Water Management District Technical Publication 83-5, 42 p. and appendixes.
- Post, Buckley, Schuh & Jernigan, Inc., 1988, Deep test/injection well engineering report: North Fort Myers Utility, Inc., April 1988.
- ————1992, Deep test/injection well engineering report, Zemel Road landfill, Charlotte County, Florida: Prepared for Charlotte County Solid Waste Authority, p. 1-1 to 9-17.
- Puri, H.S., and Winston, G.O., 1974, Geologic framework of high transmissivity zones in south Florida: Florida Bureau of Geology Special Publication 20, 101 p.
- Reese, R.S., 1994, Hydrogeology and the distribution and origin of salinity in the Floridan aquifer system, south-eastern Florida: U.S. Geological Survey Water-Resources Investigations Report 94-4010, 56 p.
- Reese, R.S., and Memberg, S.J., 1999 (in press), Hydrogeology and the distribution of salinity in the Floridan aquifer system, Palm Beach County, Florida: U.S. Geological Survey Water-Resources Investigations Report 99-4061.
- Rightmire, C.T., Pearson, F.J., Jr., Back, William, and others, 1974, Distribution of sulfur isotopes of sulfates in groundwaters from the principal artesian aquifer of Florida and the Edwards aquifer of Texas, U.S.A.; *in* Isotope Techniques in Groundwater Hydrology: Vienna, Austria, International Atomic Energy Agency, v. 2, p. 191-207.
- Sacks, L.A., and Tihansky, A.B., 1996, Geochemical and isotopic composition of ground water, with emphasis on sources of sulfate, in the Upper Floridan aquifer and intermediate aquifer system in southwest Florida: U.S. Geological Survey Water-Resources Investigations Report 96-4146, 67 p.
- Schlumberger Educational Services, 1972, Log interpretation, volume I principles: New York, Schlumberger Ltd., 113 p.
- ———1987, Log interpretations principles/applications: USA, 198 p.
- ————1988, Log interpretation charts, 1989: USA, 151 p.
- Scott, T.M., 1988, The lithostratigraphy of the Hawthorn Group (Miocene) of Florida: Florida Geological Survey Bulletin 59, 147 p.

- Singh, W.P., Eichler, G.E., Sproul, C.R., and Garcia-Bengochea, J.I., 1983, Pump testing Boulder zone aquifer, south Florida: Journal of Hydraulic Engineering, v. 9, no. 8, p. 1152-1160.
- Smith, C.A., Lidz, Lauralee, and Meyer, F.W., 1982, Data on selected deep wells in south Florida: U.S. Geological Survey Open-File Report 82-348, 144 p.
- Smith, K.R., and Adams, K.M., 1988, Ground water resource assessment of Hendry County, Florida: South Florida Water Management District Technical Publication 88-12, pts. 1 and 2, 109 p.
- Southeastern Geological Society Ad Hoc Committee on Florida Hydrostratigraphic Unit Definition, 1986, Hydrogeological units of Florida: Florida Department of Natural Resources, Bureau of Geology, Special Publication 28, 9 p.
- Sprinkle, C.L., 1989, Geochemistry of the Floridan aquifer system in Florida and in parts of Georgia, South Carolina, and Alabama: U.S. Geological Survey Professional Paper 1403-I, 105 p., 9 pls.
- Sproul, C.R., Boggess, D.H., and Woodard, H.J., 1972, Saline water intrusion from deep artesian sources in the McGregor Isles area of Lee County, Florida: Florida Bureau of Geology Information Circular 75, 30 p.

- ViroGroup, Inc./Missimer Division, 1993, North County Regional Water Treatment Plant injection well system completion report: Collier County Utilities Division Water and Wastewater Services, v. 1 and 2, 55 p., 1 pl.
- Wedderburn, L.A., Knapp, M.S., Waltz, D.P., and Burns, W.S., 1982, Hydrogeologic reconnaissance of Lee County, Florida: South Florida Water Management District Technical Publication 82-1, pts. 1, 2, and 3, 192 p.
- Wingard, G.L., Weedman, S.D., Scott, T.M., and others, 1994, Preliminary analysis of integrated stratigraphic data from the south Venice corehole in Sarasota County, Florida: U.S. Geological Survey Open-File Report 95-3, 129 p.
- Winston, G.O., 1993, A regional analysis of the Oligocene-Eocene section of the peninsula using vertical lithologic stacks: The Paleogene of Florida volume 2: Miami Geological Society, 33 p.
- ———1995, Evidence for interfingering of Suwannee, Ocala, and Avon Park lithologies in northeastern Hendry County, Florida: Miami Geological Society, Short Contributions to Florida Geology no. 7, 2 p.
- ———1996, The Boulder zone dolomites of Florida, volume 2: Paleogene zones of the southwestern peninsula: Miami Geological Society, 64 p.

Appendix I Inventory of Wells Used in this Report

[Well locations are shown in figures 2 and 3. County designations: C, Collier; CH, Charlotte, G, Dade or Broward; GL, Glades; HE, Hendry; L, Lee; MO, Monroe; PB, Palm Beach, and S, Dade. Well and casing depths are from measuring point, which is at land surface or above. Dashes indicate no data]

| Diameter Date at end of casing of con- (inches) struction | 4.5 1941 | | 4.5 1941 | 03 | | | | | | | | | | | |
|---|------------------|-----------------|------------------|----------------------|--------------------------------|---|--|--|---|--|---|---|---|---|--|
| casing of casin (feet) (inches | 166 4.5 | | 228 4.5 | 28 91 07 59 | 11 2 | 1 2 | 1 | 1 | 2 1 | | 1 2 2 | | | | |
| Well depth (feet) | 995 | 845 | | 11,900 | 11,900 | 11,900 875 783 | 11,900 875 783 1,119 | 875 783 1,119 | 11,900 875 783 1,119 700 4,400 | 875 875 1,119 700 4,400 | 11,900 875 783 1,119 700 4,400 | 11,900 875 783 1,119 700 4,400 915 900 1,000 | 875 875 1,119 4,400 900 1,000 | 11,900 875 783 1,119 700 4,400 1,000 11,626 | 875 875 783 1,119 700 4,400 1,000 11,626 11,626 |
| point (feet) | 36 | 40 | | 37 | 37 | 37 | 37 17 35 40 | 37 17 37 40 40 15 | 37 17 17 15 15 38 | 37 37 38 38 38 | 37 17 17 18 88 38 18 19 19 19 19 19 19 19 19 19 19 19 19 19 | 37 17 17 18 38 38 18 11 12 | 37 17 17 18 38 38 17 17 17 17 | 37 15 16 17 17 18 38 38 38 38 31 31 31 31 31 31 31 31 31 31 31 31 31 | 37 38 38 31 31 37 |
| Land-net location | S04 T46S R29E | S33 T46S R29E | | S03 T48S R28E | S03 T48S R28E S13 T48S R27E | S03 T48S R28E S13 T48S R27E S03 T47S R29E | S03 T48S R28E S13 T48S R27E S03 T47S R29E S07 T46S R29E | S03 T48S R28E S13 T48S R27E S03 T47S R29E S07 T46S R29E S01 T50S R30E | S03 T48S R28E S13 T48S R27E S03 T47S R29E S07 T46S R29E S01 T50S R30E | S03 T48S R28E S13 T48S R27E S03 T47S R29E S07 T46S R29E S01 T50S R30E S04 T46S R29E | S03 T48S R28E S13 T48S R27E S03 T47S R29E S07 T46S R29E S01 T50S R30E S04 T46S R29E S32 T52S R30E S32 T52S R30E | S03 T48S R28E S13 T48S R27E S03 T47S R29E S07 T46S R29E S01 T50S R30E S04 T46S R29E S05 T52S R30E S05 T50S R29E S05 T50S R29E | S03 T48S R28E S13 T48S R27E S03 T47S R29E S07 T46S R29E S01 T50S R30E S04 T46S R29E S05 T52S R30E S05 T50S R29E S05 T50S R29E S05 T50S R29E | S03 T48S R28E S13 T48S R27E S03 T47S R29E S07 T46S R29E S01 T50S R30E S32 T52S R30E S05 T50S R29E S05 T50S R29E S05 T50S R29E S05 T50S R28E S06 T50S R28E | S03 T48S R28E S13 T48S R27E S03 T47S R29E S07 T46S R29E S07 T46S R29E S04 T46S R29E S05 T50S R30E S05 T50S R29E S05 T50S R29E S05 T50S R28E S05 T50S R28E S29 T48S R30E S29 T48S R30E |
| (degrees) | 0812607 | 0812601 | | 0813044 | 0813044 | 0813044 0812306 0812459 | 0813044 0812306 0812459 0812724 | 0813044 0812306 0812459 0812724 0811559 | 0813044 0812306 0812459 0812724 0811559 | 0813044 0812306 0812459 0812724 0811559 0812523 | 0813044 0812306 0812459 0812724 0811559 0812523 0812528 | 0813044 0812306 0812459 0812724 0811559 0812523 0812528 0812528 | 0813044 0812306 0812459 0812724 0812523 0812528 0812528 0812528 | 0813044 0812306 0812459 0812724 0812523 0812528 0812528 0813337 | 0813044 0812306 0812459 0812724 0812523 0812528 0812528 0812528 0813337 0813334 |
| (degrees) | 263020 | 262557 | 262006 | | 261756 | 261756 | 261756 262504 262926 | 261756 262504 262926 260919 | 262504 262926 260919 263041 | 261756 262504 262926 260919 263041 255403 | 261756 262504 262926 260919 263041 255403 | 261756 262504 262926 260919 263041 255403 260910 | 262504 262926 262926 260919 263041 255403 260910 260908 | 262504 262926 262926 260919 255403 260910 260908 260908 | 261756 262504 262926 260919 263041 255403 260908 260908 261606 262211 |
| Jaguin | 263020081260701 | 252557080254601 | 262006081304401 | | 261756081340601 | 261756081340601 262505081245301 | 261756081340601 262505081245301 262926081272401 | 262505081340601 262505081245301 262926081272401 260919081155901 | 261756081340601 262505081245301 262926081272401 260919081155901 263041081252301 | 261756081340601 262505081245301 262926081272401 260919081155901 263041081252301 255403081200901 | 261756081340601 262505081245301 262926081272401 260919081155901 263041081252301 255403081200901 260910081252801 | 261756081340601 262505081245301 262926081272401 260919081155901 263041081252301 255403081200901 260910081252801 26090081331701 | 261756081340601 262505081245301 262926081272401 260919081155901 263041081252301 255403081200901 260910081252801 260908081331701 261606081202401 | 261756081340601 262505081245301 262926081272401 260919081155901 253403081252301 255403081252801 260908081331701 261606081202401 262211081333401 | 261756081340601 262505081245301 262926081272401 260919081155901 263041081252301 255403081252801 260910081252801 260908081331701 261606081202401 262211081333401 |
| or owner | S-482 | S-483 | W-1885, P-98 | | 617-134-1 | 617-134-1 | 617-134-1 625-124-2 629-127-4 | 617-134-1 625-124-2 629-127-4 609-115-1 | 617-134-1 625-124-2 629-127-4 609-115-1 P-319 | 617-134-1 625-124-2 629-127-4 609-115-1 P-319 | 617-134-1 625-124-2 629-127-4 609-115-1 P-319 Wooten C-2024D, W-14918 | 617-134-1 625-124-2 629-127-4 609-115-1 P-319 Wooten C-2024D, W-14918 C-2022D, W-14601 | 617-134-1 625-124-2 629-127-4 609-115-1 P-319 Wooten C-2024D, W-14918 C-2022D, W-14601 | 617-134-1 625-124-2 629-127-4 609-115-1 P-319 Wooten C-2024D, W-14918 C-2022D, W-14601 W-820, P-42 | 617-134-1 625-124-2 629-127-4 609-115-1 P-319 Wooten C-2024D, W-14918 C-2022D, W-14601 W-820, P-42 W-2103, P-103 |
| well | C-21 | C-22 | C-234 | | C-236 | C-236 C-258 | C-236 C-258 C-284 | C-236 C-258 C-284 C-308 | C-236 C-258 C-284 C-308 | C-236 C-258 C-284 C-308 C-415 | C-236 C-258 C-284 C-308 C-415 C-411 | C-236 C-258 C-284 C-308 C-415 C-411 C-679 C-680 | C-236 C-258 C-284 C-308 C-415 C-411 C-679 C-679 C-670 | C-236 C-258 C-284 C-308 C-415 C-679 C-680 | C-236 C-258 C-284 C-308 C-415 C-411 C-679 C-679 C-701 |

| Date at end of con- struction | 1948 | 01-19-47 | 08-25-51 | 06-08-55 | 01-27-61 | 1965 | 03-18-69 | 10-31-65 | 07-28-73 | 07-24-71 | 01-12-74 | ; | 1 | 1 | 01-77 | 1 | - | | ſ | 1 | ; |
|--|----------------------|----------------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| Diameter of casing (inches) | 20.0 13.4 9.6 | 20.0 13.4 9.6 | 13.4 9.6 | 13.4 | 13.4 | 9.6 | 9.6 | 13.4 | 9.6 | 9.6 | 20.0 | ; | 1 | ł | 7.0 | 1 | 1 | 4.0 | 1 | 1 | 1 |
| of casing (feet) | 48 1,111 5,111 | 63 1,013 5,595 | 1,025 4,492 | 1,434 | 1,351 4,302 | 3,696 11,700 | 3,833 | 1,140 | 3,660 | 3,676 | 241 4,213 | ł | ł | ł | 2,004 | ł | ł | 301 | ł | 1 | 1 |
| Well depth (feet) | 12,206 | 11,590 | 12,516 | 11,938 | 12,961 | 14,504 | 11,987 | 11,497 | 12,701 | 12,049 | 13,004 | 18,670 | 11,658 | 11,880 | 2,500 | 11,608 | 2,056 | 593 | 1,205 | 1,234 | 798 |
| Altitude of measuring point (feet) | 32 | 35 | 25 | 45 | 35 | 35.6 | 40 | 53.4 | 20.6 | 40 | 46.1 | 29 | 38 | 39 | 21 | 35 | 18 | 33 | 15 | 1 | : |
| Land-net location | S23 T48S R28E | S24 T48S R29E | S27 T50S R26E | S08 T47S R29E | S18 T49S R31E | S24 T48S R29E | S09 T47S R28E | S05 T46S R29E | S24 T51S R26E | S16 T46S R28E | S23 T46S R30E | S12 T52S R27E | S33 T51S R34E | S34 T49S R31E | S34 T48S R30E | S03 T49S R30E | S24 T48S R29E | S12 T46S R29E | S12 T46S R29E | ı | ; |
| Longitude (degrees) | 0812934 | 0812218 | 0814149 | 0812641 | 0811525 | 0812211 | 0813116 | 0812618 | 0813928 | 0813106 | 0811801 | 0813329 | 0805532 | 0811226 | 0811812 | 0811816 | 0812227 | 0812240 | 0811853 | 0812808 | 0814252 |
| Latitude (degrees) | 261723 | 261704 | 260518 | 262422 | 261313 | 261724 | 262403 | 263043 | 260055 | 262848 | 262802 | 255731 | 255856 | 261011 | 261531 | 261452 | 261716 | 262930 | 260916 | 255623 | 255857 |
| Site identification number | 261723081293401 | 261704081221801 | 260518081414901 | 262422081264101 | 261313081152501 | 261724081221101 | 262403081311601 | 263043081261801 | 260055081392801 | 262848081310601 | 262759081180101 | 255731081332901 | 255856080553201 | 261011081122601 | 261531081181201 | 261452081181601 | 261716081222701 | 262930081224001 | 260916081185301 | 255623081280801 | 255857081425201 |
| Other well identifier or owner | W-1820, P-64 | P-38 | W-2420, P-130 | W-3579, P-222 | P-291 | P-345 | P-401 | P-352 | P-663 | P-477 | P-697 | P-778 | P-829 | P-799 | P-856 | P-801 | W-10252 | Alico, Inc. | W-14919 | W-14920 | W-14921 |
| Local well number | C-712 | C-719 | C-726 | C-727 | C-729 | C-739 | C-742 | C-753 | C-759 | C-764 | C-781 | C-794 | C-802 | C-808 | C-820 | C-823 | C-851 | C-876 | C-913 | C-914 | C-015 |

| Other well identifier Site ic or owner | Site ic | Site identification number | Latitude (degrees) | Longitude (degrees) | Land-net location | Altitude of measuring point (feet) | Well depth (feet) | Bottom of casing (feet) | Diameter of casing (inches) | Date at end of construction |
|---|---------|-------------------------------|-----------------------|------------------------|-------------------|--|-------------------------|--------------------------------------|--------------------------------------|-----------------------------|
| CO-2081 260952081410701 260 | | 260 | 260952 | 0814107 | ł | 10 | 1,616 | 315 540 | 12.0 | 01-01-91 |
| CO-2271, MARCO-II 255733081432601 255733 | | 25573 | 33 | 0814326 | T52S R26E | 6.3 | 3,354 | 230 400 910 2,573 2,640 | 44.0 39.0 34.0 20.0 24.0 | 02-07-92 |
| CO-2272, MARCO-M1 255732081432701 255732 | 01 | 2557 | 732 | 0814327 | T52S R26E | 6.2 | 1,600 | 395 1,000 1,490 | 24.0 16.0 6.6 | 03-30-92 |
| CO-2305 255625081424201 2556 | | 255 | 255625 | 0814242 | T52S R26E | ĸ | 810 | 45 405 | 18.0 | 1992 |
| CO-2317, NCRWTP-II, 261444081404701 261444 W-16884 | | 261 | 44 4 | 0814047 | SE S35 T48S R26E | 41 | 3,380 | 16 425 1,310 2,445 2,497 | 48.0 38.0 30.0 16.0 20.0 | 10-31-92 |
| CO-2318, NCRWTP-M1 261444081404601 261444 | | 2614 | 4 | 0814046 | SE S35 T48S R26E | 14 | 1,930 | 420 900 1,815 | 24.0 16.0 6.6 | 10-14-92 |
| WA-483 262906081241201 262906 | | 2629 | 900 | 0812412 | S10 T46S R29E | 1 | 829 | 304 | 0.9 | 1 |
| 175-TWB 261012081435101 261012 | 01 | 261(| 012 | 0814351 | SW S29 T49S R26E | 10 | 2,694 | 490 905 | 12.0 | 12-14-94 |
| IWSD-TW 262448081255401 262 | | 262 | 262448 | 0812554 | SW S04 T47S R29E | 27 | 2,354 | 780 | 18.0 | 01-25-96 01-25-96 |
| P-1042 261728081205101 261 | 01 | 261 | 261728 | 0812051 | NW S20 T48S R30E | 46.6 | 12,640 | 1,508 | 16.0 | 1 |
| P-1057 261858081215701 262 | 01 | 262 | 262858 | 0812157 | SW S18 T46S R30E | 49.8 | 11,561 | 115 220 1,545 3,853 | 30.0 20.0 13.4 9.6 | 12-22-81 |
| P-1060 261426081171901 26 | | 26 | 261426 | 0811719 | SE S02 T49S R30E | 41.9 | 11,725 | 250 1,840 4,000 11,725 | 20.0 13.4 9.6 7.0 | 05-22-83 |

| P-1063 260603081024601 260603 0810246 SW S20 T50S R33E 36 11,759 P-1065 260947081100202 260947 0811002 NW S06 T50S R32E 39.8 11,802 P-1086 255255080545901 255255 0805459 NW S10 T53S R34E 32 11,606 P-1094 260652081060101 260652 0810601 SW S14 T50S R32E 38.2 11,505 P-1127 260341081040301 260841 0812508 SE S28 T475 R29E 45.5 11,507 P-1137 262130081250801 262249 0812508 SE S28 T475 R29E 45.5 11,730 P-1134 262249081264001 262249 0812640 NW S33 T46S R28E 44.9 11,720 P-1116 26205081314601 262605 0813146 NW S33 T46S R28E 44.9 11,755 P-1216 260723081040001 260723 0810400 NW S18 T50S R33E 37.5 11,755 LE00017 264745082021201 264745 0820212 T42S R23E 26 27110 | Local well number | Other well identifier or owner | Site identification number | Latitude (degrees) | Longitude (degrees) | Land-net location | Altitude of measuring point (feet) | Well depth (feet) | Bottom of casing (feet) | Diameter of casing (inches) | Date at end of construction |
|---|-------------------------|-----------------------------------|-------------------------------|-----------------------|------------------------|-------------------|--|-------------------------|----------------------------------|-----------------------------------|-----------------------------|
| P-1065 260947081100202 260947 0811002 NW S06 T50S R32E 39.8 11,802 P-1086 255255080545901 255255 0805459 NW S10 T53S R34E 32 11,680 P-1094 260652081060101 260652 0810601 SW S14 T50S R32E 38.2 11,505 P-1095 260841081040301 260841 0810403 SW S06 T50S R33E 35.8 11,790 P-1137 262130081250801 262130 0812508 SE S28 T47S R29E 45.5 11,987 P-1134 262249081264001 262249 0812640 NW S33 T46S R28E 44.9 11,720 P-1199 26205081314601 262249 0810400 NW S18 T50S R33E 37.5 11,730 LE00017 264745082021201 264745 0820212 T442S R23E 11 1,077 ZRL-II, W-16889 264729081573301 264725 0815733 SE S25 T42S R23E 26.710 | 125 | P-1063 | 260603081024601 | 260603 | 0810246 | SW S20 T50S R33E | 36 | 11,759 | 225 1,570 3,813 | 20.0 13.4 9.6 | 07-01-82 |
| P-1086 255255080545901 255255 0805459 NW SIO T53S R34E 32 11,680 P-1094 260652081060101 260652 0810601 SW SI4 T50S R32E 38.2 11,505 P-1095 260841081040301 260841 0810403 SW S06 T50S R33E 35.8 11,790 P-1127 262130081250801 262130 0812640 NW S20 T47S R29E 46.7 3,934 P-1134 262249081264001 262249 0812640 NW S33 T46S R28E 44.9 11,720 P-11199 262605081314601 262605 0813146 NW S33 T46S R28E 44.9 11,720 P-1216 260723081040001 260723 0810400 NW S18 T50S R33E 37.5 11,755 LE00017 264745082021201 264745 0820212 T42S R23E 26 2.710 | 126 | P-1065 | 260947081100202 | 260947 | 0811002 | NW S06 T50S R32E | 39.8 | 11,802 | 250 1,565 3,696 | 20.0 13.4 9.6 | 02-22-83 |
| P-1094 260652081060101 260652 0810601 SW S14 T50S R32E 38.2 11,505 P-1095 260841081040301 260841 0810403 SW S06 T50S R33E 35.8 11,790 P-1127 262130081250801 262130 0812508 SE S28 T47S R29E 45.5 11,987 P-1134 262249081264001 262249 0812640 NW S20 T47S R29E 46.7 3,934 P-1199 262605081314601 262605 0813146 NW S33 T46S R28E 44.9 11,720 P-1216 260723081040001 260723 0810400 NW S18 T50S R33E 37.5 11,755 LE00017 264745082021201 264745 0820212 T42S R23E 11 1,077 ZRL-II, W-16889 264729081575301 264729 0815753 SE S25 T42S R23E 26 2,710 | C-1127 | P-1086 | 255255080545901 | 255255 | 0805459 | NW S10 T53S R34E | 32 | 11,680 | 222 2,065 4,062 | 20 13.4 9.6 | 09-04-85 |
| P-1095 260841081040301 260841 0810403 SW S06 T50S R33E 35.8 11,790 P-1127 262130081250801 262130 0812508 SE S28 T47S R29E 45.5 11,987 P-1134 262249081264001 262249 0812640 NW S20 T47S R29E 46.7 3,934 P-1199 2622605081314601 2622605 0813146 NW S33 T46S R28E 44.9 11,720 P-1216 260723081040001 260723 0810400 NW S18 T50S R33E 37.5 11,755 LE00017 264745082021201 264745 0820212 T42S R23E 11 1,077 ZRL-II, W-16889 264729081575301 264729 0815753 SE S25 T42S R23E 26 2,710 | C-1128 | P-1094 | 260652081060101 | 260652 | 0810601 | SW S14 T50S R32E | 38.2 | 11,505 | 248 1,997 3,750 11,505 | 20.0 13.4 9.6 7.0 | 10-30-83 |
| 262130081250801 262130 0812508 SE S28 T47S R29E 45.5 11,987 262249081264001 262249 0812640 NW S20 T47S R29E 46.7 3,934 2622605081314601 262605 0813146 NW S33 T46S R28E 44.9 11,720 260723081040001 260723 0810400 NW S18 T50S R33E 37.5 11,755 264745082021201 264745 0820212 T42S R23E 11 1,077 264729081575301 264729 0815753 SE S25 T42S R23E 26 2,710 | C-1129 | P-1095 | 260841081040301 | 260841 | 0810403 | SW S06 T50S R33E | 35.8 | 11,790 | 230 1,570 3,945 | 20.0 13.4 9.6 | 03-06-83 |
| P-1134 262249081264001 262249 0812640 NW S20 T47S R29E 46.7 3,934 P-1199 262605081314601 262605 0813146 NW S33 T46S R28E 44.9 11,720 P-1216 260723081040001 260723 0810400 NW S18 T50S R33E 37.5 11,755 LE00017 264745082021201 264745 0820212 T42S R23E 11 1,077 ZRL-II, W-16889 264729081575301 264729 0815753 SE S25 T42S R23E 26 2,710 | 130 | P-1127 | 262130081250801 | 262130 | 0812508 | SE S28 T47S R29E | 45.5 | 11,987 | 246 1,842 3,737 | 20.0 13.4 9.6 | 02-02-84 |
| P-1199 262605081314601 262605 0813146 NW S33 T46S R28E 44.9 11,720 P-1216 260723081040001 260723 0810400 NW S18 T50S R33E 37.5 11,755 LE00017 264745082021201 264745 0820212 T42S R23E 11 1,077 ZRL-II, W-16889 264729081575301 264729 0815753 SE S25 T42S R23E 26 2,710 | 131 | P-1134 | 262249081264001 | 262249 | 0812640 | NW S20 T47S R29E | 46.7 | 3,934 | 281 1,935 3,934 | 20.0 13.4 9.6 | 06-04-84 |
| P-1216 260723081040001 260723 0810400 NW S18 T50S R33E 37.5 11,755 LE00017 264745082021201 264745 0820212 T42S R23E 11 1,077 ZRL-II, W-16889 264729081575301 264729 0815753 SE S25 T42S R23E 26 2,710 | 132 | P-1199 | 262605081314601 | 262605 | 0813146 | NW S33 T46S R28E | 44.9 | 11,720 | 226 1,851 4,060 11,709 | 20.0 13.4 9.6 7.0 | 04-29-86 |
| LE00017 264745082021201 264745 0820212 T42S R23E 11 1,077 ZRL-11, W-16889 264729081575301 264729 0815753 SE S25 T42S R23E 26 2,710 | 133 | P-1216 | 260723081040001 | 260723 | 0810400 | NW S18 T50S R33E | 37.5 | 11,755 | 229 3,995 | 20.0 | 05-23-88 |
| ZRL-II, W-16889 264729081575301 264729 0815753 SE S25 T42S R23E 26 2,710 | 312 | LE00017 | | 264745 | 0820212 | T42S R23E | 11 | 1,077 | 1 | I | 07-28-82 |
| | 313 | ZRL-11, W-16889 | 264729081575301 | 264729 | 0815753 | SE S25 T428 R23E | 26 | 2,710 | 73 427 1,566 2,486 | 38.0 30.0 24.0 12.0 | 06-13-92 |

| Other well identifier or owner | Site identification number | Latitude (degrees) | Longitude (degrees) | Land-net location | Altitude of measuring point (feet) | Well depth (feet) | Bottom of casing (feet) | Diameter of casing (inches) | Date at end of construction |
|-----------------------------------|-------------------------------|-----------------------|------------------------|-------------------|--|-------------------------|--|---|-----------------------------|
| | 264729081575401 | 264729 | 0815754 | SE S25 T42S R23E | 26 | 1,854 | 425 1,340 1,795 | 22.0 16.0 8.0 | 06-24-92 |
| | 261016080492601 | 261016 | 0804926 | S03 T50S R35E | 17.5 | 2,811 | 20 195 834 895 1,104 1,648 2,447 | 35.0 24.0 2.9 16.0 1.0 1.0 2.38 | 11-07-80 04-22-87 |
| Monitor tube in G-2296 | 5 261016080492602 | 261016 | 0804926 | ; | 17.8 | 1,728 | 1,648 | 1.0 | 03-16-87 |
| Same as above | 261016080492603 | 261016 | 0804926 | ı | 17.8 | 1,164 | 1,104 | 1.0 | 03-16-87 |
| Same as above | 261016080492604 | 261016 | 0804926 | 1 | 17.8 | 1,052 | 895 | 7.9 | 03-16-87 |
| P-167, W-3054 | 254540080494301 | 254540 | 0804945 | S16 T54S R35E | 24 | 11,558 | 64 90 649 3,526 11,557 | 20.0 2.9 13.4 9.6 7.0 | 02-01-54 |
| W-2912, P-152 | 264727080593701 | 264727 | 0805937 | S25 T42S R33E | 25 | 13,408 | 3,464 | 13.4 | 07-10-53 |
| | 264415081025401 | 264415 | 0810254 | S20 T43S R33E | 21 | 1,039 | 949 | 6.0 | 1 1 |
| Hendry Cattle | 264325081074601 | 264325 | 0810746 | S22 T43S R32E | 22 | 1,465 | 1 | 6.0 | 1 |
| HE-538 | 263852081260701 | 263852 | 0812607 | S16 T44S R29E | 28 | 1,300 | ł | 0.9 | 1949 |
| Denaud Cemetary | 264521081305301 | 264521 | 0813053 | S10 T43S R28E | 13 | 750 | 540 | 0.9 | 1945 |
| | 264235081315901 | 264235 | 0813159 | S28 T43S R20E | 18 | 700 | 1 | 6.0 | 1 |
| FGS-42 | 263825081334001 | 263825 | 0813340 | S19 T44S R28E | 26 | 790 | 1 1 | 6.0 | 07-53 |
| W-1995 | 263359081073901 | 263359 | 0810739 | S16 T45S R32E | 29 | 1,049 | 1,049 | 8.4 | 08-49 |
| W-2631, P-133 | 262328081114701 | 262328 | 0811147 | S14 T47S R31E | 39.6 | 11,796 | 110 1,409 4,328 | 20.0 13.4 9.6 | 02-03-52 |
| FGS-35 | 263604081263401 | 263604 | 0812634 | S05 T45S T29E | 31 | 792 | 277 | 6.0 | 03-57 |

| Date at end of construction | 1 | 12-20-70 | 1 | | 1 | 1 | 05-72 | 1 1 | 09-72 | 1972 | 1965 | 1 | 1 | 1964 | + | 1974 | 1 | 03-13-75 | 02-13-75 | 1975 | 04-73 | | 1 | 92-80 | 12-76 | 01-25-77 | 1 |
|--|-----------------|-----------------|-----------------|-----------------|------------------|------------------|-----------------|-----------------|-------------------|------------------|--------------------|------------------|-----------------|------------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| | | 12- | | | | | Ö | | 0 | | | | | | | _ | | 03- | 02- | 1 | 0 | | | õ | 1. | 01- | _ |
| Diameter of casing (inches) | 8.0 | 4.0 | 0.9 | 1 | 5.0 | 0.9 | 4.0 | 5.0 | 0.9 | 4.0 | 0.9 | 5.0 | : | 4.0 | 5.0 | 0.9 | 0.9 | 0.9 | 8.0 | 8.0 | 18.0 | 1 | : | 4.0 | 6.0 | 4.0 | - |
| Bottom of casing (feet) | 170 | 589 | 200 | 1 | 80 | 126 | 294 | 322 | 740 | 382 | 141 | 126 | 1 | 190 | 315 | 700 | 240 | 325 | 1 | 610 | 125 625 | 1 | 1 | ł | 470 | 385 | |
| Well depth (feet) | 1,015 | 740 | 700 | 1,100 | 814 | 857 | 608 | 928 | 950 | 673 | 006 | 996 | 744 | 029 | 788 | 968 | 685 | 668 | 1,450 | 750 | 850 | 616 | 029 | 750 | 855 | 999 | 007 |
| Altitude of measuring point (feet) | 5 | 12 | 5 | 20 | 1 | 19 | 12 | 15 | 4 | 5 | 4 | 26 | 5 | 15 | 1 | 3 | 9 | 30 | 31 | ∞ | 7 | ; | 1 | 20 | 5 | 9 | 0,1 |
| Land-net location | S17 T46S R25E | S23 T45S R24E | S24 T46S R22E | S09 T43S T27E | SE S02 T44S R25E | SW S16 T44S R25E | S03 T47S T25E | S23 T44S R24E | S03 T47S R24E | NW S12 T46S R21E | S26 T43S R20E | NE S05 T45S R27E | S36 T45S R23E | NE S26 T43S R26E | S26 T43S R24E | S18 T46S R23E | S07 T45S R25E | SE S28 T45S R27E | S33 T45S R27E | S20 T45S R24E | S17 T44S R23E | ŀ | ł | S22 T46S R26E | S21 T46S R23E | S05 T45S R24E | T)CG 714T 902 |
| Longitude (degrees) | 0815014 | 0815223 | 0820327 | 0813748 | 0814648 | 0814921 | 0814911 | 0815227 | 0815351 | 0821002 | 0821534 | 0813754 | 0815709 | 0814052 | 0815251 | 0820315 | 0815034 | 0813632 | 0813637 | 0815516 | 0820209 | 0814850 | 0813402 | 0814144 | 0820105 | 0815623 | 0011100 |
| Latitude (degrees) | 262831 | 263306 | 262633 | 264432 | 264029 | 263836 | 262427 | 263735 | 262435 | 262853 | 264323 | 263554 | 263006 | 264253 | 264220 | 262734 | 263448 | 263151 | 263053 | 263259 | 263818 | 263718 | 262703 | 262713 | 262704 | 263515 | 264011 |
| Site identification number | 262831081501401 | 263306081522301 | 262633082032701 | 264432081374801 | 264029081464801 | 263836081492101 | 262427081491101 | 263735081522701 | 262435081535101 | 262853082100201 | 264323082153401 | 263554081375401 | 263006081570901 | 264253081405201 | 264220081525101 | 262734082031501 | 263448081503401 | 263151081363201 | 263053081363701 | 263259081551601 | 263818082020902 | 263718081485003 | 262703081340203 | 262713081414402 | 262704082010501 | 263515081562301 | 264011081442301 |
| Other well identifier or owner | WA-931 | Seven Lakes Sub | Stokes | WA-690 | WA-129 | WA-70 | WA-143 | WA-423 | Beach Golf Course | 1 | Searboard Railroad | WA-25 | 452325BN | WA-77 | WA-526 | LM-1267 | Tweed | Baum | W-LE001 | The Landings | Pine Island | ; | ; | Lee County | Light House | Brown | Description |
| Local well number | L-1094 | L-1157 | L-1186 | L-1242 | L-1318 | L-1396 | L-1569 | L-1595 | L-1634 | L-1646 | L-1687 | L-1688 | L-1817 | L-1903 | L-1962 | L-1967 | L-2003 | L-2061 | L-2063 | L-2115 | L-2201 | L-2292 | L-2313 | L-2319 | L-2401 | L-2426 | 1 2/133 |

| Date at end of construction | 1 1 | : | 10-77 | : | 1977 | 1977 | 1 | 12-05-78 | 1 | 1 | 10-11-60 | 1977 | 09-23-53 | 11-28-58 | 09-01-60 | | 1 | 1 | 12-05-80 | : | 1 | 1 | |
|--|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|------------------------|------------------|------------------|------------------------------|-----------------|-----------------|-----------------|-----------------|-----------------|------------------|------------------|----------------------|------------------|------------------|-----------------|--|
| Diameter of casing (inches) | | 0.9 | 4.0 | ; | 4.0 | 4.0 | 0.9 | ł | 0.9 | 8.0 | 24.0 20.0 13.4 9.6 | 9.6 | 13.4 | 13.4 | 9.6 | 13.4 | 5.5 | ł | 12.0 | 4.0 | 5.0 | 4.0 | |
| Bottom of casing (feet) | 120 | 115 | 405 | ; | 420 | 340 | 162 | 64 | 195 | 144 | 107 220 1,470 4,410 | 3,866 | 1,086 5,011 | 1,206 4,312 | 3,741 | 1,018 | 114 | ł | 542 1,865 | 198 | 164 | 302 | |
| Well depth (feet) | 1,300 | 160 | 645 | 909 | 625 | 620 | 916 | 705 | 780 | 1,012 | 13,970 | 11,893 | 12,858 | 11,910 | 11,955 | 12,877 | 920 | 996 | 2,150 | 828 | 824 | 870 | |
| Altitude of measuring point (feet) | 18 | 21 | 9 | 1 | 11.4 | 3 | 9 | 8 | 1 | 1 | 39 | 53 | 43 | 46.6 | 41.9 | 24 | 6 | 'n | 27 | 16 | \$ | 1 | |
| Land-net location | S12 T44S R27E | S11 T44S R27E | S26 T45S R22E | ŀ | S11 T44S R23E | S23 T43S R26E | S36 T45S R23E | SE S23 T43S R26E | NW S21 T44S R26E | NW S09 T44S R24E | S09 T44S R24E | S11 T46S R25E | S27 T45S R26E | S16 T46S R27E | S35 T46S R27E | S23 T45S R24E | NE S10 T45S R24E | SW S28 T45S R24E | SW S06 T43S R26E | SW S27 T46S R25E | NW S02 T45S R23E | S35 T43S R24E | |
| Longitude (degrees) | 0813358 | 0813547 | 0820510 | 0820831 | 0815927 | 0814054 | 0815722 | 0814051 | 0814440 | 0815501 | 0821903 | 0814051 | 0814144 | 0813721 | 0813457 | 0815247 | 0815345 | 0815500 | 0814539 | 0814802 | 0815837 | 0815231 | |
| Latitude (degrees) | 263931 | 263931 | 263117 | 263955 | 263907 | 264308 | 263057 | 264309 | 263815 | 263935 | 264107 | 262924 | 263219 | 262828 | 262557 | 263245 | 263456 | 263148 | 264541 | 262625 | 263022 | 264027 | |
| Site identification number | 263931081335801 | 263931081354701 | 263117082051001 | 263955082083101 | 263907081592701 | 265308081405402 | 263057081572202 | 26530908145101 | 263818081433501 | 263935081550101 | 264107082190301 | 262858081411801 | 263219081414401 | 262828081372101 | 262557081345701 | 263245081524701 | 263456081534501 | 263148081550001 | 264541081453901 | 262625081480201 | 263022081583701 | 264027081523101 | |
| Other well identifier or owner | WA-27 | WA-12 | Lee County | 1 | Lee County | Lee County | WA-85 | Lee County Water Plant | WA-21 | WA-68 | P-289 | P-919 | W-2979, P-160 | W-4839, P-271 | P-408 | W-3073, P-161 | WA-98 | WA-99 | W-LE007, U.S. Gypsum | WA-105 | WA-193 | WA-439 | |
| Local well number | L-2458 | L-2460 | L-2525 | L-2527 | L-2528 | L-2530 | L-2657 | L-2901 | L-4817 | L-4846 | L-5000 | L-5001 | L-5003 | L-5009 | L-5010 | L-5013 | L-5601 | L-5602 | L-5605 | L-5608 | L-5609 | L-5611 | |

| 263410082065001 265410 0820650 S09 T45S R22E 861 263221081504801 265321 0815048 SWS 19 T45S R25E 860 2645400815100001 264540 0815100 S06 T43S R25E 1730 2645400815100001 264540 0818100 S06 T43S R25E 11230 26454081525301 264345 0820802 NW S20 T46S R25E 19 635 264345081525301 264345 0815253 SE S14 T43S R24E 20 2,603 1,1 264345081525301 264345 0815253 SE S14 T43S R24E 20 2,603 1,1 264345081525301 264345 0815253 SE S14 T43S R24E 20 2,603 1,1 264345081525301 264345 0815253 SE S14 T43S R24E 20 2,603 1,1 264345081525301 264345 0821225 SW S26 T445S R21E 2 760 -1,200 264345081525301 264345 08214150 SW S26 T445S R25E 1 770 | Other well identifier or owner | | Latitude (degrees) | Longitude (degrees) | Land-net location | Altitude of measuring point (feet) | Well depth (feet) | Bottom of casing (feet) | Diameter of casing (inches) | Date at end of construction |
|---|-----------------------------------|-----------------|-----------------------|------------------------|-------------------|--|-------------------------|----------------------------------|-----------------------------------|-----------------------------|
| 263221081504801 263221 0815048 SWN S19 T4SS R25E 5 860 148 6.0 2645450081510000 264546 0815100 S06 T438 R25E - 787 300 440 265115081433501 264345 0815100 NW S20 T46S R25E - 1,230 - - 265115081433502 263115 0814833 NES33 T45S R25E - 1,730 1,30 4.0 265115081483502 263115 0815253 SES14 T43S R24E 2 2,603 1,38 2.0 264345081525301 264345 0815253 SES14 T43S R24E 2 2,623 1,58 2.0 264345081525301 264345 0815253 SES14 T43S R24E 2 2,623 1,58 2.0 264345081525301 264345081525301 264345 0814030 NW S31 T44S R25E 1 7 7 7 264345081525301 26528 0820633 NES28 T46S R25E 1 7 7 7 26525808206301 26528 | WA-702 | 263410082065001 | 263410 | 0820650 | S09 T45S R22E | 1 | 861 | 350 | 4.0 | 1 |
| 264540081510001 264540 0815100 SOG T43S R25E - 787 300 4 0 265115081483501 263115 0814833 - - 1,230 - - 262706083208020 263115 0814833 NES371458 R25E - 170 750 11.3 262115081483502 263115 0815233 SE S14 T43S R24E 2 663 450 11.00 264345081523301 264345 0815233 SE S14 T43S R24E 2 2.603 11.00 2.00 264345081523301 264345 0815223 SE S14 T43S R24E 2 2.603 1.60 2 264345081523301 264345 0814908 NW S31 T46S R25E 1 7 7 - | WA-761 | 263221081504801 | 263221 | 0815048 | SW S19 T45S R25E | 5 | 098 | 148 | 0.9 | ŀ |
| 263115081483501 263115 0814835 — </td <td>WA-841</td> <td>264540081510001</td> <td>264540</td> <td>0815100</td> <td>S06 T43S R25E</td> <td>1</td> <td>787</td> <td>300</td> <td>4.0</td> <td>1</td> | WA-841 | 264540081510001 | 264540 | 0815100 | S06 T43S R25E | 1 | 787 | 300 | 4.0 | 1 |
| 262115081433502 262706082080201 262706082080201 262706082080201 CARAGE 0820746872E - 770 750 1.13 2641345081525301 264345 0815253 SE S14 T43S R24E 2 1,096 24.0 - 264345081525301 264345 0815253 SE S14 T43S R24E 2 2,603 1,582 - 264345081525301 264345 0815253 SE S14 T43S R24E 2 2,630 1,60 - 265129082112901 265129 0821129 SW S2G T45S R21E 2 760 - - - 265129082112901 265824 0814150 SW S2G T45S R21E 2 760 - | LM-1841 | 263115081483501 | 263115 | 0814835 | ı | ł | 1,230 | 1 | 1 | 1 |
| 263115081483502 263115 0814835 NE S33 T4SS R2SE 19 635 450 11.0 264345081525301 264345 0815253 SE S14 T43S R24E 20 2,603 1,1096 24.0 264345081525301 264345 0815253 SE S14 T143S R24E 20 2,526 200 16.0 264345081525301 264345 0815253 SE S14 T143S R24E 2 2,526 200 16.0 264345081525301 264345 0821129 SW S26 T145S R24E 2 760 2652580812690821 263824 0814908 NW S31 T45S R25E 11 822 2652580820630301 265834 0814160 SE S15 T44S R26E 20 770 2662830820630301 26583 0820633 SW S06 T44S R26E 3 4.0 2662840820630301 26433 0814063 NW S31 T47S R26E 3 7 7 | .M-2464S | 262706082080201 | 262706 | 0820802 | NW S20 T46S R22E | ; | 770 | 750 | 1.3 | 08-01-85 |
| 264345081525301 264345 0815253 SES14T438 R24E 20 2,603 1,096 24,0 264345081525301 264345 0815253 SES14T438 R24E 20 2,526 200 1,60 264345081525301 2643129 0815253 SES14T438 R24E 2 2,526 200 1,60 265358081400801 265358 0814908 NW S33 T46S R25E 11 822 262628082063030 265638 0814028 NW S33 T46S R25E 11 822 2626268082063030 266402 0820903 SW S06 T44S R25E 11 822 2626268082063030 266403 0820903 SW S06 T44S R22E 4 774 660 262626808206302 264433 0814023 NW S13 T47S R26E 3 963 340 78 2624433081360602 264433 0814023 NW S13 T44S R25E 3 645 77 26244433081360602 264433 0814023 SW | LM-1842 | | 263115 | 0814835 | NE S33 T45S R25E | 19 | 635 | 450 | 11.0 | 05-12-92 |
| 26.0345081525301 264345081525301 264345 0815253 SES14 T438 R24E 20 2.526 1,318 1,00 16.0 263129082112901 263129 0821129 SW S26 T458 R21E 2 760 - - 2625388081490801 265258 0814908 NW S33 T468 R25E 11 822 26253834081415001 26528 0814908 NW S33 T468 R25E 4 774 660 262628082063301 26528 0820633 NR S28 T468 R22E 4 774 660 264020820630301 266230 0820633 NW S13 T478 R26E 5 1,460 264433081405001 26403 0814050 NR S34 T458 R26E 4 778 450 9.8 264433081405001 264043 0814050 NR S13 T448 R23E 1 1,200 26444308145001 265320 08202227 SW S17 T448 R23E 3 1,420 | NFM-11 | 264345081525301 | 264345 | 0815253 | SE S14 T43S R24E | 20 | 2,603 | 1,096 1,582 2,340 | 24.0 20.0 | 10-01-87 |
| 263129082112901 263129 SWS26 T45S R21E 2 760 262558081490801 262558 0814908 NWS33 T46S R25E 11 822 2638349081415001 263834 0814150 SE S15 T44S R25E 11 60 264602082063301 264602 0820633 NE S28 T46S R25E 3 963 360 9.8 264002082090301 264002 0820633 NW S13 T47S R26E 3 963 360 9.8 264030081402301 26230 0814023 NW S13 T47S R26E 3 1,460 26433081360602 264433 0814050 NE S34 T45S R26E 13 1,450 26433081360812 263117 0814150 NE S34 T44S R23E 3 1,450 264336082052701 263318 0820521 SW S07 T44S R23E 3 645 488 5.0 2641208081563101 264147 0820113 S00 T44S R23E | NFM-M1 | 264345081525301 | 264345 | 0815253 | SE S14 T43S R24E | 20 | 2,526 | 8 200 1,318 1,950 | 26.0 16.0 10.0 4.0 | 08-01-86 |
| 26258081490801 262558 08149008 NW S33 T46S R25E 11 822 263834081415001 263834 0814150 SE S15 T44S R26E 20 770 262628082063301 262628 0820633 NB S28 T46S R22E 3 963 360 9.8 264002082063301 264002 0820903 SW S0G T44S R22E 3 1,460 262309081402301 26433081360602 264433 0814023 NW S13 T47S R26E 5 1,460 264433081360602 264433 0813606 SE S10 T43S R27E 19 1,200 340 7.8 263117081415001 26318 0813606 SE S10 T43S R25E 43 1,350 263318081552701 263318 0815527 SW S17 T44S R23E 8 740 455 5 264147082011301 264128 0820521 SW S07 T44S R23E 4 720 488 5.0 2643160820230101 26431 | W-16242 | 263129082112901 | 263129 | 0821129 | SW S26 T45S R21E | 2 | 092 | 1 | 1 | 12-88 |
| 263834081415001 263834 0814150 SE S15 T448 R26E 20 770 262628082063301 262628 0820633 NB S28 T46S R22E 4 774 660 26400208209301 262628 0820903 SW S06 T44S R22E 3 963 360 9.8 26403209081402301 262309 0814023 NW S13 T47S R26E 5 1,460 264433081360602 264433 0813606 SE S10 T43S R27E 19 1,200 340 7.8 263117081415001 263117 0814150 NE S34 T45S R26E 43 1,350 263318081552701 263318 0820227 SW S17 T44S R23E 5 1,200 262935082052101 264147 0820113 S00 T44S R23E 8 740 455 5 264128081563101 2641128 082032 S00 T44S R23E 4 720 485 5.0 2643160820320101 264316 0820321 | W-16523 | 262558081490801 | 262558 | 0814908 | NW S33 T46S R25E | 11 | 822 | 1 | ı | 04-15-90 |
| 262628082063301 262628 0820633 NE S28 T46S R22E 4 774 660 264002082093301 264002 0820903 SW S06 T44S R22E 3 963 360 262309081402301 264330 0814023 NW S13 T47S R26E 5 1,460 264433081360602 264433 0814023 NW S13 T44S R26E 43 1,200 340 7.8 264433081360602 264433 0814150 NE S34 T45S R26E 43 1,350 263820082022701 263818 0820227 SW S17 T44S R23E 3 1,200 263318081552701 262935082052101 262935 0820521 SW S07 T46S R23E 8 740 455 5 264136081563101 264128 0820320 S00 T43S R23E 4 720 485 5.0 264316082023001 264316 0820333 S00 T43S R23E 4 720 485 5.0 263366082033301 264316 <td>N-15286C</td> <td>263834081415001</td> <td>263834</td> <td>0814150</td> <td>SE S15 T44S R26E</td> <td>20</td> <td>770</td> <td>1</td> <td>1</td> <td>04-06-82</td> | N-15286C | 263834081415001 | 263834 | 0814150 | SE S15 T44S R26E | 20 | 770 | 1 | 1 | 04-06-82 |
| 264002082090301 264002 0820903 SW S06 T44S R22E 3 963 360 9.8 262309081402301 262309 0814023 NW S13 T47S R26E 5 1,460 264433081360602 264433 0813606 SE S10 T43S R27E 19 1,200 340 7.8 264433081405011 263117 0813606 SE S10 T43S R27E 43 1,350 26331082022701 263218 0820227 SW S17 T44S R23E 3.2 778 450 9.8 262935082022101 263318 0815527 5 1,420 262935082052101 262935 0820521 SW S02 T46S R22E 5 1,420 264147082011301 264147 0820113 S00 T44S R23E 8 740 455 5 264316082033001 264316 0820230 S00 T44S R23E 4 720 485 5.0 263416082032101 263416 0820221 <td>W-LE004</td> <td>262628082063301</td> <td>262628</td> <td>0820633</td> <td>NE S28 T46S R22E</td> <td>4</td> <td>774</td> <td>099</td> <td>ı</td> <td>02-05-81</td> | W-LE004 | 262628082063301 | 262628 | 0820633 | NE S28 T46S R22E | 4 | 774 | 099 | ı | 02-05-81 |
| 262309081402301 262309 0814023 NW S13 T47S R26E 5 1,460 264433081360602 264433 0813606 SE S10 T43S R27E 19 1,200 340 7.8 263117081415001 263117 0814150 NE S34 T45S R26E 43 1,350 263820082022701 263318 0820227 SW S17 T44S R23E 3.2 778 450 9.8 263318081552701 263318 0815527 - - 5 1,200 - - - 262935082052101 262935 0820521 SW S02 T46S R22E 5 1,420 - | 3014, LM-1622 W-14790 | 264002082090 | 264002 | 0820903 | SW S06 T44S R22E | 8 | 696 | 360 | 8.6 | 05-22-81 |
| 264433081360602 264433 0813606 SE S10 T43S R27E 19 1,200 340 7.8 263117081415001 263117 0814150 NE S34 T45S R26E 43 1,350 263820082022701 263318 0815527 - 5 1,200 262935082052101 262935 0820521 SW S02 T46S R22E 5 1,420 264147082011301 264147 0820113 S00 T43S R23E 8 740 455 5 264128081563101 264128 0815631 S00 T44S R23E 3 645 488 5.0 26416082032001 263858 0820320 S00 T44S R23E 4 720 485 5.0 264316082032101 263416 0820321 S00 T44S R23E 2 1,402 980 8.0 263906082032101 263906 0820321 S00 T44S R23E 3 1,080 898 5.0 | W-LE017 | 262309081402301 | 262309 | 0814023 | NW S13 T47S R26E | 5 | 1,460 | 1 | 1 | 01-26-81 |
| 263117081415001 263117 0814150 NE S34 T45S R26E 43 1,350 263820082022701 263820 0820227 SW S17 T44S R23E 3.2 778 450 9.8 263318081552701 263318 0815527 5 1,200 262935082052101 262935 0820521 SW S02 T46S R22E 5 1,420 264147082011301 264147 0820113 S00 T43S R23E 8 740 455 5 264128081563101 264128 0820320 S00 T44S R23E 3 645 488 5.0 263858082032001 264316 0820320 S00 T44S R23E 4 720 485 5.0 263416082020101 263416 0820321 S00 T44S R23E 2 1,402 980 8.0 263906082032101 263906 0820321 S00 T44S R23E 3 1,608 898 5.0 | /-LE022D | 264433081360602 | 264433 | 0813606 | SE S10 T43S R27E | 19 | 1,200 | 340 | 7.8 | 11-17-81 |
| 263320082022701 263320 0820227 SW S17 T44S R23E 3.2 778 450 9.8 263318081552701 263318 0815527 5 1,200 262935082052101 262935 0820521 SW S02 T46S R22E 5 1,420 264147082011301 264147 0820113 S00 T43S R24E 15 800 560 12.0 264128081563101 264128 0815631 S00 T44S R23E 3 645 488 5.0 263858082032001 264316 0820333 S00 T44S R23E 4 720 485 5.0 2643160820320101 263416 08203201 S00 T44S R23E 2 1,402 980 8.0 263906082032101 263906 0820321 S00 T44S R23E 3 1,080 898 5.0 | E023, P-979 | 263117081415001 | 263117 | 0814150 | NE S34 T45S R26E | 43 | 1,350 | 1 | ı | 09-14-79 |
| 263318081552701 263318 0815527 - </td <td>L-3004D</td> <td>263820082022701</td> <td>263820</td> <td>0820227</td> <td>SW S17 T44S R23E</td> <td>3.2</td> <td>778</td> <td>450</td> <td>8.6</td> <td>ſ</td> | L-3004D | 263820082022701 | 263820 | 0820227 | SW S17 T44S R23E | 3.2 | 778 | 450 | 8.6 | ſ |
| 262935082052101 262935 0820521 SW S02 T46S R22E 5 1,420 264147082011301 264147 0820113 S00 T43S R23E 8 740 455 5 264128081563101 264128 0815631 S00 T44S R24E 15 800 560 12.0 263858082032001 263858 0820320 S00 T44S R23E 4 720 488 5.0 26431608203301 264316 0820201 S00 T45S R23E 2 1,402 580 8.0 263906082032101 263906 0820321 S00 T44S R23E 3 1,080 898 5.0 | LE00005 | 263318081552701 | 263318 | 0815527 | ı | 5 | 1,200 | ł | 1 | 07-17-80 |
| 264147082011301 264147 0820113 S00 T43S R23E 8 740 455 5 264128081563101 264128 0815631 S00 T43S R24E 15 800 560 12.0 263858082032001 263858 0820320 S00 T44S R23E 3 645 488 5.0 264316082033301 264316 0820321 S00 T45S R23E 4 720 485 5.0 263416082020101 263416 0820321 S00 T44S R23E 2 1,402 980 8.0 263906082032101 263906 0820321 S00 T44S R23E 3 1,080 898 5.0 | 3035, W-15910 | | 262935 | 0820521 | SW S02 T46S R22E | 5 | 1,420 | 1 | 1 | 10-11-85 |
| 264128081563101 264128 264128081563101 264128 0815631 S00 T44S R24E 15 800 560 12.0 2643858082032001 264316 0820333 S00 T44S R23E 4 720 485 5.0 264316082020101 263416 0820201 S00 T44S R23E 2 1,402 580/980 8.0 263906082032101 263906 0820321 S00 T44S R23E 3 1,080 898 5.0 | -3247, Site P | 264147082011301 | 264147 | 0820113 | S00 T43S R23E | ∞ | 740 | 455 | ď | 12-90 |
| 263858082032001 263858 0820320 S00 T44S R23E 3 645 488 5.0 264316082033301 264316 0820333 S00 T43S R22E 4 720 485 5.0 263416082020101 263416 0820201 S00 T44S R23E 2 1,402 58 14.0 263906082032101 263906 0820321 S00 T44S R23E 3 1,080 898 5.0 | -3273, Site V | 264128081563101 | 264128 | 0815631 | S00 T43S R24E | 15 | 800 | 260 | 12.0 | 12-90 |
| 264316082033301 264316 0820333 S00 T43S R22E 4 720 485 5.0 263416082020101 263416 0820201 S00 T45S R23E 2 1,402 58 980 14.0 263906082032101 263906 0820321 S00 T44S R23E 3 1,080 898 5.0 | -3353, Site M | 263858082032001 | 263858 | 0820320 | S00 T44S R23E | 3 | 645 | 488 | 5.0 | 12-90 |
| 263416082020101 263416 0820201 S00 T45S R23E 2 1,402 58 14.0 980 14.00 8.0 263906082032101 263906082032101 263906 0820321 S00 T44S R23E 3 1,080 898 5.0 | -3366, site N | 264316082033301 | 264316 | 0820333 | S00 T43S R22E | 4 | 720 | 485 | 5.0 | 12-90 |
| 263906082032101 263906 0820321 S00 T44S R23E 3 1,080 898 5.0 | -3367, site O | 263416082020101 | 263416 | 0820201 | S00 T45S R23E | 2 | 1,402 | 58 980 | 14.0 | 12-01-90 |
| | -3479, site M | 263906082032101 | 263906 | 0820321 | S00 T44S R23E | 3 | 1,080 | 868 | 5.0 | 12-90 |

Appendix II

Selected Water-Quality Data Collected from Known Intervals in Wells from the Intermediate and Floridan Aquifer Systems

[Well locations are shown in figures 2 and 3. Source of water sample: completed, data from completed interval; DQW, data collected while drilling by the reverse-air rotary method; packer, data from open-hole interval by packer test; WAQW, data collected during SFWMD well abandonment program; USGS, U.S. Geological Survey; SFWMD, South Florida Water Management District; unless denoted as USGS, SFWMD, or WAQW, the samples were collected by private consultants. Other annotations: ft, feet; mg/L, milligrams per liter; μ S/cm, microsiemens per centimeter; --, no data or unknown; ?, depth to top of sample interval is unknown; *, USGS data not in QWDATA data base; **, chloride concentration calculated from specific conductance in wells C-914 and C-916; sample interval depths are from the measuring point given in appendix I]

| Local well identifier | Sampling date | Depth of sample interval (ft) | Chloride (mg/L) | Sulfate (mg/L) | Dissolved solids (mg/L) | Specific conductance (µS/cm) | Source of water sample |
|-----------------------|------------------|--|--------------------|-------------------|-------------------------------|------------------------------------|------------------------|
| C-21 | 12-15-41 | 166-566 | 820 | 302 | 1,850 | 3,310 | Completed-USGS |
| C-22 | 12-15-41 | 228-845 | 980 | 560 | 2,500 | 4,200 | Completed-USGS |
| C-236 | 03-16-59 | ?-875 | 785 | | 2,070 | | Completed-USGS* |
| C-258 | 10-07-81 | ?-783 | 1,000 | 530 | 2,660 | | Completed-USGS |
| C-284 | 10-08-59 | ?-1,119 | 1,100 | | 2,660 | | Completed-USGS* |
| C-308 | 11-21-75 | 587-700 | 1,800 | | | 7,000 | Completed-USGS |
| C-415 | 12-23-64 | 752-912 | 1,200 | | | | Completed-USGS* |
| C-441 | 03-14-66 | 412-915 | 1,530 | | | | Completed-USGS* |
| C-820 | 02-08-77 | 1,998-2,500 | 13,500 | 3,080 | 26,000 | | Completed |
| C-876 | 11-13-75 | 301-593 | 1,280 | | | | Completed-USGS* |
| C-913 | 01-11-83 | 300-1,220 | 2,190 | | | 7,910 | Completed-SFWMI |
| C-914** | 12-19-80 | 390-1220 | 2,900 | | | 9,570 | Completed-SFWM |
| C-916** | 07-22-81 | 360-880 | 1,540 | | | 5,630 | Completed-SFWM |
| C-917 | 01-11-83 | 430-880 | 1,600 | | | 6,030 | Completed-SFWM |
| C-962 | 12-13-83 | 2,228-2,280 | 17,000 | 2,000 | | 40,300 | Completed-USGS |
| C-1101 | 1990 | 390-800 | 6,550 | | | 21,600 | DQW |
| | 11-90 | 650-770 | 4,000 | | | | Completed |
| | 11-90 | 970-1,010 | 10,000 | | | | Packer |
| C-1102 | 11-90 | 1,220-1,270 | 17,000 | | | | Packer |
| | 11-90 | 1,330-1,610 | 18,000 | | | | Packer |
| G 1102 | 01-91 | 940-1,030 | 2,000 | | | | Packer |
| C-1103 | 01-91 | 1,290-1,620 | 13,300 | | | | Packer |
| G 1105 | 09-93 | 1,000-1,089 | 15,000 | 1,680 | 25,600 | 39,000 | Completed |
| C-1105 | 09-93 | 1,490-1,600 | 19,000 | 2,540 | 35,400 | 44,600 | Completed |
| | 10-20-92 | 900-995 | 435 | 725 | 5,330 | 7,000 | Completed |
| | 01-10-94 | 900-995 | 2,100 | 660 | 4,900 | 7,100 | Completed |
| C-1108 | 07-19-92 | 1,010-1,050 | 2,140 | 756 | 4,500 | 6,490 | Packer |
| | 07-22-92 | 1,300-1,331 | 8,900 | 1,010 | 16,600 | 20,900 | Packer |
| | 10-20-92 | 1,815-1,930 | 20,800 | 2,740 | 37,300 | 39,000 | Completed |
| C-1110 | 02-14-85 | 304-658 | 1,170 | | | 2,620 | Completed-WAQW |
| | | 1,158-1,185 | 10,200 | 1,340 | 17,600 | 25,400 | Packer-SFWMD |
| | | 1,287-1,318 | 14,300 | 1,750 | 27,300 | 35,700 | Packer-SFWMD |
| C-1111 | | 1,469-1,524 | 17,000 | 2,260 | 35,100 | 45,000 | Packer-SFWMD |
| | | 1,851-1,901 | 16,300 | 2,140 | 34,900 | 45,100 | Packer-SFWMD |
| | | 2,195-2,251 | 19,300 | 2,510 | 34,600 | 46,600 | Packer-SFWMD |
| C-1124 | 12-10-82 | 1,840-1,890 | 2,440 | 900 | 5,170 | | Completed |

| Local well identifier | Sampling date | Depth of sample interval (ft) | Chloride (mg/L) | Sulfate (mg/L) | Dissolved solids (mg/L) | Specific conductance (μS/cm) | Source of water sample |
|-----------------------|------------------|--|--------------------|-------------------|-------------------------------|------------------------------------|------------------------|
| C-1133 | 04-23-88 | 229-1,084 | 770 | 390 | 1,870 | | Completed |
| | 02-06-92 | 427-992 | 301 | | 959 | 1,400 | DQW |
| CH-313 | 03-03-92 | 1,536-1,568 | 3,840 | 340 | 7,880 | 11,200 | Packer |
| | 03-02-92 | 1,566-1,601 | 89 | 290 | 15,400 | 22,300 | Packer |
| CH-314 | 06-24-92 | 1,340-1,415 | 925 | 432 | | 4,100 | Completed |
| CITST | 06-23-92 | 1,795-1,830 | 17,500 | 2,700 | 34,900 | 46,200 | Completed |
| | 10-19-81 | 811-816 | 1,600 | 500 | 3,500 | 6,200 | Completed-USGS |
| | 03-09-81 | 895-1,125 | 850 | | 2,000 | 3,330 | Packer-USGS |
| G-2296 | 03-07-81 | 1,430-1,620 | 1,800 | | 3,640 | 6,050 | Packer-USGS |
| | 03-03-81 | 2,450-2,810 | 19,500 | | 38,000 | 50,000 | Packer-USGS |
| | 01-15-92 | 2,447-2,811 | 20,000 | 2,700 | 37,200 | 50,800 | Completed-USGS |
| G-2617 | 01-10-92 | 1,648-1,728 | 1,100 | 450 | 2,570 | 4,220 | Completed-USGS |
| G-2618 | 01-14-92 | 1,104-1,164 | 620 | 340 | 1,650 | 2,750 | Completed-USGS |
| G-2619 | 01-13-92 | 895-1,052 | 1,100 | 400 | 2,590 | 4,360 | Completed-USGS |
| HE-9 | 01-05-43 | 949-1,039 | 1,430 | | | | Completed-USGS |
| HE-46 | 05-07-53 | ?-1,110 | 925 | | | 3,840 | Completed-USGS |
| HE-54 | 05-01-53 | ?-1,300 | 1,390 | | | 4,880 | Completed-USGS |
| HE-81 | 12-02-75 | 540-750 | 1,170 | | | 4,400 | Completed-USGS |
| HE-116 | 03-07-75 | ?-700 | 1,300 | | 2,950 | 4,460 | Completed-USGS |
| HE-278 | 12-10-53 | 520-790 | 1,030 | 245 | 2,300 | 3,820 | Completed-USGS |
| HE-293 | 12-04-75 | 277-792 | 1,080 | | | | Completed-USGS |
| HE-296 | 05-14-58 | 346-872 | 2,250 | | | | Completed |
| HE-297 | 05-14-58 | 319-782 | 2,170 | | | | Completed |
| | 01-94 | 1,266-1,284 | 490 | 366 | 1,370 | 2,240 | Packer-SFWMD |
| | 01-94 | 1,442-1,494 | 445 | 322 | 1,370 | 2,230 | Packer-SFWMD |
| HE-1087 | 01-94 | 1,652-1,704 | 882 | 440 | 2,160 | | Packer-SFWMD |
| | 01-94 | 1,890-1,908 | 3,080 | 424 | 5,550 | 9,990 | Packer-SFWMD |
| | 01-94 | 2,072-2,124 | 10,700 | 1,360 | 19,100 | 30,800 | Packer-SFWMD |
| HE-1088 | 04-23-85 | 220-738 | 917 | | | 2,640 | Completed-WAQV |
| HE-1104 | 04-04-83 | 2,020-2,070 | 7,850 | 350 | 13,200 | | Completed |
| HE-1105 | 10-20-82 | 1,578-1,598 | 730 | 256 | 2,090 | | Completed |
| HE-1107 | 06-12-82 | 1,546-1,579 | 518 | 300 | | | Completed |
| L-448 | 04-08-46 | 390-847 | 825 | 313 | | 3,330 | Completed-USGS |
| L-468 | 06-15-77 | 438-689 | 740 | 360 | 1,970 | 3,250 | Completed-USGS |
| L-470 | 04-11-46 | 427-843 | 675 | 286 | | 2,840 | Completed-USGS |
| L-562 | 01-14-85 | 698-863 | 750 | | | 2,180 | Completed-WAQV |
| L-591 | 03-29-75 | 405-654 | 870 | 360 | 2,090 | 4,020 | Completed-USGS |

| Local well identifier | Sampling date | Depth of sample interval (ft) | Chloride (mg/L) | Sulfate (mg/L) | Dissolved solids (mg/L) | Specific conductance (µS/cm) | Source of water sample |
|-----------------------|------------------|--|--------------------|-------------------|-------------------------------|------------------------------------|------------------------|
| L-592 | 01-09-73 | 367-724 | 1,100 | 352 | | 4800 | Completed-USGS |
| L-907 | 04-22-81 | 340-997 | 1,350 | | | 4,850 | Completed-WAQV |
| L-912 | 03-07-73 | 650-836 | 1,400 | 340 | | 5,000 | Completed-USGS |
| L-964 | 12-13-72 | 362-808 | 780 | 320 | | 3,380 | Completed-USGS |
| L-1094 | 02-07-73 | 508-1,009 | 940 | 340 | | 3,810 | Completed-USGS |
| L-1094 | 01-21-88 | 508-1,009 | 936 | | | 4,280 | Completed-WAQV |
| L-1157 | 02-21-73 | 589-740 | 700 | 320 | | 2,980 | Completed-USGS |
| L-1186 | 03-29-75 | 500-700 | 1,300 | 630 | 3,280 | 5,440 | Completed-USGS |
| L-1242 | 10-22-86 | 318-730 | 755 | | | 1,880 | Completed-WAQV |
| L-1569 | 09-23-81 | 296-772 | 1,020 | | | 4,000 | Completed-WAQV |
| L-1634 | 08-28-80 | 740-950 | 1,400 | 470 | 3,160 | 5,310 | Completed-USGS |
| L-1646 | 01-07-77 | 382-673 | 825 | | 2,350 | 3,910 | Completed-USGS |
| L-1687 | 03-65 | 755(?)-760 | 17,600 | | | | Packer |
| L-1903 | 06-24-80 | 190-669 | 413 | | 4,930 | 2,060 | Completed-WAQV |
| L-1962 | 05-22-85 | 315-788 | 745 | | | 2,300 | Completed-WAQV |
| L-1967 | 07-11-84 | 700-881 | 2,700 | | | 8,050 | Completed-WAQV |
| L-2003 | 12-24-74 | 240-685 | 1,300 | 320 | 2,820 | 4,650 | Completed-USGS |
| L-2061 | 02-06-75 | 325-899 | 1,150 | | | | Completed-USGS |
| L-2115 | 06-30-75 | 610-750 | 720 | 290 | 1,690 | 2,970 | Completed-USGS |
| L-2201 | 08-20-80 | 625-850 | 960 | 280 | 2,390 | 3,730 | Completed-USGS |
| L-2292 | 06-07-78 | 302-616 | 940 | 300 | 2,320 | 3,690 | Completed-USGS |
| L-2292 | 10-05-82 | 302-616 | 900 | | | 3,500 | Completed-USGS |
| L-2313 | 06-07-78 | 400-670 | 1,000 | 550 | 2,790 | 4,400 | Completed-USGS |
| L-2319 | 06-08-78 | 492-750 | 410 | 240 | 1,250 | 2,210 | Completed-USGS |
| L-2401 | 11-10-77 | 470-855 | 1,350 | 250 | 2,900 | 5,000 | Completed-USGS |
| L-2426 | 01-26-77 | 385-665 | 460 | 120 | 1,090 | 1,730 | Completed-USGS |
| L-2433 | 02-10-77 | ?-700 | 870 | 310 | 1,980 | 3,400 | Completed-USGS |
| L-2434 | 06-16-78 | 353-700 | 400 | 130 | 1,200 | 1,900 | Completed-USGS |
| L-2525 | 11-30-77 | 405-645 | 440 | 280 | 1,230 | 2,000 | Completed-USGS |
| L-2527 | 12-19-77 | 360-605 | 2,000 | 290 | 3,660 | 6,000 | Completed-USGS |
| L-2321 | 10-05-82 | 360-605 | 1,860 | | | 5,700 | Completed-USGS |
| L-2528 | 06-09-78 | 420-625 | 920 | 240 | 2,220 | 3,650 | Completed-USGS |
| L-2530 | 09-25-79 | 340-620 | 500 | 270 | 1,520 | 2,500 | Completed-USGS |
| 1 5605 | 11-18-80 | 542-945 | 1,000 | | | 4,000 | DQW |
| L-5605 | 12-19-80 | 1,865-1,985 | 19,400 | 2,900 | | 45,000 | DQW-USGS |
| L-5611 | 09-14-84 | 302-870 | 1,150 | | | 3,490 | Completed-WAQV |
| L-5612 | 04-24-85 | 360-670 | 634 | | | 1,480 | Completed-WAQV |

| Local well identifier | Sampling date | Depth of sample interval (ft) | Chloride (mg/L) | Sulfate (mg/L) | Dissolved solids (mg/L) | Specific conductance (µS/cm) | Source of water sample |
|-----------------------|------------------|--|--------------------|-------------------|-------------------------------|------------------------------------|------------------------|
| L-5613 | 06-16-86 | 750-760 | 730 | | | 2,180 | Completed-WAQW |
| L-5614 | 11-25-86 | 350-861 | 440 | | | 1,930 | Completed-WAQW |
| L-5616 | 07-09-87 | 300-787 | 960 | | | 3,500 | Completed-WAQW |
| L-5641 | 04-82 | 305-1,100 | 1,000 | | | | DQW |
| L-5735 | 10-27-87 | 740-770 | 960 | | | 3,830 | Completed-USGS |
| L-5801 | 04-22-92 | 450-635 | 1,160 | | | 4,380 | Completed-USGS |
| L-5802 | 06-07-87 | 1,479-1,489 | 3,300 | 460 | 2,140 | 3,700 | Packer |
| L-3002 | 06-05-87 | 1,559-1,569 | 7,150 | 260 | 11,700 | 20,000 | Packer |
| | 10-23-87 | 1,318-1,422 | 720 | | 1,770 | 3,000 | Completed |
| L-5803 | 12-12-90 | 1,318-1,422 | 555 | 379 | 1,580 | 2,600 | Completed |
| L-5803 | 10-30-87 | 1,930-2,004 | 19,400 | | 35,600 | 56,000 | Completed |
| | 12-12-90 | 1,930-2,004 | 18,600 | 2,820 | 35,200 | 49,900 | Completed |
| L-6412 | | 360-590 | 6,000 | | | | DQW |
| L-6431 | 05-90 | 455-740 | 750 | | | | Completed |
| L-6432 | 07-90 | 560-800 | 520 | | | 2,210 | Completed |
| L-6433 | 07-90 | 488-645 | 1,450 | | | | Completed |
| L-6434 | 07-90 | 485-720 | 680 | | | | Completed |
| L-6435 | | 980-1,060 | 5,450 | | | 10,100 | DQW |
| L-6436 | | 900-940 | 13,100 | | | | DQW |
| L-6437 | | 800-1,070 | 5,200 | | | 17,000 | DQW |
| L-6438 | 05-90 | 494-780 | 580 | | | | Completed |
| L-6439 | 05-90 | 505-760 | 800 | | | | Completed |
| L-6440 | 07-90 | 520-760 | 700 | | | | Completed |
| L-6441 | 07-90 | 395-750 | 1,100 | | | | Completed |
| L-6442 | 07-90 | 430-740 | 560 | | | | Completed |
| S-450 | 06-30-41 | 1,002-1,046 | 1,180 | | | 4,760 | Completed-USGS |
| 3-430 | 06-30-41 | 1,200-1,210 | 1,410 | 644 | | 5,720 | Completed-USGS |

Appendix III Tops of Geologic Units in Selected Wells as Determined for this Study

[Well locations are shown in figures 2 and 3. Asterisk indicates top determined using lithologic description only. Dashes indicate well not deep enough or inadequate data available to determine top. Tops for Ocala Limestone and Avon Park Formation not determined for all wells in this appendix. Depths are from measuring point, which is at land surface or above]

| Local well identifier | Altitude measuring point (feet) | Depth to top of basal Hawthorn unit (feet) | Depth to basal contact of Hawthorn Group (feet) | Depth to top of Ocala Limestone (feet) | Depth to top of Avon Park Formation (feet) | Depth to top of dolomite- evaporite unit (feet) |
|-----------------------|--|---|---|--|--|--|
| C-234 | 37 | 530 | 800 | 1,000 | 1,280 | 1,820 |
| C-679 | 14 | 626 | 768 | | | |
| C-680 | 12 | 647 | 855 | | | |
| C-701 | 34 | | 860* | 970 | 1,230 | 1,835 |
| C-708 | 32 | 560 | 850 | | | 1,960 |
| C-710 | 38 | 520 | 760 | 910 | 1,330 | 2,230 |
| C-711 | 32 | 580 | 810 | 1,000 | 1,540 | 2,070 |
| C-712 | 32 | 583 | 710 | 1,010 | 1,264 | 1,760 |
| C-719 | 35 | | | 1,020 | 1,398 | 1,873 |
| C-726 | 25 | | 805* | 1,270 | 1,625 | 2,350 |
| C-727 | 45 | 592* | 801* | | 1,365 | 2,080 |
| C-729 | 35 | | | | | 2,250 |
| C-739 | 36 | 586 | 756 | | | |
| C-742 | 40 | 525 | 720* | 1,060 | 1,382 | |
| C-753 | 42 | 517 | 650 | 1,055 | 1,394 | 2,027 |
| C-759 | 21 | 580 | 790 | 1,110 | | |
| C-764 | 40 | 534 | 680 | 1,090 | 1,360 | 2,255 |
| C-781 | 46 | 556 | 846 | 1,134 | 1,441 | |
| C-794 | 29 | 645 | 820 | 1,020 | | |
| C-802 | 39 | 760 | 960 | 1,150 | 1,300 | |
| C-808 | 40 | 650 | 825 | 1,200 | | |
| C-820 | 41 | 665 | 840 | 1,080 | 1,395 | 2,100 |
| C-851 | 18 | | | 968 | 1,381 | |
| C-913 | 5 | 695 | 858 | | | |
| C-914 | 6 | 646 | 880 | | | |
| C-915 | 5 | 630 | 780 | | | |
| C-916 | 5 | 615 | 780 | | | |
| C-917 | 6 | 701 | | | | |
| C-918 | 8 | 678 | 837 | 1,227 | | |
| C-919 | 9 | 707 | 935 | 1,081 | | |
| C-920 | 9 | 684 | 890 | 1,140 | | |
| C-921 | 10 | 712 | 930 | 1,088 | | |
| C-922 | 5 | 720* | 920* | 1,070 | | |
| C-923 | 8 | 708 | 882 | 1,272 | | |

| Local well identifier | Altitude measuring point (feet) | Depth to top of basal Hawthorn unit (feet) | Depth to basal contact of Hawthorn Group (feet) | Depth to top of Ocala Limestone (feet) | Depth to top of Avon Park Formation (feet) | Depth to top of dolomite- evaporite unit (feet) |
|--------------------------|--|---|---|--|--|--|
| C-924 | 7 | 689 | 858 | 1,267 | | |
| C-925 | 8 | 705 | 905 | 1,330 | | |
| C-926 | 11 | 645 | 880 | 1,350 | | |
| C-927 | 5 | 670* | 920* | | | |
| C-928 | 6 | 670* | 860* | | | |
| C-929 | 5 | 690* | 880* | 1,270 | | |
| C-930 | 15 | | 1,028* | 1,240 | | |
| C-931 | 5 | 670* | 850* | 1,170 | | |
| C-932 | 10 | 610* | 840* | 1,225 | | |
| C-933 | 8 | 600 | 833 | 1,320 | | |
| C-934 | 12 | 600 | 852 | 1,260 | | |
| C-935 | 14 | 650 | 864 | 1,240 | | |
| C-938 | 26 | 558 | 800 | 1,055 | | |
| C-962 | 26 | 766 | 982 | 1,150 | 1,290 | 2,550 |
| C-1091 | 13 | 693 | Not reached at 702 | | | |
| C-1102 | 5 | 575 | 750 | 1,100 | 1,350 | |
| C-1103 | 10 | 545 | 800 | 1,300 | | |
| C-1104 | 6 | 596 | 860 | 1,300 | 1,500 | 2,350 |
| C-1106 | 5 | 612 | 778 | | | |
| C-1107 | 14 | 639 | 870 | 1,270 | 1,540 | 2,220 |
| C-1111 | 10 | 560 | 750 | 1,240 | 1,485 | 2,210 |
| C-1112 | 27 | | | | 1,460 | 2,165 |
| C-1122 | 24 | 570 | 730 | 970 | | |
| C-1123 | 50 | 570* | 740* | 1,010 | 1,337 | 1,580 |
| C-1124 | 42 | 717 | 870 | 1,130 | 1,420 | 2,120 |
| C-1125 | 36 | 676 | 840 | 1,080 | 1,240 | 2,480 |
| C-1126 | 40 | 670 | 910 | 1,130 | 1,328 | 2,360 |
| C-1127 | 32 | 772 | 960 | 1,140 | 1,270 | 2,570 |
| C-1128 | 38 | | 920* | 1,200 | 1,450 | |
| C-1129 | 36 | | 900* | 1,130 | | |
| C-1130 | 56 | 651 | 790 | 1,120 | 1,403 | 2,180 |
| C-1131 | 47 | | 800* | 1,100 | | |
| C-1132 | 45 | 470 | 650 | 1,020 | | |
| C-1133 | 38 | 690 | 840 | | | |

| Local well identifier | Altitude measuring point (feet) | Depth to top of basal Hawthorn unit (feet) | Depth to basal contact of Hawthorn Group (feet) | Depth to top of Ocala Limestone (feet) | Depth to top of Avon Park Formation (feet) | Depth to top of dolomite- evaporite unit (feet) |
|-----------------------|--|---|---|--|--|--|
| CH-312 | 11 | 520 | 710 | | | |
| CH-313 | 22 | 447 | 720 | 1,250 | 1,580 | 1,970 |
| G-2296 | 17 | 775 | 980 | 980 | 1,128 | 2,440 |
| G-3239 | 25 | 838* | 1,050* | Not present | 1,155 | 2,550 |
| GL-240 | 25 | 613 | 805 | 850 | | |
| HE-281 | 29 | 609 | 910 | 980 | | |
| HE-282 | 40 | 747* | 1,040* | 1,160 | 1,390 | 2,300 |
| HE-343 | 54 | | | | | 2,010 |
| HE-941 | 48 | | 640* | 1,010 | 1,400 | 2,100 |
| HE-948 | 49 | | | | 1,409 | 2,060 |
| HE-949 | 53 | 520 | 800 | 1,050 | | 2,130 |
| HE-953 | 40 | 490 | 700 | 960 | 1,327 | |
| HE-970 | 45 | | | | | 2,280 |
| HE-973 | 40 | | | | | 2,260 |
| HE-976 | 39 | 689 | 830 | 1,151 | 1,426 | 2,370 |
| HE-981 | 32 | | 862 | 950 | | |
| HE-982 | 30 | | 950 | | | |
| HE-983 | 31 | 538 | 870 | 935 | | |
| HE-984 | 29 | 559 | 855 | 905 | | |
| HE-986 | 23 | 543 | 730* | 835 | | |
| HE-987 | 15 | | 790 | 860 | | |
| HE-1084 | 14 | 560 | Not reached at 622 | | | |
| HE-1085 | 25 | 620 | Not reached at 740 | | | |
| HE-1086 | 27 | | 930* | | | |
| HE-1087 | 15 | 611 | 780 | 780 | 1,010 | 2,060 |
| HE-1101 | 30 | 742 | 920 | 1,165 | 1,430 | |
| HE-1102 | 49 | | 930* | | | 1,990 |
| HE-1103 | 49 | 639* | 1,050* | 1,050 | | Not reached at 2,180 |
| HE-1104 | 49 | 532 | 960 | 1,060 | 1,290 | 2,310 |
| HE-1105 | 53 | 534 | 750 | 1,030 | 1,330 | |
| HE-1106 | 54 | 514 | 710 | 1,054 | 1,380 | 1,920 |
| L-550 | 4 | 418 | 690 | | | |
| L-755 | 22 | 434 | 748 | | | |

| Local well identifier | Altitude measuring point (feet) | Depth to top of basal Hawthorn unit (feet) | Depth to basal contact of Hawthorn Group (feet) | Depth to top of Ocala Limestone (feet) | Depth to top of Avon Park Formation (feet) | Depth to top of dolomite- evaporite unit (feet) |
|--------------------------|--|---|---|--|--|--|
| L-1018 | 13 | 446 | 853 | | | |
| L-1044 | 20 | 360 | 590 | | | |
| L-1094 | 5 | 648 | 962 | | | |
| L-1318 | 15 | 468 | 685 | | | |
| L-1396 | 20 | 334 | 648 | | | |
| L-1569 | 12 | 530 | Not reached at 809 | | | |
| L-1595 | 15 | 556 | 785 | | | |
| L-1688 | 30 | 442 | 790 | | | |
| L-1817 | 5 | 482 | 744 | | | |
| L-1903 | 15 | 350 | 537 | | | |
| L-1967 | 3 | 660 | 870 | | | |
| L-2061 | 30 | 682 | 815 | | | |
| L-2063 | 31 | | 815* | 1,300 | | |
| L-2458 | 25 | 420 | 640 | | | |
| L-2460 | 5 | 408 | 580 | | | |
| L-2657 | 9 | 486 | 720 | | | |
| L-2901 | 5 | 360 | 640 | | | |
| L-4817 | 21 | 380 | 570 | | | |
| L-4846 | 10 | 390 | 710 | | | |
| L-5000 | 40 | 475 | 870 | | | 1,670 |
| L-5001 | 53 | 673 | 815 | 1,175 | 1,380 | |
| L-5003 | 43 | | 786* | 1,190 | 1,450 | 1,920 |
| L-5009 | 47 | 537* | 802* | 1,120 | 1,450 | 1,900 |
| L-5010 | 42 | 525 | 650 | | | |
| L-5013 | 24 | 534* | | 1,206 | 1,420 | 2,120 |
| L-5601 | 5 | 400 | 720 | | | |
| L-5602 | 10 | 580 | 820 | | | |
| L-5605 | 27 | 455 | 740 | 1,200 | 1,500 | 1,950 |
| L-5608 | 16 | 473 | 823 | | | |
| L-5609 | 5 | 370 | 580 | | | |
| L-5615 | 5 | 490 | 750 | | | |
| L-5802 | 20 | 455 | 740 | 1,210 | 1,520 | 1,900 |
| L-6400 | 2 | 554 | 675 | | | |
| L-6401 | 11 | 467 | 789 | | | |

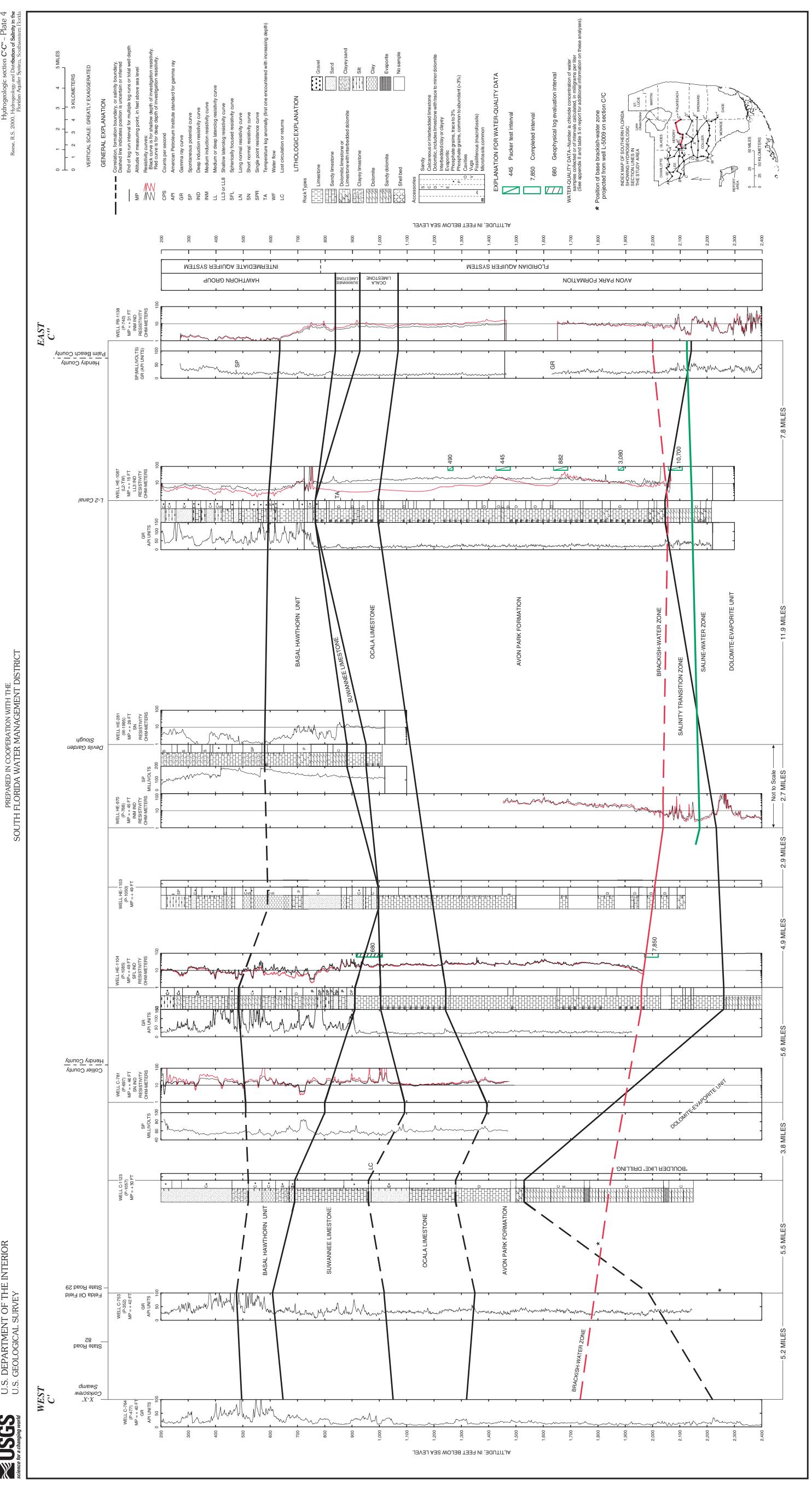
| Local well identifier | Altitude measuring point (feet) | Depth to top of basal Hawthorn unit (feet) | Depth to basal contact of Hawthorn Group (feet) | Depth to top of Ocala Limestone (feet) | Depth to top of Avon Park Formation (feet) | Depth to top of dolomite- evaporite unit (feet) |
|--------------------------|--|---|---|--|--|--|
| L-6411 | 4 | | 732* | | | |
| L-6412 | 3 | 390 | 518 | | | |
| L-6413 | 5 | | 840* | | | |
| L-6414 | 19 | 464 | 915 | | | |
| L-6415 | 43 | 568* | 750* | 1,113 | | |
| L-6417 | 3 | 340 | 710 | | | |
| L-6421 | 5 | 365 | 610 | | | |
| L-6423 | 5 | 608 | 755 | 1,225 | | |
| L-6435 | 2 | 402 | 860 | 1,220 | | |
| L-6436 | 3 | 423 | 720 | 1,050 | | |
| L-6437 | 6 | 488 | 820 | 1,120 | | |
| L-6439 | 18 | 428 | 730 | | | |
| L-6443 | 5 | 366 | 610 | | | |
| L-6444 | 15 | 380 | 770 | 1,170 | 1,570 | |
| L-6445 | 4 | 580 | 792 | 1,144 | 1,479 | |
| L-6461 | 46 | 646 | 830 | 1,170 | 1,460 | 1,920 |
| L-6462 | 38 | 496 | 705 | 1,085 | | |
| L-6463 | 45 | 593 | 800 | 1,205 | 1,470 | 2,104 |
| L-6471 | 5 | 273 | 730 | 1,050 | 1,360 | 1,740 |
| MO-141 | 25 | 895 | 1,110 | 1,270 | 1,390 | |
| PB-1137 | 32 | 707 | 932 | 932 | 1,112 | 2,330 |
| PB-1138 | 31 | 666 | 865 | 956 | 1,098 | 2,170 |
| PB-1163 | 12 | | | 840 | 1,020 | |
| PB-1164 | 18 | | 750* | 800 | | |
| S-479 | 18 | 853 | 1,060 | 1,115 | 1,150 | 2,560 |

HYDROGEOLOGIC SECTION A-A'

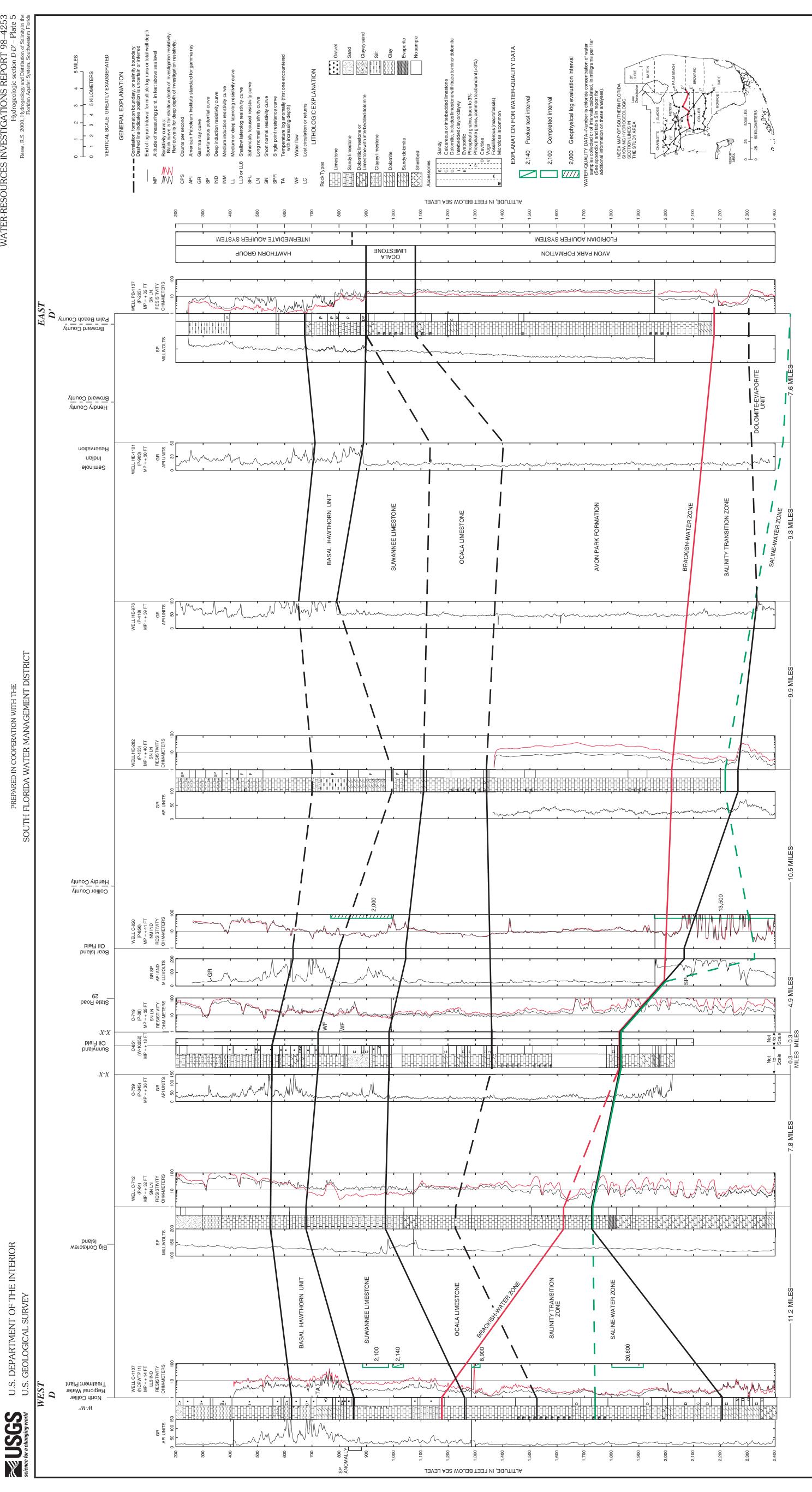
Secience for a changing world

B-B'HYDROGEOLOGIC SECTION Ronald S. Reese 2000

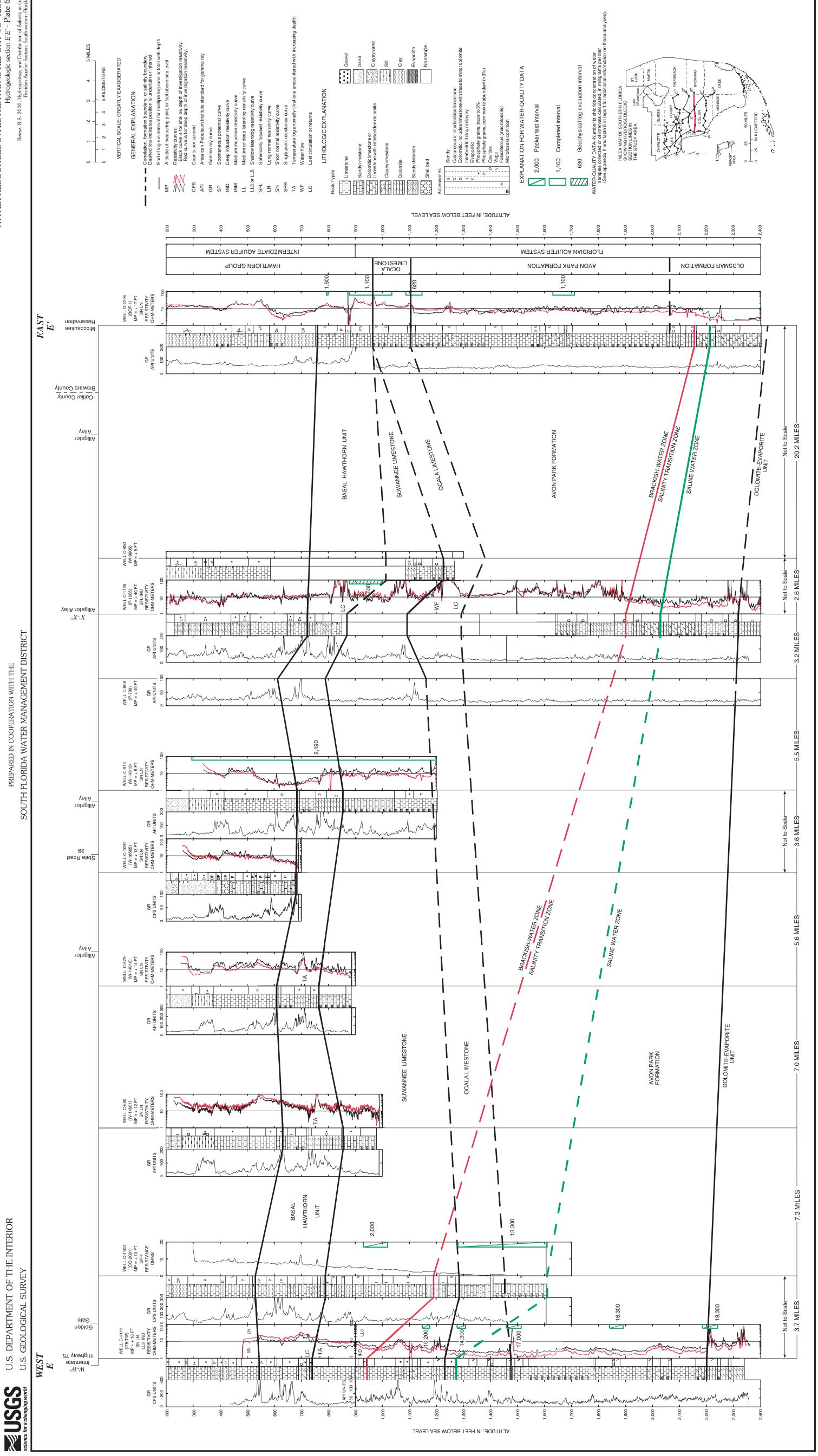
TION C-C' HYDROGEOLOGIC SECT By Ronald S. Reese 2000



HYDROGEOLOGIC SECTION By Ronald S. Reese 2000

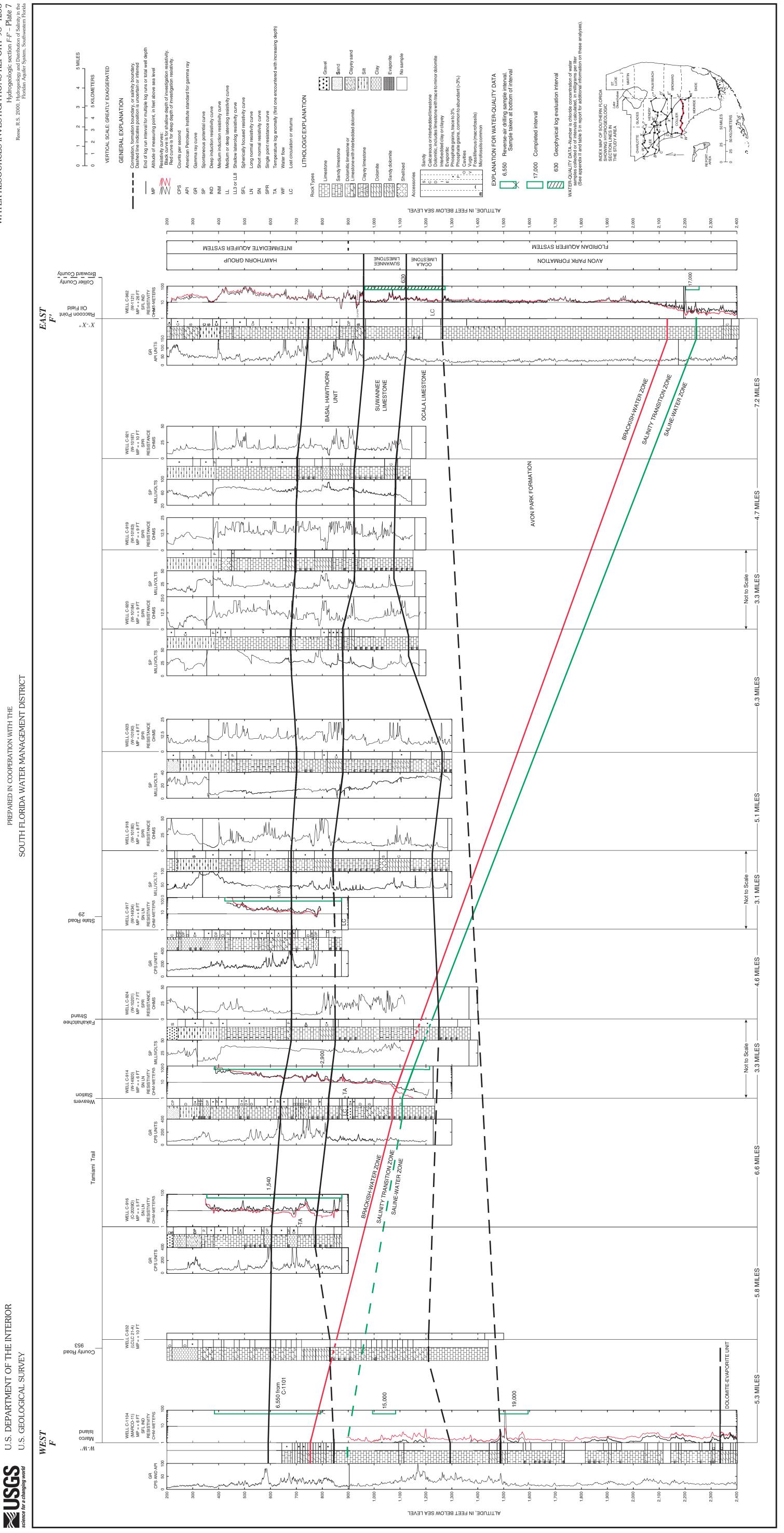


HYDROGEOLOGIC SECTION

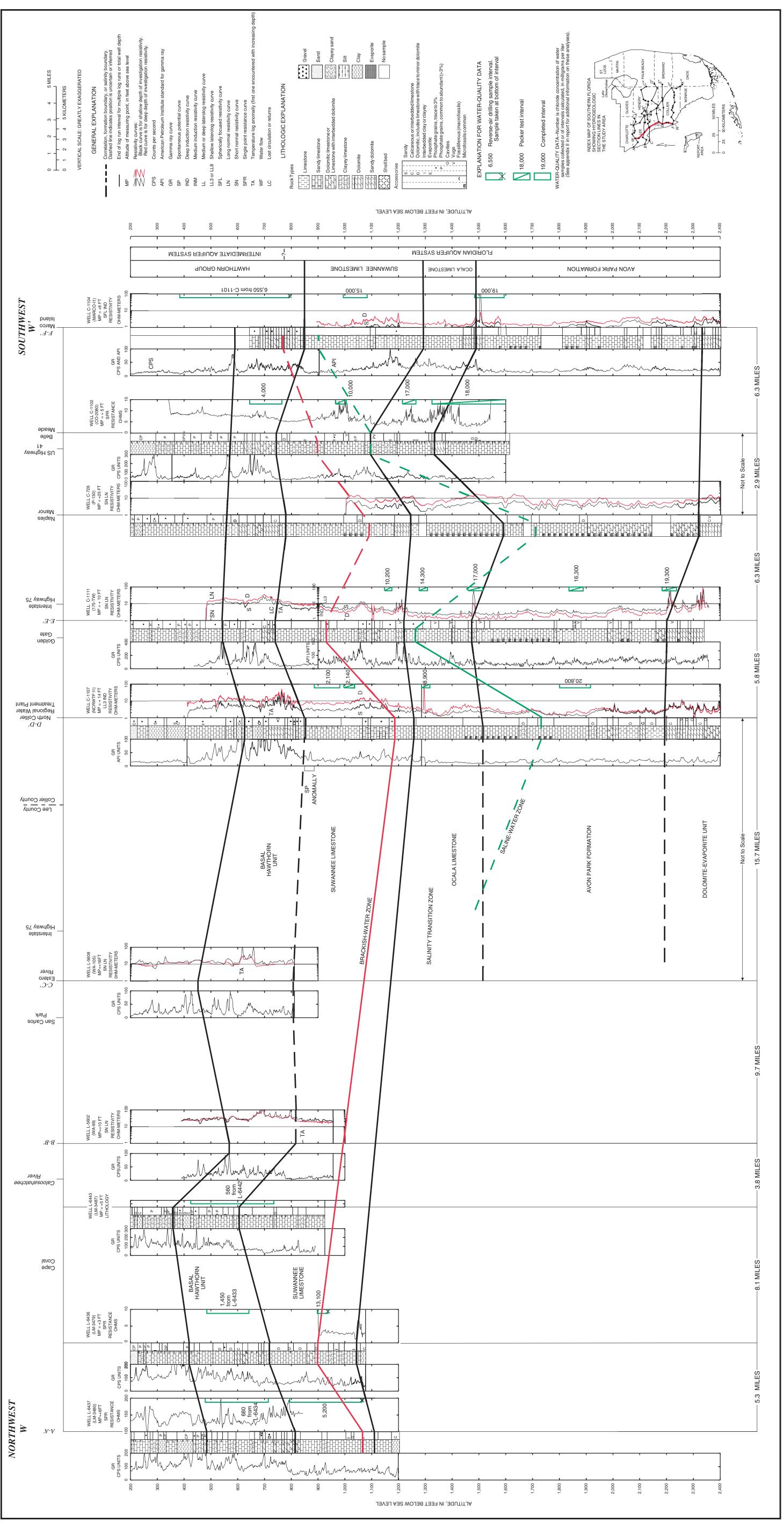


SECTION E-E' By Ronald S. Reese 2000 HYDROGEOLOGIC





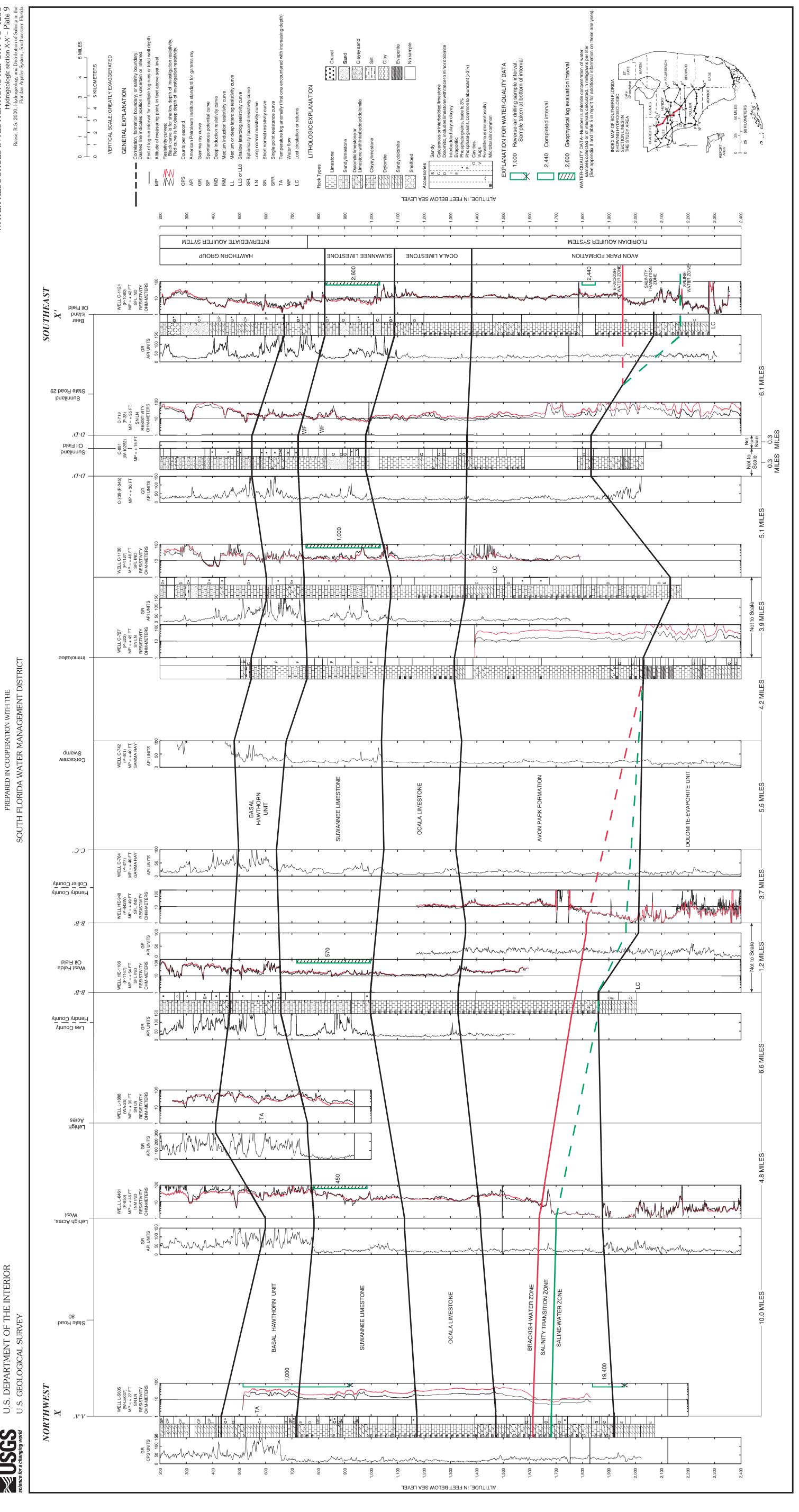
HYDROGEOLOGIC SECTION F-F By Ronald S. Reese 2000



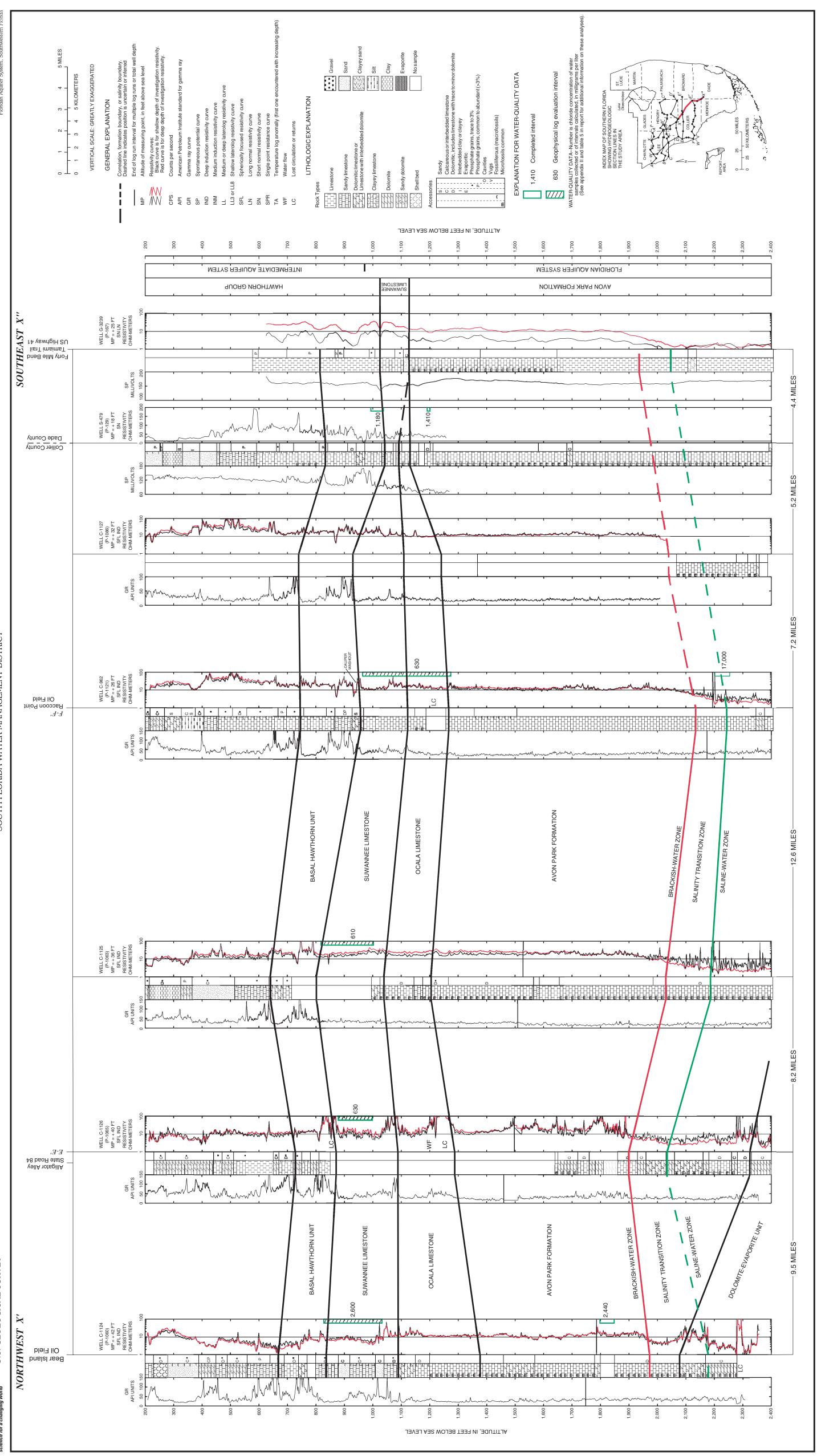
HYDROGEOLOGIC SECTION W-W'



PREPARED IN COOPERATION WITH THE SOUTH FLORIDA WATER MANAGEMENT DISTRICT



SECTION X-X' HYDROGEOLOGIC



X'-X''HYDROGEOLOGIC SECTION By Ronald S. Reese 2000