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Scheduled Civil Aircraft Emission Inventories for 1999: Database Development and Analysis

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Glossary

| AEAP | Atmospheric Effects of Aviation Project (NASA) |
|------------------|---|
| ANCAT | Abatement of Nuisances Caused by Air Transport |
| ASK | Available seat kilometer (the number of seats an airline |
| | provides times the number of kilometers they are flown) |
| BMAP | Boeing Mission Analysis Process |
| CAEP | ICAO Committee on Aviation Environmental Protection |
| CO | Carbon Monoxide |
| CO2 | Carbon Dioxide |
| DOE | United States Department of Energy |
| DOT | United States Department of Transportation |
| DLR | Deutsches Zentrum fuer Luft- und Raumfahrt |
| EI(CO) | Emission Index (grams CO/kg fuel burn) |
| EI(HC) | Emission Index (grams hydrocarbon/kg fuel burn) |
| EI(NOx) | Emission Index (grams NOx (as NO ₂)/kg fuel burn) |
| FRT | Freighter designator in schedule data |
| GAEC | Global Atmospheric Emissions Code |
| GE | General Electric |
| HC | Unburned hydrocarbons |
| H ₂ O | Water |
| ICAO | International Civil Aviation Organization |
| kg | kilogram |
| lb | pound |
| Load Factor | Percentage of an airplane's seat capacity occupied by |
| | passengers on a given flight |
| LTO cycle | Landing takeoff cycle |
| М | Mach number |
| MTOW | Maximum takeoff weight |
| NASA | National Aeronautics and Space Administration |
| NOx | Oxides of nitrogen (NO + NO ₂) in units of gram |
| | equivalent NO2 |
| OAG | Official Airline Guide |
| OEW | Operating Empty Weight |
| P&W | Pratt & Whitney |
| PAX | passengers |
| SO2 | Sulfur dioxide |
| TOGW | Takeoff gross weight |
| US | United States |
| 3-D | Three dimensional |

Scheduled Civil Aircraft Emission Inventories for 1999: Database Development and Analysis

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Executive Summary

This report describes the development of three-dimensional inventories of aircraft fuel burned and emissions (NOx, CO, and hydrocarbons) from scheduled air traffic for each month of 1999. The data are on a 1° latitude x 1° longitude x 1 km altitude grid. The data files were delivered to NASA electronically. These emission inventories were developed for the NASA Ultra Efficient Engine Technology (UEET) Program under contract NAS1-20341, Task Assignment 19. They will be available for use by atmospheric scientists conducting modeling studies on the atmospheric effects of aviation, including the NASA Global Modeling Initiative (GMI).

Emissions produced by the world's entire aircraft fleet come from scheduled, military, charter and general aviation air traffic. In this report, we present only the results and methodology used for the calculation of emissions from scheduled air traffic which includes turboprops, passenger jets, and jet cargo aircraft.

Global fuel use for 1999 by scheduled air traffic was calculated to be 1.28×10^{11} kilograms. Global NOx emissions by scheduled air traffic in 1999 were calculated to be 1.69×10^{9} kilograms (as NO₂). Calculated global emissions show a seasonal variation, peaking in August with a minimum in February. Emissions for the month of December 1999 were closest to global annual average emissions, although emissions for May (the month typically used as an 'average' month in past NASA inventory studies) were within 1 percent of the global annual average.

A trend analysis for emissions and fuel burned was performed using the results of this current work and previously published emission inventories and scenarios. This analysis showed an increase in the absolute amount of fuel burned, distance traveled, NOx, and CO emissions produced by the scheduled fleet between 1992 and 1999 and a decrease in the absolute amount of hydrocarbon emissions produced. Calculated global fuel use increased by 33% and NOx emissions increased by 35% between 1992 and 1999. The analysis

also showed that scheduled fleet fuel burned and NOx emissions normalized by available seat kilometers decreased between 1992 and 2015.

The methodology used to extract and process air traffic data from the Official Airline Guide was changed from that used to calculate previous scheduled fleet inventories for 1976, 1984 and 1992. To quantify the effects of the methodology changes, an emission inventory for August 1992 was recalculated using the new methodology. Comparisons between the previously published and new August 1992 inventories show good agreement for global fuel burned and NOx totals. For CO and hydrocarbons, the global totals increased by 20 percent and 18 percent respectively with the use of the new methodology. Much of this difference arises from changes in the selection of combustor types for certain engines in the fleet. Hydrocarbon and CO emissions levels for many older technology engines can vary widely depending on the combustor used in the engine.

To improve the accuracy of global emissions calculations for freighters, United States Department of Transportation Form T-100 data was used to determine typical payloads for freighter aircraft. This information was then used to model freighter aircraft more accurately in the inventory calculations by using more realistic payloads.

To assess the effect of the different freighter payload assumptions, results were compared with previous inventory calculations done using 70 percent passenger payload for all aircraft. This comparison showed that improved freighter payload assumptions increased total global fuel burned by 0.6 percent and increased total global NOx by 1.5 percent for August 1999. These increases are relatively small and will not significantly change trends for fuel use or NOx created using the published inventories for 1976, 1984, and 1992.

In order to evaluate the 1999 scheduled aircraft fleet global emission inventory calculations, comparisons were made with aviation fuel use and traffic data reported on the U.S. Department of Transportation (DOT) Form 41 by US air carriers. In general, emission inventory calculations of departures and distance traveled for 1999 compared well (within 5 percent) with the DOT Form 41 data for the ten largest passenger carriers that reported fuel use and traffic data to the DOT. In contrast, for the four largest cargo carriers reporting to the DOT, calculated departures and distance traveled were significantly less than those reported. It appears that the OAG flight schedule data do not contain a complete listing of cargo flights.

For the passenger carriers in the DOT Form 41 data comparison, the emission inventory calculations consistently under-predicted fleet fuel burned. The magnitude of these under-predictions varied depending on the carrier being considered. For the ten largest air carriers reporting data to the DOT, the total fuel burn was under-predicted by 21 percent. This result is likely due to the simplifying assumptions used in the development of the global inventory, including our inability to consider air traffic control delays/diversions, weather/wind factors, more realistic routing, less than optimum aircraft/engine performance and actual aircraft operating weights.

1. Introduction

The NASA Ultra Efficient Engine Technology (UEET) program has been initiated to promote the development of fuel efficient and low NOx emissions jet engines for the future and to evaluate the effects of aircraft emissions on the atmosphere and human health. The work described herein was done in support of the UEET program Environmental Impact Assessment Element (WBS 1.2) which includes atmospheric modeling, health risk assessment, and emission characterization work. The creation of global emission inventories for the scheduled aircraft fleet as a function of altitude and geographical position (referred to as "3-D emission scenarios") is an important component of the atmospheric modeling portion of this element. These scenarios are used as the input to chemical transport models to evaluate the effect of aircraft emissions: how long they persist in the atmosphere, how much they perturb the chemistry or microphysics of the upper troposphere, and how they compare with other sources of NOx, water, soot, and condensation nuclei in the upper troposphere.

In previous NASA studies funded under the High Speed Research and Advanced Subsonic Technology programs, we have developed 3-D emission scenarios for aircraft fleets for 1976, 1984 and 1992 (Baughcum, *et al.*, 1996a and 1996b), and have projected 3-D emission scenarios of both subsonic and supersonic traffic for 2015 (Baughcum, *et al.*, 1998; Baughcum and Henderson, 1998). ANCAT and DLR have also published historical 3-D emission inventories and projections for 2015 (Schmitt and Brunner, 1997; Gardner, 1998). The emission scenario work of NASA, ANCAT and DLR has been compared and contrasted in the *Intergovernmental Panel on Climate Change Special Report on Aviation and the Global Atmosphere* (Henderson, *et al.*, 1999).

The NASA-funded work as well as that of ANCAT and DLR has used a "bottoms-up" approach in which aircraft schedules are obtained or estimated and the aircraft/engine combinations in these schedules are identified. Detailed calculations of fuel burned and emissions are then made along each flight path and the results are distributed over a 3-dimensional global grid space.

Emissions produced by the world's entire aircraft fleet come from scheduled, military, charter and general aviation air traffic. In this report, we present the results and methodology used for the calculation of emissions from scheduled air traffic, including turboprops, passenger jets, and jet cargo aircraft. In 1992, fuel usage for scheduled air traffic accounted for approximately 68% of the fuel usage of the entire aircraft fleet. The scheduled air traffic inventories presented in this report are calculated using the Official Airline Guide (OAG) as the source of scheduled flight data. The OAG accurately accounts for scheduled passenger flights in most regions of the world but it is unclear to what extent it covers cargo flights and flights within China and the former Soviet Union.

This report documents an emission inventory for only the 1999 scheduled aircraft fleet. In order for a complete emission inventory for the world's entire 1999 aircraft fleet to be created, the 3-D scheduled inventory documented in this work would need to be combined with 1999 3-D inventories of the military, charter and general aviation components of the world's fleet. Such inventories were developed earlier for 1976, 1984, 1992 and 2015 (Landau, *et al.*; 1994, Metwally, 1995; Mortlock and Van Alstyne, 1998). In addition, 3-D inventory calculations for year 1999 flights within the former Soviet Union and People's Republic of China not included in the OAG schedule would have to be included if it is determined that the OAG schedule is incomplete for these regions. As of the writing of this report, these additional inventories have not yet been developed for 1999.

To calculate scheduled aircraft fleet inventories, flight schedule data (number of departures for each city pair along with airplane and engine type) are combined with performance and emissions data to calculate fuel burned, oxides of nitrogen (NOx), carbon monoxide (CO), and total hydrocarbons (HC) on a 1° longitude x 1° latitude x 1 kilometer altitude grid. The results for all the different routes and airplane/engine combinations are then summed to produce the total inventory. The details of this process are described in Section 2 of this report.

Results of the 1999 scheduled aircraft fleet emission inventory calculations are analyzed and discussed in Section 3 of this report. The methodology used to create this inventory was changed in a number of ways from that which was used to calculate previously published NASA scheduled aircraft emission inventories. In order to assess the effects on inventory results of changes made to the calculation methodology, an emission inventory for August 1992 was calculated using the same methodology used to calculate the 1999 scheduled inventory. The results of this calculation were then compared to results of the previously published NASA August 1992 inventory calculations (Baughcum, *et al.*, 1996a). This comparison is documented in Section 2.5 of this report. The calculation of the August 1992 inventory using the current methodology is also utilized in Section 3.4 of this report to develop a self-consistent trend analysis of fuel use and emissions.

In the current work, improved modeling of freighter aircraft performance was utilized to improve the overall accuracy of global emissions calculations. A discussion of these improvements is presented in Section 2.3.3 and results of their implementation are presented in Section 3.5. The work described in this report was conducted under NASA Contract NAS1-20341, Task 19. The NASA Glenn Research Center Task Manager was Chowen C. Wey.

The principal investigator was Steven L. Baughcum. Donald J. Sutkus extracted aircraft departure data from the Official Airline Guide and assigned engines to aircraft types listed in the schedule using the Boeing proprietary computer code "The Emissions Desktop Flight Schedule Creation Module" (TED/FSCM). Donald J. Sutkus also calculated the 3-dimensional aircraft emission inventories using the Boeing proprietary Global Aircraft Emissions Code (GAEC). Douglas P. DuBois provided guidance on the selection of appropriate performance aircraft and emissions engines characteristics to use when modeling aircraft in the inventories and Steven J. Moskalik and Daniel Wajerski provided data to update the aircraft performance database used in the inventory calculations. The TED/FSCM code used to process flight schedule data was written by David F. Tankersley and the GAEC code used to calculate the aircraft emission inventories was written by Peter S. Hertel. The analysis of the results was completed by Steven L. Baughcum, Donald J. Sutkus and Douglas P. DuBois.

2. Database Development Methodology

The calculation of emission inventories has been described previously (Baughcum, *et al.*, 1994; Baughcum, *et al.*, 1996) and will be briefly summarized here. The overall process is shown schematically in Figure 2-1.

Global Emissions Database Calculation Schematic

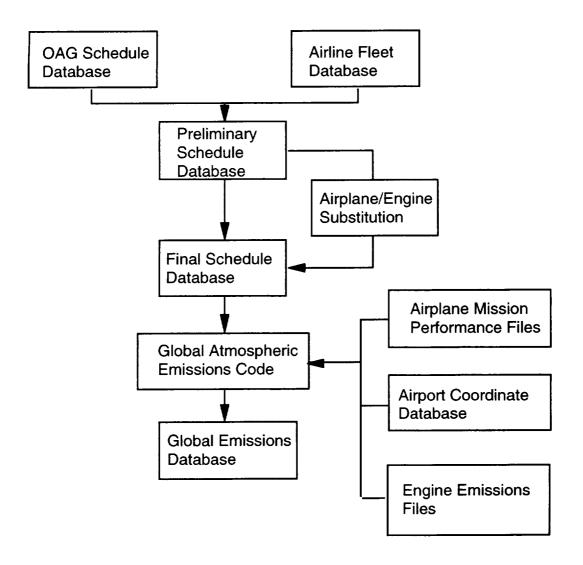


Figure 2-1. Schematic of emission inventory calculation.

2.1 Database Acquisition and Description

The projected flight schedule data used to create the twelve month 1999 global emission inventory for the scheduled aircraft fleet were purchased by The Boeing Company from Official Airline Guide (OAG) (Oakbrook, IL) for four months (January, April, July and October). OAG data purchased in January include schedule forecasts for February, March, and April. The OAG schedule data contain listings of every scheduled jet and turboprop flight by city-pair and airline, and include departure and arrival times, airplane code, and trip frequency projected for several months into the future. This data are processed to create standard flight schedule databases that are used in a variety of airline and airplane studies within The Boeing Company. OAG flights for the 16th through the 22nd of each month were used to represent the entire month in this study. Fuel burned and emissions calculated in this study for this seven day period were divided by seven and multiplied by the number of days in the month to obtain monthly totals.

The coverage of the OAG database depends on schedule data submitted by individual airlines. While it is quite accurate overall, changes in airline planned operations during any month or operations not reported by the airline as part of their schedule are not included. The 1999 OAG did not include charter flights, military flights, general aviation flights and full coverage of freighter flights. In addition, Boeing analysis shows that the 1999 OAG under predicted scheduled air traffic by approximately 25 percent for China and approximately 30 percent for the former Soviet Union (on an available seat kilometer basis). The majority of the under prediction in China and the Soviet Union is for smaller jet aircraft.

The emission inventory calculations reported previously for the 1992 scheduled fleet (Baughcum, *et al.*, 1996a) used published schedule data obtained monthly directly from OAG. For the 1999 scheduled fleet inventory calculations, however, the OAG database normally used by Boeing, which is updated quarterly, was utilized. This means that projections of flight schedule data up to three months into the future were utilized in creating the 1999 scheduled fleet inventory.

In order to evaluate the effect of using schedule data projected for multiple months into the future, scheduled emission inventories for May 1999 were created using both one-month and four-month (from the previous quarter's OAG) projections. The 4-month projection was a longer-range forecast than was actually used in developing the 1999 monthly inventories. Table 2-1 compares the fuel burned, flight distance, and emissions for selected geographical regions for the one month and four month projections. Globally, fuel burned was under predicted by about 1% and distance by 1.7% by the 4-month projection. NOx, CO, and hydrocarbon emissions were also under predicted globally by the four month projection by approximately 1%. Discrepancies between results of the two projection methods are slightly greater in the Southern Hemisphere than those in the Northern Hemisphere. In the Southern Hemisphere, air traffic appears to have been over predicted by the 4-month projection while air traffic in the Northern Hemisphere was under predicted slightly by the four month projection.

The agreement between the one month and four month projections is within 1-3% for the US, North America, North Atlantic, and North Pacific for fuel burned, distance and emissions, with traffic (flight distance) increasing faster than projected by the 4-month projection. Air traffic in Europe also grew faster than expected from the 4-month projection but the under-prediction was slightly larger (4.5%) than the regions mentioned above. The most dramatic discrepancy is for China where the 4-month projection under-predicted the fuel use by 6% and the flight distance by 10%. The effect on global emissions of this discrepancy is relatively minor though considering that China is responsible for only 4% on global fuel burned (see Table 3-2).

When the one-month and 4-month projections are compared on an airplane by airplane basis, some differences are clearly evident. In general, these manifest themselves as under prediction of fuel use by airplanes which were currently in production (e.g., Boeing 737, Boeing 777, Boeing 757, Airbus A310, Airbus A319, and McDonnell Douglas MD-90), and over prediction of older aircraft (e.g., McDonnell Douglas DC-10, McDonnell Douglas DC-8, Lockheed L-1011). These effects are probably due to retirements, changes in utilization, and introduction of new airplanes.

Overall, from the perspective of using the aircraft emission inventories in global atmospheric modeling assessments, the errors associated with using projections based on quarterly data seem small and acceptable.

An airport listing is needed to calculate global emissions and fuel burn for the scheduled fleet using the OAG schedule. For each three-letter airport code listed in the OAG schedule, the airport listing gives the city name and position (latitude, longitude, and altitude) of the airport. Three-letter airport codes that have been 'retired' either because the airport they used to represent no longer exists or because a different code has been assigned to that airport may be reused by the OAG. For this reason, an airport listing corresponding to the specific month and year for which the inventory calculation is being done must be used when making inventory calculations. Table 2-1.Regional changes in May 1999 global scheduled fleet emission
inventory calculation results due to use of a 4-month projection
of OAG flight schedule data instead of a one month projection
(positive percent difference denotes an over-prediction by the
4-month projection).

| | Global | Northern Hemisphere | Southern Hemisphere |
|--------------|---------------|------------------------|------------------------|
| | <u>uiobui</u> | | |
| Fuel burned | -0.9% | -1.2% | 2.8% |
| NOx | -1.0% | -1.4% | 3.1% |
| со | -1.1% | -1.5% | 3.5% |
| Hydrocarbons | -0.6% | -1.1% | 4.4% |
| Distance | -1.7% | -2.0% | 1.8% |

| | US | Europe | North America | North Atlantic | North Pacific | China | Far East |
|--------------|-------|--------|------------------|-------------------|------------------|--------|-------------|
| Fuel burned | -1.1% | -2.8% | -1.2% | 0.3% | -1.5% | -6.3% | -1.1% |
| NOx | -1.9% | -2.2% | -1.8% | 0.3% | -1.5% | -5.2% | -1.7% |
| CO | -0.4% | -2.6% | -0.5% | -0.3% | -1.1% | -8.5% | 0.5% |
| Hydrocarbons | -0.2% | -3.3% | -0.4% | -2.8% | -0.4% | -2.6% | 6.1% |
| Distance | -0.9% | -4.5% | -1.0% | 1.1% | -1.8% | -10.0% | -2.6% |

2.2 Data Extract Challenges

The OAG database is designed for the purpose of travel itinerary planning by airline passengers and travel agents. As a result, certain duplicate listings of the same actual flight segment may occur in the schedule data and legs of trips using transportation modes other than air travel may also be listed. While nonaircraft trip legs are tagged in the database and easily filtered, duplicate listings are not noted explicitly in the database. Logic must be built into an extract code to eliminate these duplications as much as possible.

The logic used to eliminate duplicate flight listings in this study differed from that used in past NASA scheduled inventory studies (Baughcum *et al.*, 1996a and 1996b). The new approach is much more automated, requires less expert judgment by the analyst, and is very reproducible. In order to determine the effect of these differences, a schedule for August 1992 was extracted using

the new duplicate removal scheme and compared to the August 1992 schedule used to generate the previously published NASA 1992 scheduled inventory. Differences between the two schedules were minimal and judged to be insignificant.

The flight duplications which must be eliminated fall into three main categories, which we term "Codeshare Duplication", "Starburst Duplication" and "Effectivity Duplication". A description of each of these three categories is given below.

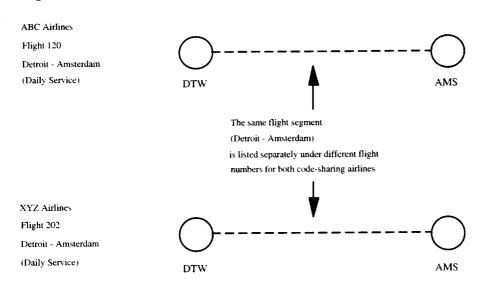


Figure 2-2. "Codeshare" flight duplication.

"Codeshare Duplication"

This form of schedule duplication occurs when both airlines involved in a cooperative flight sharing arrangement (codesharing) will list the same flight segment under their own airline code and flight number. This results in the flight being listed twice in the OAG schedule, once under each airline's name. For instance, the same flight from Detroit to Amsterdam may be listed under both ABC Airlines and XYZ Airlines. Codeshare duplications are removed by checking for flights that are listed under two different airlines, but with the same airport-pair, time of day departure and arrival, same day and same equipment (See Figure 2-2).

A provision to retain certain known "head to head" competition flights was made in the codeshare duplication removal logic. "Head to head" flights are those flights where two airlines have directly competing flights between the same airport-pair with the same departure and arrival times on the same day with the same equipment.

"Starburst Duplication"

This form of duplication arises from the practice of airlines listing under separate flight numbers one-stop or multi-stop itineraries that contain the same flight segment. As a simple example of this practice, an airline listing a one-stop flight from Cleveland to London through New York and another one-stop flight from Washington to London through New York will combine the passengers from both flight numbers on the same New York - London flight segment. The published schedule, however, would lead one to believe that there are two separate flights from New York to London. This duplication is removed by checking flight itineraries for segments listed under the same airline, airport-pair, time of day departure and arrival, same day and equipment. (See Figure 2-3)

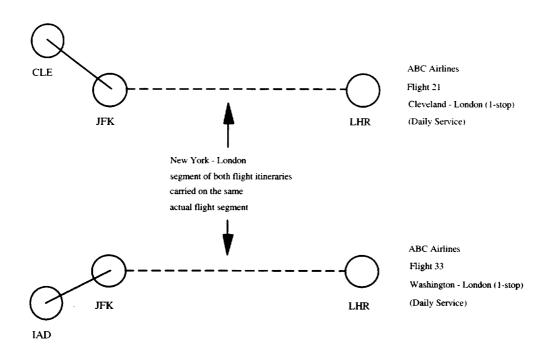
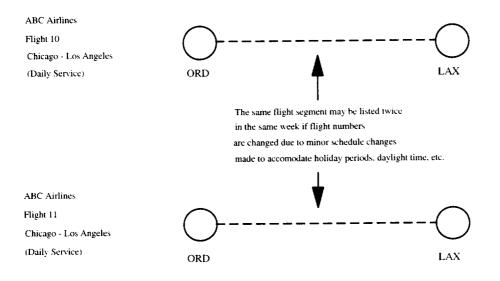


Figure 2-3. "Starburst" flight duplication.





"Effectivity Duplication"

Although the OAG schedule data are supplied as representing the airline schedules for a certain month, data within the schedules show the dates at which flights cease operation or begin operation within the month. The flight data show which days of the week the flight operates. If every flight that operates in a given week is counted, then the same flight segment may be counted twice as airlines change schedules (and flight numbers) within the week to account for holidays, daylight time, change of airplane type, etc. This duplication can be removed by choosing a single date for flight effectivity, rather than a whole week. All flights effective on the 16th day of the month are included in the analyses presented here. (See Figure 2-4)

Once the logic to remove the types of duplicate flights noted above was in place and tested, a complete set of schedules was extracted for each month of 1999 and August of 1992.

2.3 Creation of the Emissions Database:

2.3.1. Schedule Data Translation

Each flight listing in the monthly airline schedules extracted from the OAG database gives the airline, the airplane type, the origin airport, the destination airport and the number of times the flight is scheduled to fly between the specified airport pair in a one week period. The following is an example of a typical OAG flight database listing:

| <u>Airline</u> | <u>Airplane</u> | <u>Origin</u> | Destination | Weekly Freq. |
|----------------|-----------------|---------------|--------------------|--------------|
| JL | 74F | ANC | ATL | 3 |

In order to calculate performance and emissions for a particular flight, the specific type of engine installed on the aircraft must be known. The OAG database flight listings do not contain information about engines installed on an aircraft used for a particular flight. In order to assign engines to flights listed in the OAG database, a fleet information database purchased from the Airclaims Company was used. This database provides a comprehensive listing of the aircraft owned by each of the world's airlines and the engines installed on them. This database differs from the Boeing internal fleet information database that was used to produce previous NASA emission inventories. The database used previously is now out of date and is no longer maintained by Boeing.

A Boeing proprietary computer code was used to automate the process of assigning engines to flights listed in the OAG database using airline fleet information contained in the Airclaims database. Engines were assigned to flights listed in the OAG database using a "majority rules" criteria where the most prevalent engine used in the given airline's fleet on the given airplane type was assigned to the flight.

To illustrate how the Airclaims Database was used to assign engines to flights listed in the OAG schedule database, we will build an example using the sample OAG database flight listed above.

OAG airplane and airline codes are different than Airclaims airplane and airline codes and so airplane and airline code translation tables were necessary to link the two databases. For illustration purposes, simplified airplane and airline translation tables relevant to the current example are shown in Tables 2-2 and 2-3.

| Table 2-2. | Sample OAG to Aircla | ims airline code translation table. | |
|------------|----------------------|-------------------------------------|--|
| | OAG Airline Code | Airclaims Airline | |
| | | Code | |
| | JL | JAL | |

| Table 2-3. | Sample O | AG to | Airclaims | airplane | translation | table. |
|------------|----------|-------|-----------|----------|-------------|--------|
|------------|----------|-------|-----------|----------|-------------|--------|

| OAG Specific Aircraft Code | Airclaims Aircraft Type | Airclaims Aircraft Variant | Airclaims Aircraft Usage |
|-------------------------------|----------------------------|-------------------------------|-----------------------------|
| 74F | 747 | 200F (SCD) (P&W) | All Freight-Cargo |
| 74F | 747 | 200F (P&W) | All Freight-Cargo |
| 74F | 747 | 200SF (P&W) | All Freight-Cargo |

For the current example, using an airline code translation table (like that in Table 2-2), the OAG airline code "JL" would be translated to the Airclaims airline code "JAL". Using the airplane code translation table (like that in Table 2-3), the OAG airplane code "74F" would be translated to the following three possible Airclaims aircraft type/aircraft variant/aircraft usage names: "747/200F (SCD) (P&W)/All Freight-Cargo", "747/200F (P&W)/All Freight-Cargo" and "747/200SF (P&W)/All Freight-Cargo".

Appendix A contains a sample listing from the Airclaims database for the Japan Airlines fleet as it existed on May 16th 1999. Using the "translated" Airclaims airline code and aircraft type/aircraft variant/aircraft usage names along with this Airclaims database sample listing, we find that the 747-200F (SCD) (P&W)/JT9D-7Q aircraft/engine combination is the one that has the largest representation in the Japan Airlines fleet of all combinations corresponding to the OAG schedule's 74F code. Therefore, by use of the "majority rules" criterion, the 747-200F (SCD) (P&W)/JT9D-7Q aircraft/engine combination would be assigned to the sample OAG flight. The "(SCD)" and "(P&W)" would then be stripped from the Airclaims aircraft variant name because they contain no useful information for the inventory calculation process.

With the above process being completed, the OAG listed flight with the new engine assigned using the Airclaims database would be as follows:

| <u>Airline</u> | <u>Airplane</u> | Engine | <u>Origin</u> | Destination | Weekly Freq. |
|----------------|-----------------|---------|---------------|--------------------|--------------|
| JL | 747-200F | JT9D-7Q | ANC | ATL | 3 |

Once aircraft performance data and engine emissions data are assigned to the above flight, the emissions for the flight can be calculated.

The make-up of the world's airline fleet is always changing. For this study, a "snapshot" of the Airclaims database as it existed on the 16th of each month was used when performing the schedule data translation. The 16th of the month was chosen in order to coincide with the effectivity date of the OAG schedule data.

2.3.2. Airplane/Engine Performance Data Substitution

In some cases, it was necessary to substitute one type of aircraft/engine combination for another in the translated schedule created using the process described in Section 2.3.1 above. While Boeing has performance information needed to calculate fuel burned for a large number of turbojet-powered airplane types, including all Boeing models and many non-Boeing models, we do not have such information for all airplane types in airline service. For some of these airplane types, performance data for a similar airplane were used to approximate fuel burned. The airplane type in the following flight is an example:

| <u>Airline</u> | <u>Airplane</u> | <u>Engine</u> | <u>Origin</u> | Destination | Weekly Freq. |
|----------------|-----------------|---------------|---------------|--------------------|--------------|
| IT | Mercure | JT8D-9 | PAR | LYS | 21 |

Boeing does not have enough detailed information on the Dassault Mercure to calculate fuel burned or emissions on this flight. The Mercure is a twin-engined aircraft of similar size to the 737-200, and is powered by the same engines as some of the 737-200 models. The data for this flight can therefore be revised to:

| <u>Airline</u> | <u>Airplane</u> | Engine | <u>Origin</u> | Destination | Weekly Freq. |
|----------------|-----------------|--------|---------------|--------------------|--------------|
| IT | 737-200 | JT8D-9 | PAR | LYS | 21 |

For the RJ-85, RJ-100 and Fokker 70 aircraft types, no aircraft were present in the Boeing performance database that had performance characteristics similar enough to make a reasonable direct substitution. For these aircraft types, the performance characteristics of larger aircraft of the same general type were scaled to provide a reasonable performance estimate.

For emission calculation purposes, all of the myriad turboprop models that existed in the 1999 OAG database were grouped into three categories, small, medium and large. The "small" category includes airplanes such as the DeHaviland Twin Otter, the "medium" category includes airplanes such as the DeHaviland Dash-8, and the "large" category includes airplanes such as the Fokker F-27 and F-50. In addition, performance of all of the various types of regional jets was modeled using a single general regional jet performance model.

Appendix B contains a listing of all the airplane types appearing in the processed 1999 OAG data and the performance airplanes used to model each type in the emissions calculations. For 1999, the number of different airplane/engine combinations listed in the flight schedule data files varied between months from 369 to 387. These airplane/engine combinations were modeled using 89 airplane/engine combinations for which detailed performance and emissions data were available. A list of the 89 performance airplanes used to model the 1999 fleet is shown in Table 2-4.

The number of different airplane/engine combinations listed in the 1999 flight schedule data is considerably higher than the 228-235 different airplane/engine combinations appearing in the flight schedule data for the 1992 NASA inventory. This is partly due to the introduction of new airplane types into the fleet since 1992 and partly because the new process used to create the flight schedule data for the 1999 inventory extracts airplane types at a more detailed level. List of airplane-engine combinations used in airplane performance calculations for the 1999 emission Table 2-4.

| | inventory. | | | | | | |
|---------------|-----------------|-----------|---------------|-----------------|-----------------|------------------|-------------|
| Airplane | Engine | Airplane | Engine | Airplane | Engine | Airplane | Enaine |
| | | | | | | | 8 |
| 707-320B-C | JT3D-3B | 747-300 | RB211-524D4UP | 777-300 | TRENT892 | DC-8-63-63CF | JT3D-7 |
| 727-100 | JT8D-7 | 747-300F | CF6-50E2 | A300-600R | CF6-80C2 | DC-8-71-71CF | CEM56-1R |
| 727-100 | JT8D-9 | 747-400 | CF6-80C2-B1F | A300-621R-ER | JT9D-7R4H1 | DC10-10 | CF6-6D |
| 727-200 | JT8D-15-15A | 747-400 | PW4056 | A300-622R-ER | PW4056 | DC10-10F | C.F6-6D |
| 727-200 | JT8D-9 | 747-400 | RB211-524G | A300-B2-B4 | CF6-50C2 | DC10-40 | 00-UDI. |
| 727-200F | JT8D-15-15A | 747-400F | CF6-80C2B1F | A310-300 | CF6-80A3 | DC8-55-55CF | JT3D-3B |
| 737-100 | JT8D-9 | 747-400F | PW4056 | A310-300 | CF6-80C2A2 | DC9-30 | JTBD-7 |
| 737-200 | JT8D-15 | 747-400F | RB211-524H | A310-300 | JT9D-7R4E1 | DC9-31 | JT8D-15 |
| 737-200 | JT8D-7 | 747SP | JT9D-7A | A319 | CFM56-5B3P-25 | DC9-50 | JT8D-15 |
| 737-200ADV | JT8D-9-9A | 747SP | RB211-524C2 | A319-200 | CFM56-5-A1 | F-28-4000 | MK555-15H |
| 737-300 | CFM56-3-B1 | 757-200 | PW2037 | A319-200 | V2522-A5 | FOKKER-100 | TAY-650 |
| 737-500 | CFM56-3-B1-18.5 | 757-200 | PW2040 | A320-200 | CFM56-5-A1 | FOKKER-70 | MARK-620-15 |
| 737-600 | CFM56-7B18 | 757-200 | RB211-535C | A320-200 | CFM56-5B3P-26.5 | L-1011-1-100 | RB211-22B |
| 737-700 | CFM56-7B20 | 757-200 | RB211-535E4 | A320-200 | V2525-A5 | L-1011-1-100F | RB211-22B |
| 737-800 | CFM56-7B24 | 767-200 | CF6-80A | A321-100 | CFM56-5B1 | L1011-500AC | RB211-524B4 |
| 737-800 | CFM56-7B27 | 767-200 | JT9D-7R4D | A321-100 | V2530-A5 | MD-11 | CF6-80C2D1F |
| 747-100-100SR | CF6-45A2 | 767-200ER | CF6-80C2B4F | A321-200 | V2533-A5 | MD-11ER | PW4460 |
| 747-100-200 | CF6-50E2 | 767-200ER | PW4056 | A330-200 | CF6-80E1A3 | MD-11F | CF6-80C2D1F |
| 747-100-200 | JT9D-7A | 767-300 | CF6-80A2 | A330-200 | PW4168 | MD-11F | PW4460 |
| 747-100F | JT9D-7F | 767-300 | JT9D-7R4E | A330-200 | TRENT72 | MD-82 | JT8D-217A |
| 747-200 | JT9D-7J | 767-300ER | CF6-80C2B6F | A330-300 | CF6-80E1A1 | MD-83 | JT8D-219 |
| 747-200 | JT9D-7R4G2 | 767-300ER | PW4060 | A330-300 | PW4164 | MD-87 | JT8D-217C |
| 747-200 | RB211-524C | 767-300ER | RB211-524H | A330-300 | TRENT768 | MD-95-30 | BR715 |
| 747-200 | RB211-524D4U | 777-200 | PW4084 | A340-200 | CFM56-5C-2 | MD90-30 | V2525-D5 |
| 747-200B-C-F | JT9D-7Q | 777-200 | TRENT877 | BAC111-500 | MK512-14 | RJ-100 | LF507 |
| 747-200F | JT9D-7J | 777-200ER | GE90-85B | BAE146-200 | ALF502R-5 | RJ-85 | LF507 |
| 747-200F | RB211-524D4 | 777-200ER | GE90-90B | BAE146-300 | ALF502R-5 | Small Turboprop | PT6A |
| 747-300 | CF6-50E2 | 777-200ER | PW4084 | CRJ (Estimated) | CF34-3A1 | Medium Turboprop | |
| 747-300 | CF6-80C2B1 | 777-200ER | TRENT877 | DC-10-30 | CF6-50C2 | Large Turboprop | _ |
| 747-300 | JT9D-7R4G2 | 777-300 | PW4090 | DC-10-30F | CF6-50C2 | Concorde | Olympus 593 |
| | | | | | | | |

2.3.3. Airplane Mission Performance Calculation

Boeing proprietary performance data files for the airplane/engine combinations shown in Table 2-4 and were used to model all of the airplane/engine combinations listed in the OAG schedule. These data files provide tables of time, fuel burned and distance flown as a function of airplane gross weight and altitude for climbout, climb, and descent conditions. They also provide tables of fuel mileage (nautical miles per pound of fuel burned) as a function of gross weight, cruise Mach number and altitude for cruise conditions and tables of long range cruise Mach number vs. gross weight and altitude. Constant fuel burn rates for taxi-in, taxi-out and approach based on typical mission allowances are also included in these data files. These performance data files were generated using the proprietary Boeing Mission Analysis Program (BMAP), and each file covered the whole operating envelope of the airplane. Simple interpolation routines were used to obtain engine fuel flow for a given flight condition.

Airplane performance calculations were done assuming 70% passenger load factors for all passenger and 'combi' airplanes (airplanes that can be used to carry either passengers or cargo).

Typical payloads for freighter airplanes were determined using cargo loading data reported on the United States Department of Transportation (DOT) Form T-100. DOT Form T-100 data for U.S. domestic flights and flights to and from the U.S. were combined and used to determine the average payload carried by each general freighter airplane type existing in the 1999 OAG flight schedule. For each general freighter type, the average payload carried was added to a typical operating empty weight (OEW) for that airplane type to obtain an 'average' zero fuel weight (ZFW). If the 'average' ZFW for a given general freighter type matched the passenger version's ZFW reasonably well, then performance data for the passenger version loaded at 70% passenger load were used to model it. If the 'average' ZFW for a given general freighter type did not match well with the passenger version's ZFW, then a special performance file for that freighter type was created. This performance file used passenger version operating empty weights (OEW) and an estimated average freighter payload.

Of the 16 general freighter airplane types that existed in the 1999 OAG flight schedule, only the very large freighters (747, Antonov An-124, DC-10, L-1011 and MD-11) had 'average' ZFWs that differed enough from the passenger version ZFW to warrant their being modeled with typical freighter payloads. All other freighter types were modeled as passenger airplanes with 70% passenger load.

Table 2-5 shows the increase in ZFW relative to the 70% passenger loading ZFW for the specific very large freighter airplane types that were modeled using estimated typical freighter payloads.

| Specific Freighter Airplane | Freighter Loading ZFW Percent Increase Over PAX Loading ZFW |
|---------------------------------|--|
| 747-100F FRT JT9D-7A | 12.5% |
| 747-200C_F_FRT_CF6-50E2 | 11.4% |
| 747-200F FRT CF6-50E2 | 11.4% |
| 747-200F_FRT_JT9D-7F | 19.4% |
| 747-200F_FRT_JT9D-7J | 19.4% |
| 747-200F_FRT_JT9D-7Q | 19.4% |
| 747-200F FRT JT9D-7R4G2 | 19.4% |
| 747-200F_FRT_RB211-524D4 | 14.6% |
| 747-200SF_FRT_CF6-50E2 | 11.4% |
| 747-200SF_FRT_JT9D-7J | 19.4% |
| 747-200SF_FRT_JT9D-7Q | 19.4% |
| 747-200SF_FRT_JT9D-7R4G2 | 19.4% |
| 747-200SF_FRT_RB211-524D4 | 14.6% |
| 747-400F_FRT_CF6-80C2B1F | 10.9% |
| 747-400F_FRT_PW4000-4056 | 15.6% |
| 747-400F_FRT_RB211-524H2 | 10.2% |
| An-124-*_FRT_D-18-T | 10.9% |
| DC-10-10F_FRT_CF6-6D | 5.7% |
| DC-10-30F_FRT_CF6-50C2 | 17.8% |
| DC-10-30F_FRT_CF6-50C2B | 17.8% |
| L-1011-200_FRT_RB211-524B | 11.5% |
| L-1011-200_FRT_RB211-524B4 | 11.5% |
| MD-11-Freighter_FRT_CF6-80C2D1F | 16.3% |
| MD-11-Freighter_FRT_PW4000-4460 | 13.5% |

Table 2-5. Increase in ZFW relative to the 70% passenger loading case for very large freighters.

2.3.4. Calculation of Global Emissions

The primary emissions produced by the combustion of jet fuel are water vapor (H_2O) and carbon dioxide (CO_2). The emission levels of H_2O and CO_2 are determined by the fuel consumption and the fraction of hydrogen and carbon contained in the fuel. Results from a Boeing study of jet fuel properties measured from samples taken from airports around the world have yielded an average hydrogen content of 13.8% (Hadaller and Momenthy, 1989). Emissions of sulfur dioxide (SO_2) from aircraft engines are determined by the levels of sulfur

compounds in the jet fuel. Although jet fuel specifications require sulfur levels below 0.3%, they are typically much lower than this in the fuel supply utilized by the world's aircraft fleet. The Boeing measurements obtained an average sulfur content of 0.042% with 90% of the samples below 0.1% (Hadaller and Momenthy, 1989). These measurements are in the range of values reported in more recent fuel surveys (Hadaller, *et al.*, 2000). Future sulfur levels are projected to drop to about 0.02% (Hadaller and Momenthy, 1993).

Aircraft engine emissions are characterized in terms of an emission index, which has units of grams of emission per kilogram of fuel burned. Current and projected emission indices are summarized in Table 2-6, based on the analyses of Hadaller and Momenthy for commercial Jet A fuel.

| Emission | Emission Index |
|-------------------------------------|----------------|
| Carbon Dioxide (CO2) | 3155 |
| Water (H ₂ O) | 1237 |
| Sulfur oxides (as SO ₂) | 0.8 |

Table 2-6.Recommended emission indices (in units of grams
emission/kilogram fuel).

Emissions of nitrogen oxides (NO_X) , carbon monoxide (CO) and hydrocarbons from an aircraft engine vary in quantity according to the combustor conditions. Nitrogen oxides are produced in the high temperature regions of the combustor primarily through the oxidation of atmospheric nitrogen. Thus, the NO_X produced by an aircraft engine is sensitive to combustor pressure, temperature, flow rate, and geometry. The NO_X emission index varies with the power setting of the engine, being highest at high thrust conditions. By contrast, carbon monoxide and hydrocarbon emission indices are highest at low power settings where combustor temperatures and pressures are low and combustion is less efficient.

Nitrogen oxides consist of both nitric oxide (NO) and nitrogen dioxide (NO₂). For NO_x, the emission index [EI(NO_x)] is given as gram equivalent NO₂ to avoid ambiguity. Although hydrocarbon measurements of aircraft emissions by species have been made (Spicer *et al.*, 1992), only total hydrocarbon emissions are considered in this work.

For the majority of the engines considered in this study, emissions data from engine certification measurements (ICAO, 2000) were used to model emissions characteristics. In these measurements, emissions of nitrogen oxides (NOx), carbon monoxide (CO) and total hydrocarbons (HC) are measured at standard day sea level conditions at four power settings [7% (idle), 30% (approach), 85% (climbout) and 100% (takeoff)]. If the ICAO database did not contain a particular engine, the data for that engine were obtained from the engine manufacturer. This was done for the three sizes of turboprops considered. If a source could not be found (e.g., JT3C and JT4A), engines with a similar core were used with an adjustment for different fuel flow rates.

In the global emissions calculations, each OAG airplane/engine combination is matched to both a performance engine and an emissions engine (see Appendix B for the matchup table). Fuel flow is calculated using the performance data. Then the emissions are calculated using the fuel flow based technique discussed later in this section.

In most cases, the emissions engine used to model an airplane was the same as that used to calculate the performance. In some cases, performance data for the airplane model identified in the processed OAG flight schedule were available but the engine assumed in the performance data was different than the engine identified in the schedule. In the majority of these cases, the basic engine type is matched but not the specific maximum take-off thrust rating (a 737-700/CFM56-7B20 airplane/engine combination listed in the OAG schedule might be modeled using 737-700/CFM56-7B18 performance data).

If the engine identified in the processed OAG schedule for a particular airplane was similar to the engine assumed in the performance data used to model the airplane, the emissions engine was selected to match the OAG engine. If the engine identified in the processed OAG schedule was significantly different from the engine assumed in the performance data, the emissions engine was selected to match the performance engine.

Boeing has developed an empirical method that allows the calculation of emissions for a wide variety of airplanes and a large number of missions. This method was described in detail previously (Baughcum, *et al.*, 1996a, Appendix D) and is referred to as the Boeing Fuel Flow Method #2. In this method, emission indices measured during sea level static engine certification tests are correlated with engine fuel flow and then scaled for ambient temperature, pressure, flight Mach number and humidity to determine emissions at flight conditions.

All global emissions calculations were done using the GAEC (Global Atmospheric Emissions Code) as described previously (Baughcum, *et al.*, 1994; Baughcum, *et al.*, 1996a). The GAEC graphical user interface was used to associate airplane/engine combinations listed in the OAG airplane schedule with the performance and emissions data that were used to model them in the inventory calculation. Once these associations were made, the GAEC was used to calculate a global emission inventory using OAG schedule data, performance data, emissions data and airport location data.

For purposes of the emissions calculations, the Earth's atmosphere was divided into a grid of three-dimensional cells with dimensions of 1 degree of latitude by 1 degree of longitude by 1 kilometer in altitude, up to 22 kilometers.

2.5 Methodology Changes from Previous Boeing Inventory Calculations

The methodology used to create the 1999 scheduled aircraft fleet global emission inventory documented in this report is slightly different from the methodology used to calculate the NASA full year 1992 scheduled aircraft fleet emission inventory (Baughcum, *et al.*, 1996a). Differences between the two methodologies are as follows:

- 1. A new procedure was used to extract flight schedules from OAG data for creating the 1999 inventory. The new procedure uses the same basic OAG flight schedule data for input as the previously used procedure and utilizes similar algorithms to filter double counted flights from the data but is much more automated, requires less expert judgment by the analyst, and is more reproducible. The new procedure uses a different fleet information database to assign engines to a specific OAG airplane type. The new procedure utilizes the commercially available "Airclaims" database for fleet information (See Appendix A for a sample of Airclaims fleet information data) instead of the Boeing proprietary fleet information database called "Jet Track" which was utilized by the previously used procedure. The "Jet Track" database is no longer in use by the Boeing company.
- 2. OAG schedules forecasted up to three months into the future were used for the current work while published schedules for each month of the year were used to create the 1992 scheduled aircraft fleet emission inventory (see Section 2.1).
- 3. In the current work, some specific airplane/engine types were modeled using different emissions and/or performance data than those used in the 1992 full year scheduled aircraft fleet emission inventory calculations. As noted earlier, the 1999 study uses a larger set of airplane performance and engine data.

4. As discussed in Section 2.3.3 of this report, some freighter airplanes were modeled differently in the current work than in previous NASA scheduled inventory calculations by using a more realistic payload.

To quantify the effects of the above methodology changes, the NASA emission inventory for August 1992 scheduled aircraft was recalculated using the same methodology that was used to create the 1999 scheduled aircraft inventory. Global totals of fuel burned, distance traveled and NOx emissions for the recalculated August 1992 inventory compared well with the global totals for August 1992 reported previously (Baughcum, *et al.*, 1996a). Totals by general aircraft classes (737, A320, etc.) were also compared between the original and recalculated August 1992 inventories.

A comparison of the recalculated August 1992 inventory and the previously published August 1992 inventory shows that global totals for distance are in excellent agreement, differing by only 0.1%. Distance totals for general aircraft classes also compared well between the previous and recalculated inventories, they differed from one another by no more than 1.8%. The agreement in distance totals indicates that the new procedure used to extract flight schedules from OAG data gives results that are very similar to the previously used procedure.

Comparisons between the new and old calculations for global totals of NOx, CO and hydrocarbon emissions and fuel burned show differences of -0.3%, 19.7%, 18.2% and 0.0% respectively (a positive percent difference in these and the comparisons that follow indicates that values for the recalculated inventory are greater than the previously published inventory). Totals of NOx, CO and hydrocarbon emissions for some general aircraft classes differed between the two inventory calculations significantly more than the global totals did.

The differences in NOx, CO and hydrocarbon emissions between the recalculated and the previously calculated August 1992 inventories are due to differences in the emissions characteristics selected to model specific engines in the two inventory calculations.

Some engine types have had more than one combustor type implemented during their production run. For some engines used on a significant number of flights flown by the 1992 scheduled aircraft fleet, NOx, CO and hydrocarbon emission indices can change dramatically depending on the combustor selected for the engine. Further study and more complete data regarding implementation of various combustor options has led to a revised distribution and assignment of combustors for selected engine types. These revised assignments were used for the August 1992 recalculated inventory so they would be consistent with combustor assumptions made when creating the 1999 inventory. Because of the changes in methodology discussed above, in order to do a self consistent trend analysis of emissions and fuel burn from 1976 to 1999, the previously published 1976 and 1984 inventories would have to be recalculated using the same methodology that was used to create the 1999 scheduled inventory if trends in hydrocarbon or carbon monoxide emissions are required. Recalculation of the 1976 and 1984 emission inventories is beyond the scope of the current work but should be considered for the future. The analysis suggests that trends of fuel burn and NOx emissions would not be impacted by the change in methodology, at least in terms of global totals. A more detailed analysis would be required to evaluate whether this is true for regional and "by-aircraft" trends as well.

3. Results and Analysis - Scheduled Aircraft Emissions

3.1 Overview of Results

The fuel burned and emissions calculated for the scheduled aircraft fleet for each month of 1999 are summarized in Table 3-1.

| | of 1999. | | | | |
|-----------|----------|---------------------------------------|----------|----------|----------|
| | Fuel | NOx | HC | CO | Distance |
| Month | (kg/day) | (kg/day) | (kg/day) | (kg/day) | (km/day) |
| | | | | | |
| January | 3.42E+08 | 4.49E+06 | 5.30E+05 | 1.87E+06 | 6.80E+07 |
| February | 3.40E+08 | 4.48E+06 | 5.24E+05 | 1.86E+06 | 6.82E+07 |
| March | 3.43E+08 | 4.52E+06 | 5.20E+05 | 1.86E+06 | 6.88E+07 |
| April | 3.45E+08 | 4.54E+06 | 5.12E+05 | 1.85E+06 | 6.90E+07 |
| Мау | 3.47E+08 | 4.58E+06 | 5.14E+05 | 1.87E+06 | 7.01E+07 |
| June | 3.57E+08 | 4.70E+06 | 5.24E+05 | 1.90E+06 | 7.21E+07 |
| July | 3.61E+08 | 4.75E+06 | 5.28E+05 | 1.92E+06 | 7.27E+07 |
| August | 3.64E+08 | 4.80E+06 | 5.36E+05 | 1.94E+06 | 7.36E+07 |
| September | 3.57E+08 | 4.70E+06 | 5.23E+05 | 1.91E+06 | 7.26E+07 |
| October | 3.54E+08 | 4.66E+06 | 5.12E+05 | 1.88E+06 | 7.21E+07 |
| November | 3.46E+08 | 4.58E+06 | 4.90E+05 | 1.82E+06 | 7.02E+07 |
| December | 3.50E+08 | 4.64E+06 | 4.93E+05 | 1.83E+06 | 7.10E+07 |
| | | · · · · · · · · · · · · · · · · · · · | | | |
| Total | 1.28E+11 | 1.69E+09 | 1.89E+08 | 6.85E+08 | 2.58E+10 |
| | kg/year | kg/year | kg/year | kg/year | km/year |

Table 3-1.Fuel burned and emissions for scheduled air traffic for each month
of 1999.

The geographical distribution of the NOx emissions calculated for May 1999 scheduled air traffic is shown in Figures 3-1 and 3-2. This distribution is representative of the geographical distributions of fuel burn, NOx, CO and hydrocarbon emissions for scheduled air traffic for all months of 1999.

Figure 3-1 shows cruise emissions (9-13 km altitude band) as a function of latitude and longitude. As in scheduled inventories previously calculated for 1976, 1984 and 1992, peak emissions occur over the United States, Europe, the North Atlantic flight corridor, and Japan.

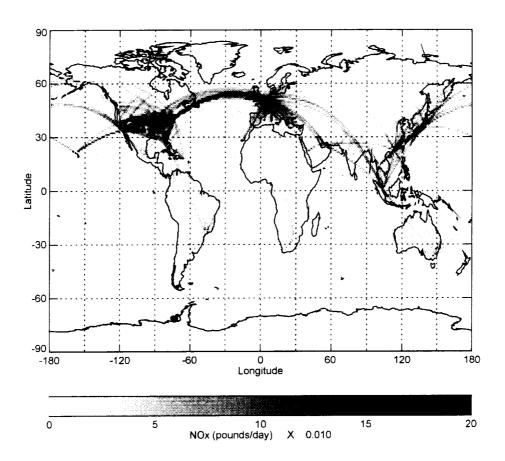


Figure 3-1. Global cruise (9-13 km) NOx distribution for the scheduled aircraft fleet, May 1999.

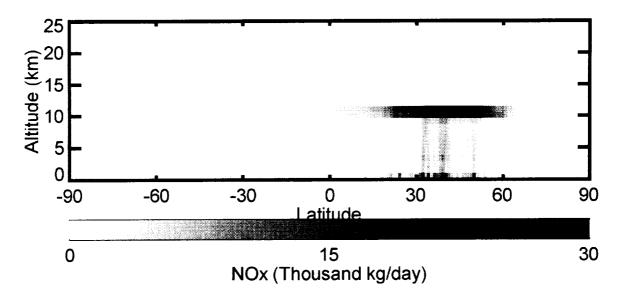


Figure 3-2. NOx emissions for the scheduled aircraft fleet, May 1999, as a function of altitude and latitude (summed over longitude).

Figure 3-2 shows NOx emissions as a function of altitude and latitude. This figure illustrates that the majority of global NOx emissions occur between 30° North and 60° North latitude at typical cruise altitudes (9-13 km).

Approximately 91 percent of emissions from the scheduled aircraft fleet are produced in the Northern Hemisphere. Table 3-2 shows the percentage of global fuel burned, NOx emitted and distance traveled amongst seven selected regions of the world for May 1999. The largest percentage of global fuel burned and emissions occur over the United States and Europe.

| | | d in selecte led aircraft | ed regions o fleet. | of the world | by the N | /lay 1999 |) |
|-------------|-----|------------------------------|------------------------|-------------------|------------------|-----------|----------|
| | US | Europe | North America | North Atlantic | North Pacific | China | Far East |
| Fuel burned | 30% | 14% | 32% | 4% | 3% | 4% | 3% |
| NOx | 28% | 14% | 30% | 4% | 3% | 5% | 4% |
| Distance | 39% | 16% | 41% | 3% | 2% | 4% | 2% |

Percentage of global fuel burned, NOx emitted and distance Table 3-2.

Distributions of fuel burned and emissions as a function of altitude are shown in Figure 3-3. This figure shows that peak fuel burned and NOx emissions occur at cruise altitudes, while peak CO and hydrocarbon emissions occur during the landing/takeoff cycle in the 0-1 km altitude band. Approximately 31% of the fuel burned and 35% of NOx emissions occur below 9 km while approximately 70% of the hydrocarbon and carbon monoxide emissions are emitted below 9 km.

The plots of fuel burned and emissions as a function of latitude in Figure 3-4 emphasize that peak emissions from the scheduled fleet occur at northern mid-latitudes, with the majority of emissions occurring between 30° North and 60° North latitude.

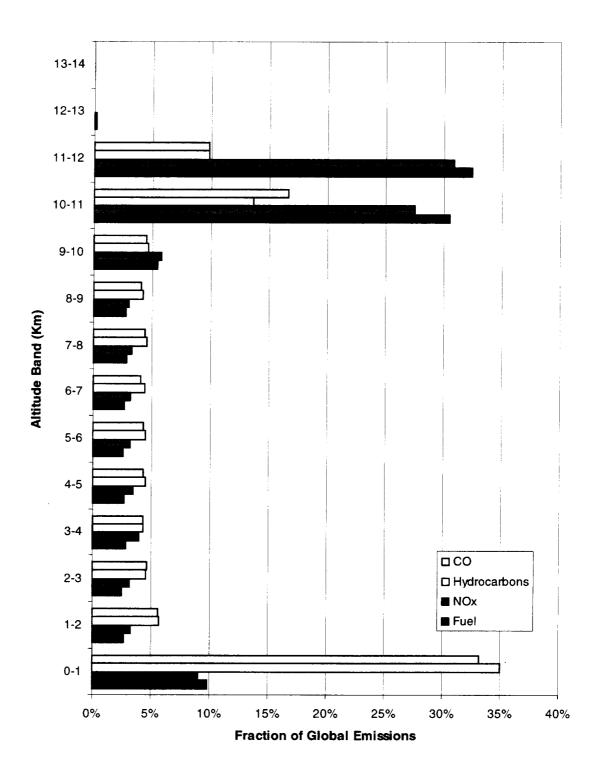


Figure 3-3. Altitude distribution of fractional fuel burned and fractional global emissions of CO, Hydrocarbons and NOx for the scheduled aircraft fleet, May 1999.

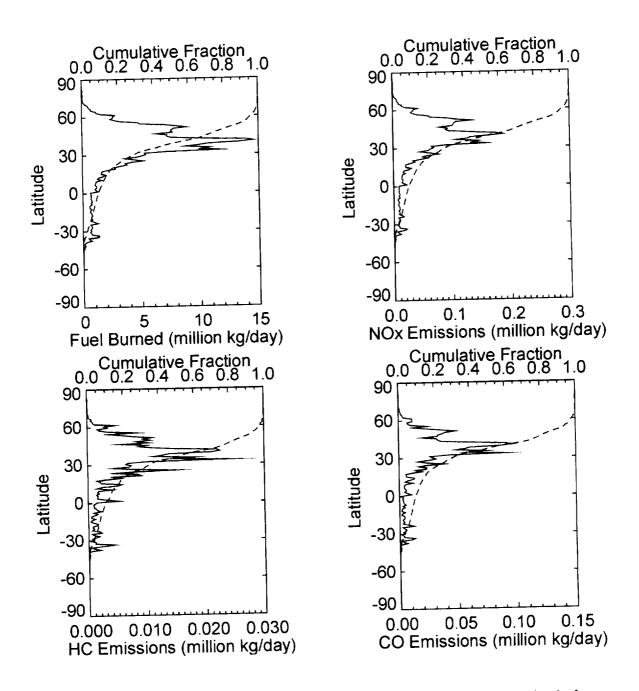


Figure 3-4. Fuel burned and emissions (solid line) as a function of latitude for scheduled May 1999 air traffic. Dashed lines show the cumulative fraction of emissions.

3.2 Fleet Movement Statistics, Fuel Usage and Effective Emission Indices

To summarize results of the emission inventory calculations, specific aircraft types were grouped into general aircraft classes and their fuel burned, emissions, departures and distance traveled were totaled. Global effective emission indices for each general aircraft class were also calculated for the 1-9 km and 9-13 km band. Here we define an effective emission index as the ratio of emittant integrated over a given geographical region (latitude, longitude, altitude band) to the integrated fuel use over the same region. Effective emission indices reported herein were calculated using global emissions and are therefore referred to as *global* effective emission indices.

Fleet movement statistics for May 1999 by general aircraft class are summarized in Table 3-3. This table shows the total daily distance flown, the daily departures, and their fraction of the global total for each general aircraft class. It also shows the average route distance for each general class. A more detailed summary identifying similar results for each specific OAG airplane/engine combination in a given aircraft class is provided in Appendix E, which also identifies how each of the general aircraft classes in Table 3-3 is defined. The statistics for May 1999 shown in Table 3-3 and Appendix E are representative of those for all other months in 1999.

| 1999. | l | % of | | % of | Average Route |
|------------------------|------------|------------|------------------------|------------------------|---------------|
| | Daily | Global | Distance | Global | Distance |
| General Type | Departures | Departures | (km/day) | Distance | (km) |
| General Type | Departures | Departures | (Kilbudy) | Biotanoo | (((,,,,))) |
| Turbopropo | 21,296 | 30.56% | 6,608,584 | 9.43% | 310 |
| Turboprops | 10,224 | 14.67% | 9,147,802 | 13.05% | 895 |
| Boeing 737-300/400/500 | · · | 7.74% | 9,147,802 5,619,233 | 8.02% | 1,041 |
| MD-80 | 5,397 | | 3,176,590 | 4.53% | 792 |
| Boeing 737-100/200 | 4,013 | 5.76% | | 4.53 <i>%</i> 3.39% | 752 |
| DC-9 | 3,346 | 4.80% | 2,379,550 | | 656 |
| Regional Jets | 3,198 | 4.59% | 2,096,416 | 2.99% | |
| Airbus A320 | 3,071 | 4.41% | 3,818,451 | 5.45% | 1,243 |
| Boeing 757-200 | 2,741 | 3.93% | 4,828,701 | 6.89% | 1,762 |
| Boeing 727-200 | 2,353 | 3.38% | 2,532,550 | 3.61% | 1,077 |
| Fokker 100 | 1,697 | 2.43% | 1,079,091 | 1.54% | 636 |
| Boeing 767-300 | 1,533 | 2.20% | 4,043,356 | 5.77% | 2,638 |
| Boeing 747-400 | 1,006 | 1.44% | 5,664,264 | 8.08% | 5,632 |
| BAE 146 | 993 | 1.43% | 630,398 | 0.90% | 635 |
| Airbus A300-600 | 825 | 1.18% | 1,012,579 | 1.44% | 1,228 |
| Boeing 737-600/700/800 | 771 | 1.11% | 1,047,151 | 1.49% | 1,357 |
| Russian Aircraft | 701 | 1.01% | 1,266,310 | 1.81% | 1,806 |
| Fokker 28 | 626 | 0.90% | 358,254 | 0.51% | 572 |
| Boeing 747-100/200/300 | 570 | 0.82% | 2,573,174 | 3.67% | 4,517 |
| Airbus A319 | 537 | 0.77% | 692,169 | 0.99% | 1,289 |
| Boeing 767-200 | 492 | 0.71% | 1,417,564 | 2.02% | 2,884 |
| Boeing 777-200 | 473 | 0.68% | 1,583,564 | 2.26% | 3,345 |
| Airbus A310 | 464 | 0.67% | 1,044,357 | 1.49% | 2,251 |
| Airbus A321 | 448 | 0.64% | 361,687 | 0.52% | 807 |
| MD-90 | 442 | 0.63% | 331,624 | 0.47% | 750 |
| DC-10 | 379 | 0.54% | 1,523,344 | 2.17% | 4,022 |
| MD-11 | 308 | 0.44% | 1,541,979 | 2.20% | 5,006 |
| DC-8 | 266 | 0.38% | 451,733 | 0.64% | 1,699 |
| Boeing 727-100 | 261 | 0.37% | 205,915 | 0.29% | 789 |
| Airbus A330-300 | 250 | 0.36% | 510,219 | 0.73% | 2,044 |
| Airbus A340-300 | 230 | 0.32% | 1,250,423 | 1.78% | 5,589 |
| | 199 | 0.29% | 273,690 | 0.39% | 1,377 |
| Airbus A300-B2/B4/F4 | 199 | 0.29% | 273,690 149,699 | 0.39% | 756 |
| Fokker 70 | | | 288,761 | 0.21% 0.41% | 2,058 |
| Lockheed L-1011 | 140 | 0.20% | | 0.41% 0.19% | 1,614 |
| Boeing 777-300 | 82 | 0.12% | 131,672 | | |
| BAC111 | 57 | 0.08% | 45,221 | 0.06% | 797 |
| Boeing 707 | 41 | 0.06% | 105,766 | 0.15% | 2,607 |
| Airbus A330-200 | 39 | 0.06% | 138,796 | 0.20% | 3,572 |
| Airbus A340-200 | 20 | 0.03% | 140,216 | 0.20% | 6,961 |
| Concorde | 6 | 0.01% | 33,890 | 0.05% | 5,648 |
| Miscellaneous | 5 | 0.01% | 3,013 | 0.00% | 659 |
| Total | 69,690 | | 70,107,755 | | |

Table 3-3.Summary of departure statistics by general aircraft type for May 1999.

Tables 3-4 and 3-5 show a summary of average daily fuel burned, global effective emission indices and the fractional contribution to the global fuel burned and emissions totals calculated for May 1999 for each general aircraft class. In Table 3-4, separate global effective emission indices are shown for NOx, CO and hydrocarbons for the 1-9 km band and the 9-13 km band. A more detailed summary of global effective emission indices showing the results for each OAG airplane/combination is included as Appendix D. Some variation in the global effective emission indices listed in Appendix D may occur between similar aircraft/engine types because of differences in average mission distances flown by them and differences in engine and performance data used to model them.

The data in Table 3-4 represent results of calculations done assuming typical OEWs and average seat counts and load factors, actual configurations and loading will be unique to specific operators and routes.

Table 3-3 shows that global departures are dominated by smaller aircraft (turboprops, 737s, MD-80s, DC-9s and regional jets) with 31% of global departures being made by turboprop aircraft alone. Tables 3-4 and 3-5 show that no general aircraft class dominates global scheduled aircraft fleet fuel burned and NOx emissions. These tables show that roughly 48% of scheduled fleet fuel was consumed and 52% of scheduled fleet NOx was created by large long-range aircraft (747s, A340s, L-1011s, DC-10s, 777s and 767s).

| traffic). | | | 1.0 km | Altitude | Band | 9-13 ki | m Altitude | Band |
|---|--|---|--|--|--|---|---|---|
| | | | | Ainuuc | | | | |
| | Fuel (1000 | % of Global Scheduled Traffic Fuel Burned | El (NOx) | El (CO) | El (HC) | EI (NOx) | EI (CO) | EI (HC) |
| General Type | kg/day) | | | (00) | 3.107 | | | |
| Boeing 747-400 Boeing 737-300/400/500 Boeing 747-100/200/300 MD-80 Boeing 767-300 Boeing 757-200 | 59,837 30,765 30,638 22,367 22,153 19,717 | 17.22% 8.85% 8.82% 6.44% 6.37% 5.67% | 25.3 13.23 27.51 15.96 21.33 18.64 | 8.1 11.5 15.4 4.2 7.0 8.4 | 1.9 0.9 10.2 1.2 1.4 0.5 | 13.3 9.6 15.2 10.6 12.5 11.0 | 1.0 3.5 2.2 4.4 1.2 1.7 | 0.4 0.2 1.1 1.6 0.3 0.1 1.0 |
| Boeing 727-200 DC-10 Boeing 737-100/200 MD-11 Airbus A320 | 14,334 12,679 12,223 11,952 11,884 | 4.12% 3.65% 3.52% 3.44% 3.42% | 11.91 24.23 11.18 18.98 17.45 25.17 | 9.6 7.5 10.0 5.9 5.6 5.4 | 3.1 2.8 3.3 0.5 0.5 6.0 | 8.3 14.9 7.1 12.9 12.0 16.8 | 5.4 2.0 6.8 1.2 2.0 0.6 | 1.0 0.9 1.3 0.1 0.4 0.3 |
| Boeing 777-200 DC-9 Turboprops Airbus A340-300 Russian Aircraft | 11,260 9,130 8,788 8,242 7,138 | 3.24% 2.63% 2.53% 2.37% 2.05% | 10.99 11.92 22.97 12.33 | 11.8 3.8 11.3 15.5 6.6 | 4.2 0.2 4.7 9.0 1.6 | 7.6 13.7 9.2 11.1 | 6.7 1.7 8.4 2.0 | 1.0 0.2 1.5 0.3 |
| Boeing 767-200 Airbus A300-600 Airbus A310 Regional Jets Fokker 100 | 7,110 6,397 5,298 4,479 3,444 | 2.05% 1.84% 1.52% 1.29% 0.99% | 22.6 17.77 18.46 11.63 11.05 | 10.1 15.3 9.4 21.0 | 2.0 4.7 1.4 2.0 | 12.2 11.3 9.1 6.4 | 1.7 2.2 0.6 7.0 | 0.3 0.6 0.1 1.0 |
| Airbus A330-300 Boeing 737-600/700/800 DC-8 Lockheed L-1011 | 3,402 3,219 2,883 2,415 | 0.98% 0.93% 0.83% 0.70% 0.67% | 23.04 16.32 11.24 18.74 9.14 | 7.0 6.4 16.3 19.4 5.0 | 1.5 0.9 11.2 13.6 0.5 | 14.5 11.8 8.6 14.4 7.8 | 1.3 1.8 7.2 9.0 1.6 | 0.5 0.3 1.4 2.2 0.1 |
| BAE 146 Airbus A319 Airbus A300-B2/B4/F4 Airbus A321 MD-90 | 2,330 2,048 2,004 1,405 1,243 | 0.59% 0.58% 0.40% 0.36% | 14.55 22.17 17.45 16.44 | 5.7 13.1 6.4 5.2 | 0.7 5.2 0.6 0.1 | 10.9 14.5 13.3 11.9 | 2.5 1.9 1.7 1.8 | 0.3 1.2 0.2 0.1 |
| Fokker 28 Boeing 777-300 Boeing 727-100 Airbus A340-200 | 1,211 1,131 1,094 910 | 0.35% 0.33% 0.31% 0.26% | 10.47 24.77 10.8 23.05 | 13.5 4.4 14.8 11.2 | 7.8 10.3 5.7 4.6 | 7.4 15.7 7.1 13.7 | 7.2 0.8 10.2 1.8 | 2.7 0.5 2.1 0.1 |
| Airbus A30-200 Boeing 707 Fokker 70 Concorde BAC111 | 848 607 453 351 158 | 0.24% 0.17% 0.13% 0.10% 0.05% | 24.34 8.35 10.3 11.03 14.44 8.61 | | 1.0 39.4 1.2 1.3 15.1 2.3 | 16.3 5.4 7.1 10.0 10.1 7.3 | 1.6 17.9 2.7 26.1 14.7 0.8 | 0.3 8.5 1.0 1.8 6.0 0.2 |

Table 3-4.Summary of fuel burned and global effective emission indices for
commercial aircraft types (based on May 1999 scheduled air
traffic)

| General Type | Fuel | NOx | HC | CO | Distance |
|------------------------|--------|--------|--------|--------|----------|
| | | | | | |
| Boeing 747-400 | 17.22% | 18.94% | 6.68% | 6.67% | 8.08% |
| Boeing 737-300/400/500 | 8.85% | 7.22% | 3.91% | 14.79% | 13.04% |
| Boeing 747-100/200/300 | 8.82% | 11.17% | 15.36% | 7.86% | 3.67% |
| MD-80 | 6.44% | 6.04% | 6.75% | 5.68% | 8.01% |
| Boeing 767-300 | 6.37% | 6.78% | 2.73% | 3.43% | 5.77% |
| Boeing 757-200 | 5.67% | 5.55% | 0.87% | 4.46% | 6.89% |
| Boeing 727-200 | 4.12% | 3.04% | 6.34% | 6.56% | 3.61% |
| DC-10 | 3.65% | 4.45% | 4.08% | 2.74% | 2.17% |
| Boeing 737-100/200 | 3.52% | 2.36% | 6.44% | 6.40% | 4.53% |
| MD-11 | 3.44% | 3.53% | 0.42% | 1.28% | 2.20% |
| Airbus A320 | 3.42% | 3.51% | 1.04% | 2.58% | 5.45% |
| Boeing 777-200 | 3.24% | 4.42% | 4.13% | 1.10% | 2.26% |
| DC-9 | 2.63% | 1.72% | 6.85% | 6.25% | 3.39% |
| Turboprops | 2.53% | 2.13% | 0.53% | 2.13% | 9.42% |
| Airbus A340-300 | 2.37% | 2.63% | 1.00% | 1.33% | 1.78% |
| Boeing 767-200 | 2.05% | 2.01% | 0.95% | 1.27% | 2.02% |
| Russian Aircraft | 2.05% | 1.53% | 7.52% | 4.92% | 1.83% |
| Airbus A300-600 | 1.84% | 1.93% | 1.36% | 2.07% | 1.44% |
| Airbus A310 | 1.52% | 1.46% | 1.65% | 1.67% | 1.49% |
| Regional Jets | 1.29% | 1.01% | 0.83% | 1.82% | 2.99% |
| Fokker 100 | 0.99% | 0.62% | 1.14% | 3.04% | 1.54% |
| Airbus A330-300 | 0.98% | 1.24% | 0.57% | 0.65% | 0.73% |
| Boeing 737-600/700/800 | 0.93% | 0.92% | 0.41% | 0.77% | 1.49% |
| DC-8 | 0.83% | 0.57% | 2.85% | 1.82% | 0.64% |
| Lockheed L-1011 | 0.69% | 0.82% | 3.51% | 1.90% | 0.41% |
| BAE 146 | 0.67% | 0.43% | 0.22% | 0.67% | 0.90% |
| Airbus A319 | 0.59% | 0.54% | 0.23% | 0.50% | 0.99% |
| Airbus A300-B2/B4/F4 | 0.58% | 0.74% | 1.37% | 0.93% | 0.39% |
| Airbus A321 | 0.40% | 0.47% | 0.13% | 0.44% | 0.52% |
| MD-90 | 0.36% | 0.38% | 0.02% | 0.32% | 0.47% |
| Fokker 28 | 0.35% | 0.22% | 5.18% | 1.43% | 0.51% |
| Boeing 777-300 | 0.33% | 0.45% | 1.24% | 0.15% | 0.19% |
| Boeing 727-100 | 0.31% | 0.21% | 0.81% | 0.76% | 0.29% |
| Airbus A340-200 | 0.26% | 0.29% | 0.09% | 0.14% | 0.29% |
| Airbus A330-200 | 0.24% | 0.33% | 0.07% | 0.12% | 0.20% |
| Boeing 707 | 0.17% | 0.08% | 2.13% | 0.76% | 0.20% |
| Fokker 70 | 0.13% | 0.09% | 0.12% | 0.17% | 0.15% |
| Concorde | 0.10% | 0.12% | 0.09% | 0.18% | 0.21% |
| BAC111 | 0.05% | 0.04% | 0.38% | 0.20% | 0.05% |

Table 3-5.Fractional contribution of each commercial airplane type to global
fuel burned and emissions totals for May 1999 scheduled traffic.
(Summed over all altitudes, latitudes, and longitudes)

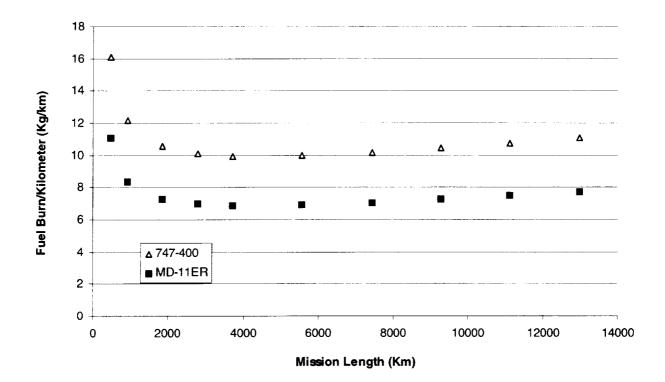
There has been some confusion in the scientific literature and with various emission inventory calculations with regard to emission indices at flight altitudes. Most of the available data are from certification measurements at sea level conditions (International Civil Aviation Organization (ICAO), 2000). In some cases, these have been used incorrectly as being representative of the emission levels at cruise conditions, without corrections being used for ambient conditions of pressure and temperature.

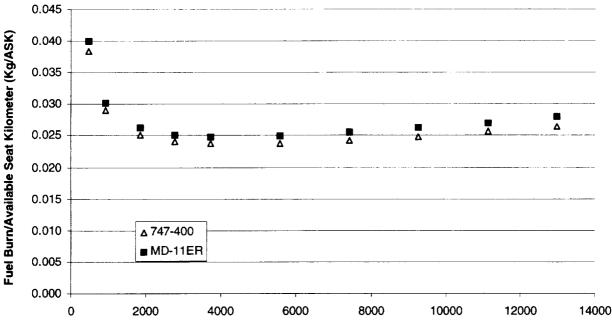
In order to help reduce the confusion about the global effective emission indices for commercial aircraft, Table 3-4 shows the global effective emission indices for NOx, CO, and hydrocarbons for each general aircraft class. Global effective emission indices are shown for two altitude bands: 1-9 km (climb and descent averaged together) and 9-13 kilometers (primarily cruise but some final climb and initial descent).

These global effective emission indices represent our best estimate of fleet averages (averaged over all missions) and should not be compared directly with an emission index measured behind an individual aircraft in flight. The methodology used to calculate emissions at altitude in this study (see Section 2.3.4 of this report) can be used for such a comparison if accurate and precise measurements of actual fuel flow, ambient temperature, ambient pressure, humidity, Mach number and corresponding emission index are made. Comparisons with in-flight emission index measurements should provide a way to evaluate the accuracy of the emission methodology used to calculate the inventories documented in this report.

Care must be exercised if attempting to use the information in Table 3-3 and Table 3-4 to calculate fuel efficiencies for the various general aircraft classes. Any aircraft fuel efficiency comparison requires a consideration of the amount of payload (passengers and freight) being carried by each aircraft for a given mission length. Comparisons of aircraft on a strict fuel burn per distance traveled basis without normalizing the data for the number of passengers carried may result in misleading comparisons.

Figure 3-5 illustrates this point. This figure contains plots of fuel burned per kilometer traveled (top panel) and fuel burned per passenger kilometer traveled (bottom panel) as a function of mission length for a 747-400 and an MD-11ER. The top panel of Figure 3-5 shows that the fuel burned per kilometer for the MD-11ER is significantly lower (approximately 46 percent) than that of the 747-400 for all mission lengths shown. This though is a misleading comparison because the number of passengers carried by the MD-11ER is less than that carried by the 747-400. The bottom panel of Figure 3-5 shows the effect of normalizing the data by average seat count. Fuel burned per ASK (available seat kilometer) is plotted versus mission range. For this comparison the fuel burned per ASK values for the 747-400 and MD-11ER are within 6 percent of each other for all mission lengths shown.





Mission Length (Km)

Figure 3-5. Fuel burned per kilometer traveled (top panel) and fuel burned per available seat kilometer traveled (bottom panel) as a function of mission length for the 747-400 and the MD-11ER.

3.3 Seasonal Variability

There is a noticeable- seasonal variation in air traffic departures in some regions as airlines shift schedules and aircraft to accommodate passenger demand. For example, increased air traffic may mean that airlines will utilize their aircraft more frequently and that some airplanes will be used more than others. There are seasonal variations in emissions which reflect both changes in passenger flow and in the equipment being used.

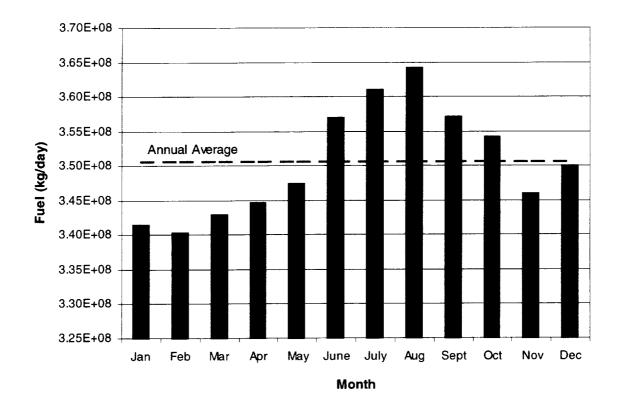
Trends of emissions and fuel burned global totals for the fleet are a composite of three trends: (1) The seasonal variation in traffic demand, (2) Demand growth and changes in overall fleet technology brought about by the introduction of new aircraft and (3) The retirement of old aircraft.

Figure 3-6 shows the seasonal variation in total global fuel burned by the scheduled aircraft fleet (summed over all altitudes). The top panel shows the daily fuel use as a function of month. The bottom panel shows the percent deviation from the annual average fuel use as a function of month. Global fuel use for 1999 peaked at roughly 4% above the annual average in August and was the lowest in February when it was roughly 3% below the annual average. The month having a daily fuel use that was closest to the annual average was December.

Both water vapor and carbon dioxide emission indices are functions of the hydrogen and carbon content, respectively, of the jet fuel. For typical jet fuel,

 $EI(H_2O) = 1237$ grams H₂O/kg fuel burned EI (CO₂) = 3155 grams CO₂/kg fuel burned

Thus, the seasonal variation in carbon dioxide and water vapor emissions from the commercial fleet will be the same as that shown for the fuel usage in Figure 3-6.



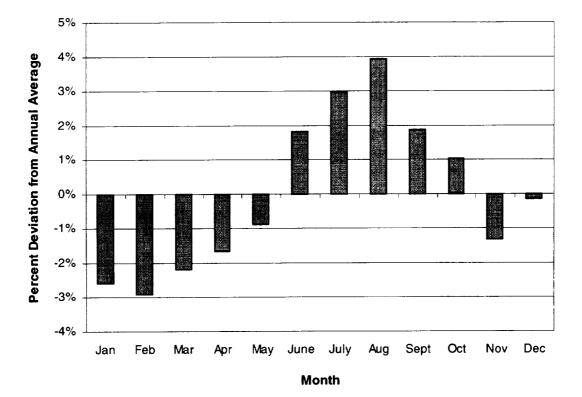


Figure 3-6. Global fuel burned in the 0-19 km altitude band for scheduled air traffic and percent deviation from the annual average fuel burn for each month of 1999.

3.4 Trend Analysis

In order to assess changes in scheduled fleet global emissions and fuel burned between 1992 and 1999, August 1999 emission inventory global totals were compared to August 1992 emission inventory global totals calculated using the same updated methodology outlined in Section 2 of this report.

Table 3-6 shows a comparison between the scheduled fleet global emissions, distance and fuel burned totals for August 1992 and August 1999 that were calculated using the same methodology. Both the total change in emissions, distance and fuel burned over the seven year period and the yearly rate of change are given in Table 3-6. Yearly rate of change values were calculated by assuming exponential growth.

| scheduled aircra | Fuel (kg/day) | NOx (kg/day) | HC (kg/day) | CO (kg/day) | Distance (km/day) |
|--------------------------------|------------------|-----------------|----------------|----------------|----------------------|
| August 1992 | 2.74E+08 | 3.57E+06 | 6.63E+05 | 1.71E+06 | 5.07E+07 |
| August 1999 | 3.64E+08 | 4.80E+06 | 5.36E+05 | 1.94E+06 | 7.36E+07 |
| Total Change (1992 to 1999) | 33% | 35% | -19% | 14% | 45% |
| Average Yearly Change | 4.1% | 4.3% | -3.0% | 1.9% | 5.5% |

| Table 3-6. Fuel burned and emissions calculated self-consistently for the | Э |
|---|---|
| Table 5-6. The burned and enhouse the sums 1992 and August 1999. | |
| scheduled aircraft fleet for August 1992 and August 1999. | |

Fuel use was calculated to have increased by 33% between 1992 and 1999, while NOx emissions were calculated to increased by 35%. These increases correspond to an average annual growth rate of approximately 4%. During this same period, the total distance flown by all scheduled aircraft was calculated to increase by 45%, corresponding to an annual growth rate of 5.5%. By contrast, CO emissions were calculated to increase by only 14% and hydrocarbon emissions were calculated to decrease by 19% between 1992 and 1999.

The relatively small yearly growth of CO emissions and the reduction of hydrocarbon emissions between 1992 and 1999 is mainly due to the retirement of old aircraft from the fleet and the delivery of new technology engines as the fleet grew. The new technology engines have more efficient combustors with higher overall pressure ratios (OPR). These engines generally produce less hydrocarbons and CO than the ones they replaced.

The average yearly growth in NOx emissions between August 1992 and August 1999 is slightly larger than that of fuel burned. Higher engine OPRs, although they lead to fuel efficiency improvements, lead to higher temperatures and pressures within the combustor and typically higher NOx emissions for a given combustor design. This tendency presents a challenge to engine manufacturers who are trying to improve engine fuel efficiency while reducing NOx emissions.

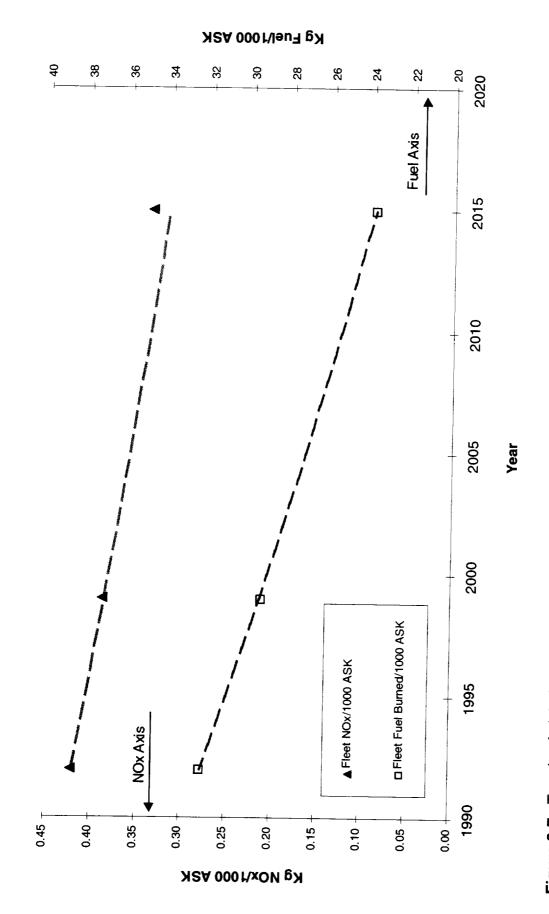
Absolute quantities of fleet emissions and fuel burned do not take into account trends of the productivity of the fleet. In order to establish a trend in scheduled fleet global emissions that takes fleet productivity into account, total global NOx emissions and fuel burned for 1992, 1999 and projected emissions and fuel burned for 2015 were normalized by available seat kilometers (ASK) flown and plotted as a function of year in Figure 3-7.

To generate the trends in Figure 3-7, results of the previously published NASA 1992 scheduled fleet global emission inventory (Baughcum, *et al.*, 1996a) were used for the 1992 NOx emissions and fuel burned totals. Results of the previously published NASA 2015 scheduled fleet global emission scenario (Baughcum, et al., 1998) were used for the 2015 NOx emissions and fuel burned totals. As was discussed in Section 2.5, the methodology used to create the NASA 1992 and 2015 inventories was different than that used for the 1999 inventory, but differences in NOx emissions and fuel burned global totals that come about from the use of the two different methodologies are small. Therefore, it is reasonable to use previous NASA calculations of NOx and fuel burned global totals with the current results to develop a trend analysis.

Total ASKs for 1992, 1999 and 2015 were calculated by multiplying average seat counts for each individual aircraft type in the respective inventory by the number of kilometers flown by that aircraft type and adding the ASK totals for all of the individual aircraft types. Total fleet NOx emissions and fuel use were then normalized by these ASK totals

Figure 3-7 shows that both global NOx/ASK and global fuel use/ASK for the scheduled aircraft fleet decrease with time. The dashed trend lines running through the data points in Figure 3-7 represent a 1.2 percent per year improvement and 1.3 percent per year improvement in NOx/ASK and Fuel Use/ASK, respectively. When the trend lines are extrapolated to 2015, the fuel trend is consistent with the previous 2015 scenario projected, while the NOx trend is slightly better than projected in that scenario.

The trend toward a reduction in NOx/ASK and fuel use/ASK with time demonstrates the effect of introducing improved fuel efficiency and NOx emission reduction technology into the scheduled fleet.





3.5 Effects of Improved Freighter Modeling

In the earlier NASA emission inventories, (Baughcum, *et al.*, 1996a and 1996b) no distinction was made between flights flown by freighter aircraft and those flown by passenger aircraft. All aircraft flights were modeled using performance data generated assuming a 70% passenger load factor. In the OAG flight schedules created for this study, flights flown by freighters are distinguished from those flown by passenger aircraft. This increased detail in the schedule made it possible in the 1999 inventory calculations to more accurately model freighters by modeling them with more representative payloads.

As described in Section 2.3.3 of this report, DOT Form T-100 data were analyzed to determine average payloads for various types of freighter aircraft. Based on this analysis, it was determined that more accurate inventory results could be obtained if very large freighter aircraft types (747, MD-11, L-1011, DC-10 and Antonov An-124) were modeled using passenger versions with payloads heavier than those associated with 70% passenger loading. This analysis also showed that small and medium freighter aircraft could be modeled accurately enough by using passenger versions with payloads corresponding to 70% passenger load factor as was done in previous NASA inventory calculations.

In order to determine the effect of improved freighter payload assumptions on global fuel burned and NOx totals, inventory calculations were made with and without the improved freighter payload assumptions discussed above for August 1999. For general aircraft types that included very large freighters, Table 3-7 shows fuel burned and NOx emissions global totals for the two different calculations along with percent difference comparisons. A positive percent difference indicates that the new freighter payload assumptions increased fuel burn or NOx emissions. Table 3-7 also shows the percent of the total distance within each aircraft type that was traveled by freighter aircraft.

Total fuel use and NOx for the 1999 scheduled aircraft fleet were increased by 0.6 and 1.5 percent respectively when the improved freighter payload assumptions were used. For each aircraft type modeled using improved payload assumptions, global NOx emissions and fuel use increased because the aircraft operated at higher takeoff gross weights (TOGW). Higher TOGWs require higher engine thrust throughout the mission. This leads to increased fuel burn and higher combustor temperatures, which in turn lead to increased NOx emissions.

This improved treatment of freighter aircraft represents a fairly small correction to the emission inventories.

Comparison of August 1999 global fuel burned and NOx emissions with and without the use of freighter cargo loading assumptions. Table 3-7.

| | | | Fuel Burned | - | ž | NOX Emissions | Suc |
|------------------------|-------------------------------|----------------------|-----------------------------------|-----------------------|-----------------------------------|-----------------------------------|-----------------------|
| | Percent of General Type | With | Without | | With | Without | |
| General Aircraft Type | Traveled by Freighters | Payloads (kg/day) | Freignter Payloads (kg/day) | Percent Difference | Freighter Payloads (kg/day) | Freighter Payloads (kg/day) | Percent Difference |
| | | | | | | | |
| Boeing 747-100/200/300 | 41.7% | 2.88E+07 | 2.74E+07 | 5.3% | 4.83E+05 | 4.83E+05 4.34E+05 | 11 3% |
| Boeing 747-400 | 3.7% | 6.46E+07 | 6.44E+07 | 0.4% | 9 30F-05 | 0 25E 105 | |
| DC-10 | 9.8% | 1.38E+07 | 1.37F+07 | 1 10/ | 0.01E.0E | | 0.0% |
| Lockheed L-1011 | A E0/ | | | 0 | 504312.2 | Z.1/E+05 | 2.0% |
| | 4.0% | 2.50E+06 | 2.55E+06 | 0.4% | 3.99E+04 | 3.96E+04 | 0.6% |
| | 23.5% | 1.29E+07 | 1.24E+07 | 4.0% | 1.74E+05 | 1.65E+05 | 5.9% |
| Kussian Aircraft | 4.4% | 8.10E+06 | 8.09E+06 | 0.1% | 7.86E+04 | 7.85E+04 | 0.1% |
| Global Totals | | | | | | | |
| | | 3.65E+08 | 3.62E+08 | 0.6% | A BAELAE A TAFLAD | 1 70L . 00 | ÌĊĹ |

3.6 Database Availability

The 3-dimensional scheduled aircraft emission inventories of fuel burned and emissions calculated on a 1 degree latitude x 1 degree longitude x 1 km altitude grid for each month of 1999 and for August 1992 have been delivered in electronic format to the NASA Langley Research Center. Questions concerning the availability of these data should be directed to Dr. Chowen C. Wey (Chowen.C.Wey@grc.nasa.gov), the NASA GRC contract monitor for this work. Technical questions about the data set should be sent to Steven L. Baughcum (Steven.L.Baughcum@boeing.com) or Donald J. Sutkus (Donald.J.Sutkus@boeing.com) at the Boeing Company, P. O. Box 3707, MS 0R-RC, Seattle, WA 98124-2207. .

4. Comparison of 1999 Inventory Results with DOT Form 41 Data

As discussed in Section 2 of this report, the 1999 scheduled aircraft fleet global emission inventory was created using Official Airline Guide (OAG) flight schedule data, Boeing aircraft performance data and International Civil Aviation Organization (ICAO) engine emissions data.

In developing the performance data used to model aircraft in the 1999 scheduled aircraft fleet global emission inventory, certain simplifying assumptions were made about the conditions under which aircraft operate. These assumptions, which are listed below, lead to errors in the calculation of global aircraft fleet fuel burned and emissions. These errors have been discussed in detail in previous work (Baughcum, *et al.*, 1996a; Daggett, *et al.*, 1999).

Performance Assumptions for the NASA 1999 scheduled emission inventory calculations:

- No winds
- International Standard Atmosphere (ISA) temperatures and pressures
- Continuous climb cruise flight segment with typical westbound flight beginning and ending cruise altitudes
- All aircraft were modeled as passenger aircraft except 747, MD-11, DC-10, L-1011 and An-124 freighter aircraft which were modeled using typical freighter cargoes and OEWs
- Passenger aircraft were modeled assuming no cargo (Payload = passengers + baggage weight)
- Passenger aircraft were modeled using a 70% passenger load factor
- Passenger and baggage weight were assumed to be 200 lb/passenger for single aisle and 210 lb/passenger for wide body aircraft
- Boeing typical weight calculations were used for Operating Empty Weight, Maximum Landing Weight, Maximum Zero Fuel Weight, etc.
- Fuel density of 6.75 lb/gallon and fuel energy content of 18,580 BTU/lb
- Direct great circle routes--no turns or air traffic control diversions
- Takeoff Gross Weights (TOGW) are calculated assuming city pairs are at sea level. Performance calculations assume origin and destination
- airports are at their respective actual airport altitudes.
- Optimum aircraft operating rules
- Engine and airframe performance at new airplane level

Some of the characteristics of the OAG flight schedule data used in creating the scheduled aircraft fleet emission inventories also lead to inaccuracies in global aircraft emission inventory calculations. As discussed in

Section 2 of this report, the 1999 scheduled aircraft fleet global emission inventory calculations are based on the OAG listing of flights which is used as a resource for travelers attempting to book flights. Flights listed in the OAG are those that are *projected* to take place and not ones that necessarily occurred. In addition, the OAG flight schedule often contains duplicate listings of the same flights due to phenomena such as codesharing between airlines. Filtering of the OAG schedules must be done prior to their use for calculating emission inventories and the filtering process is another possible source for inaccuracies in emission inventory results.

In order to evaluate the 1999 scheduled aircraft fleet global emission inventory calculations, comparisons were made between results of these calculations and aviation fuel use and traffic data reported on the U.S. Department of Transportation (DOT) Form 41. Details of this comparison are discussed below.

Each large U.S. air carrier must report statistics for aircraft fuel used, revenue aircraft departures performed and revenue aircraft statute ground track miles flown during a given year on U.S. DOT Form 41. A more detailed description of DOT Form 41 data is contained in previous work (Daggett, *et al.*, 1999). Although these statistics are reported by specific aircraft type (i.e. 747, DC-10 etc.) and geographic region (i.e. North America, Atlantic Ocean, etc.), only airline totals were compared with 1999 scheduled emission inventory results.

DOT Form 41 fuel issue, departure and ground track miles flown data were obtained for the 1999 calendar year for each carrier that reported traffic and capacity data to the U.S. Department of Transportation. Results of the 1999 scheduled aircraft emission inventory calculations were compared to these data. Comparisons were made for the ten passenger airlines that burned the most fuel in 1999 (according to the DOT data) and for the four major cargo carriers that report their fuel use and air traffic statistics to the DOT. The ten passenger airlines considered reported 87% of all fuel use reported by passenger carriers included in the DOT Form 41 database. The four cargo airlines considered account for 87% of all carrier cargo fuel use and approximately 10% of total fuel use reported on DOT Form 41 by all US carriers (passenger and cargo).

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By airline comparison of DOT Form 41 reported departures, distance and fuel burned with 1999 scheduled inventory global totals for selected passenger carriers. Table 4-1.

| | Ď | Departures/Year | 'ear | Departures/Year Distan | Distance/Year (km) | (m | Fuel | Fuel Burned/Year (Kg) | r (Kq) |
|-----------------------------|-------------|-------------------|---------|------------------------|--------------------|---------|----------|-----------------------|---------|
| Air Carrier | DOT | Inventory % Diff. | % Diff. | рот | Inventory | % Diff. | DOT | Inventory % Diff. | % Diff. |
| | | | | | | | | | |
| United Air Lines | 8.20E+05 8. | 8.59E+05 | 5% | 1.06E+09 | 1.10E+09 | 4% | 9.38E+09 | 7,68F+09 | -18% |
| USAir | 7.11E+05 | 6.84E+05 | -4% | 5.04E+08 | 5.26E+08 | 4% | 3.38E+09 | 2.70E+09 | ~0~- |
| America West Airlines | | 2.10E+05 2.17E+05 | 3% | 2.09E+08 | 2.16E+08 | 4% | 1.26E+09 | 9.81E+08 | -22% |
| American Airlines | 8.18E+05 8. | 8.45E+05 | 3% | 1.13E+09 | 1.16E+09 | 2% | 8.88E+09 | 7.10E+09 | -20% |
| Alaska Airlines | 1.70E+05 | 1.75E+05 | 3% | 1.50E+08 | 1.55E+08 | 3% | 9.37E+08 | 7.52E+08 | -20% |
| Delta Air Lines | 9.58E+05 9. | 9.32E+05 | -3% | 9.37E+08 | 9.44E+08 | 1% | 8.33E+09 | 6.55E+09 | -21% |
| Northwest Airlines | 5.85E+05 6. | 6.00E+05 | 3% | 6.09E+08 | 6.19E+08 | 2% | 6.24E+09 | 4.96E+09 | -21% |
| Southwest Airlines | 8.48E+05 8. | 8.59E+05 | 1% | 4.54E+08 | 4.60E+08 | 1% | 2.84E+09 | 2.27E+09 | -20% |
| Trans World Airlines | 2.87E+05 | 2.91E+05 | 1% | 2.78E+08 | 2.78E+08 | %0 | 2.09E+09 | 1.61E+09 | -23% |
| Continental | 4.82E+05 4. | 4.78E+05 | -1% | 6.18E+08 | 6.11E+08 | -1% | 4.85E+09 | 3.49E+09 | -28% |
| | | | | | | | | | |
| Passenger Carrier Totals | 5.89E+06 | 5.89E+06 5.94E+06 | 1% | 5.95E+09 | 6.07E+09 | 2% | 4 82E-10 | 4 82E±10 3 81E±10 | -01% |
| | | | | | | 2.1 | | 011100 | 0/17- |
| | | | | | | | | | |

By airline comparison of DOT Form 41 reported departures, distance and fuel burned with 1999 scheduled inventory dishal totals for selected cardo carriers Table 4-2.

| Inveniory | inventory global totals for selected cargo carriers. | tor selected | ed cargo | carriers. | | | | | |
|--|--|-------------------|----------|-------------------|--------------------|---------|-------------------|------------------------|-------------|
| | De | Departures/Year | /ear | Dista | Distance/Year (km) | (m | Fuel | Fuel Burned/Year (Kg) | (Ka) |
| Air Carrier | DOT | Inventory % Diff. | % Diff. | DOT | Inventory % Diff. | % Diff. | DOT | Inventory % Diff | % Diff. |
| | | | | | | | 1 | | |
| Federal Express | 3.36E+05 5.07E+04 -85% | 5.07E+04 | | 2.39E+08 9.02E+07 | 9.02E+07 | -62% | 2.58E+09 1.02E+09 | 1.02E+09 | -60% |
| Emery Worldwide | 7.48E+04 4.26E+04 | 4.26E+04 | -43% | 8.38E+07 | 4.10E+07 | -51% | 6.18E+08 | 3.60E+08 | -42% |
| DHL Airways | 7.83E+04 5.22E+04 | 5.22E+04 | -33% | 3.78E+07 | 3.18E+07 | -16% | 2.88E+08 | 1.99E+08 | -31% |
| United Parcel Service 1.33E+05 1.26E+05 | 1.33E+05 | 1.26E+05 | -5% | 1.49E+08 1.29E+08 | 1.29E+08 | -13% | 1.57E+09 | 1.12E+09 | -29% |
| | | | | | | | | | 1 - - |
| Cargo Carrier Totals 6.22E+05 2.71E+05 -56% 5.09E+08 2.92E+08 -43% | 6.22E+05 | 2.71E+05 | -56% | 5.09E+08 | 2.92E+08 | -43% | 5.06E+09 | 5.06E+09 2.69E+09 -47% | -47% |

Table 4-1 shows the results of the comparison of yearly totals for departures, distance traveled and fuel burned for the ten passenger carriers considered. Comparisons are made on a percent difference basis relative to the DOT Form 41 reported values. A negative percent difference denotes that 1999 emission inventory values are lower than those reported on DOT Form 41.

Table 4-1 shows that total departures and distance flown agree within 5 percent for all of the ten passenger air carriers considered with the differences in total departures and distance traveled for the ten passenger carriers being 1 percent and 2 percent respectively. The agreement for total departures and distance traveled is reasonably good considering that the OAG schedule data used to calculate the 1999 emission inventory is based on projections of air traffic demand. Both flight cancellations and code sharing between airlines or their subsidiaries will contribute to the differences.

Because total departures and distance traveled are in relatively good agreement, comparisons of fuel burned between the two data sets may be used to give an indication of how well the emission inventory calculations predicted fuel burned for the ten passenger airlines considered. For the passenger air carriers listed in Table 4-1, the inventory calculations under predicted total fuel by 21 percent on average. The differences in fuel burned for passenger carriers are similar to those found in a similar analysis of 1992 scheduled aircraft emission inventory results (Daggett, *et al*, 1999). The majority of these differences are likely due to the simplifying assumptions made regarding the performance calculations used in creating the emission inventory. Major factors here are the effect of air traffic control, the effect of weather and winds, assumed payload, cargo load, and the assumption of great circle routing between airports.

Table 4-2 shows the results of the comparison of yearly totals for departures, distance traveled and fuel burned for the four cargo carriers considered in this analysis. This table shows that, for the four cargo carriers considered, the total departures and total distance traveled calculated in the 1999 scheduled aircraft emission inventory are significantly less than those reported in the DOT Form 41 data. The inventory under predicts total departures and distance traveled by 56 percent and 43 percent respectively on average. This indicates that the OAG flight schedule data used to create the 1999 scheduled aircraft fleet emission inventory do not contain a complete listing of flights flown by cargo carriers. Fuel use by these four selected cargo carriers was under predicted by 47 percent on average. Similar behavior was observed for DOT Form 41 comparisons made for 1992 emission inventory results (Daggett, *et al*, 1999).

To put the under prediction of cargo flights in perspective, the fuel use reported on DOT Form 41 by all cargo carriers for 1999 was approximately 10 percent of the fuel use reported by all carriers (passenger and cargo). Thus, missing the cargo carrier fuel use by approximately 50 percent in the emission inventory would correspond to an error of approximately 5 percent in the calculated fuel use by all US carriers.

Although this percentage may not necessarily be representative for non-U.S. carriers, it is large enough to justify further investigation of the effect that the lack of coverage of cargo flights in the OAG has on global emission inventory calculations. An investigation of this type is not within the scope of the current work but should be considered for future study.

Overall, this comparison indicates that the OAG data are relatively complete, at least for US carriers, but that there is a systematic under prediction of fuel use of approximately 21 percent in the emission inventories. For cargo carriers, the comparison indicates that there is a systematic under counting of cargo flights in the OAG data with which we are working. This would introduce an additional 5 percent under prediction in the inventory calculations of US carriers. It is unclear how to extend these results to global totals or how to account for them explicitly in the 3-dimensional emission inventory calculation.

5. Summary and Conclusions

Emissions produced by the world's entire aircraft fleet come from scheduled, military, charter and general aviation air traffic. In this report, we only present the results and methodology used for the calculation of emissions from scheduled air traffic which includes turboprops, passenger jets, and jet cargo aircraft.

Global fuel use for 1999 by scheduled air traffic was calculated to be 1.28×10^{11} kilograms. Global NOx emissions by scheduled air traffic in 1999 were calculated to be 1.69×10^{9} kilograms (as NO₂). The calculated global emissions show a seasonal variation, peaking in August with a minimum in February. Emissions for the month of December 1999 were closest to global annual average emissions, although emissions for May (the month typically used as an 'average' month in past NASA inventory studies) were within 1 percent of the global annual average.

A trend analysis for emissions and fuel burned was performed using the results of this current work and previously published emission inventories and scenarios. This analysis showed an increase in the absolute amount of fuel burned, distance traveled, NOx, and CO emissions produced by the scheduled fleet between 1992 and 1999 and a decrease in the absolute amount of hydrocarbon emissions produced. Calculated global fuel use increased by 33% and NOx emissions increased by 35% between 1992 and 1999. The analysis also showed that scheduled fleet fuel burned and NOx emissions normalized by available seat kilometers decreased between 1992 and 2015.

The methodology used to extract and process air traffic data from the Official Airline Guide was changed from that used to calculate previous scheduled fleet inventories for 1976, 1984 and 1992. To quantify the effects of the methodology changes, an emission inventory for August 1992 was recalculated using the new methodology. Comparisons between the previously published and new August 1992 inventories show good agreement for global fuel burned and NOx totals. For CO and hydrocarbons, the global totals increased by 20 percent and 18 percent respectively with the use of the new methodology. Much of this difference arises from the different combustor types selected in the two methodologies for certain engines in the fleet. Emissions from a specific engine model can vary widely depending on the combustor that is installed in the engine.

To improve the accuracy of global emissions calculations for freighters, United States Department of Transportation Form T-100 data were used to determine typical payloads for freighter aircraft. This information was then used to model freighter aircraft more accurately in the inventory calculations by using more realistic payloads.

To assess the effect of the different freighter payload assumptions, results were compared with previous inventory calculations done using 70 percent passenger payload for all aircraft. This comparison showed that improved freighter payload assumptions increased total global fuel burned by 0.6 percent and increased total global NOx by 1.5 percent for August 1999. These increases are relatively small and will not significantly change trends for fuel use or NOx created using the published inventories for 1976, 1984, and 1992.

In order to evaluate the 1999 scheduled aircraft fleet global emission inventory calculations, comparisons were made with aviation fuel use and traffic data reported on the U.S. Department of Transportation (DOT) Form 41 by US air carriers. In general, emission inventory calculations of departures and distance traveled for 1999 compared well (within 5 percent) with the DOT Form 41 data for the ten largest passenger carriers. In contrast, for the four largest cargo carriers, departures and distance traveled calculated were significantly less than those reported on DOT Form 41. It appears that the OAG flight schedule data do not contain a complete listing of cargo flights.

For the passenger carriers in the DOT Form 41 data comparison, the emission inventory calculations consistently under-predicted fleet fuel burned. The magnitude of these under-predictions varied depending on the carrier being considered. For the ten largest air carriers, the total fuel burn was underpredicted by 21 percent. This result is likely due to the simplifying assumptions used in the development of the global inventory, including our inability to consider air traffic control delays/diversions, weather/wind factors, more realistic routing, less than optimum aircraft/engine performance and actual aircraft operating weights.

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Appendix A – Sample Airclaims Fleet Information Data

This Appendix contains a sample of the fleet information obtained from the Airclaims database that was used to assign engines to aircraft listed in the filtered OAG flight schedule. The sample data in this appendix show the Japan Airlines fleet as it existed on May 16, 1999.

| Carrier | Carrier | | | | . | | |
|----------------|---------|--|---|--|--|---|-----------------------------|
| Carrier Name | Code | Aircraft Type | Aircraft Variant | Aircraft Usage | Engine | Engine | Aircraft in |
| Japan Airlines | JAL | 737 (CFMI) | 400 | All Passenger | CFM56 | 3C1 | Service 4 |
| Japan Airlines | JAL | 747 747 747 | 100 100B/SR (SUD) (P&W) 100B/SR (P&W) | All Passenger All Passenger All Passenger | 061L 019D 051L | 7A 77 77 | N N - |
| Japan Airlines | JAL | 747 747 747 747 747 747 747 747 | 200B (P&W) 200B (P&W) 200B (P&W) 200B (P&W) 200F (SCD) (P&W) 200F (SCD) (P&W) 200F (SCD) (P&W) 200F (SCD) (P&W) 200SF (P&W) | All Passenger All Passenger All Passenger All Fassenger All Freight / Cargo All Freight / Cargo All Freight / Cargo All Freight / Cargo | 061L 061L 061L 061L 061L 061L 061L 061L | 70 78 784G2 78 70 70 70 70 | - ©いろくオターー・ |
| Japan Airlines | JAL | 747 | 300 (P&W) | All Passenger | JT9D | 7R4G2 | · £ |
| Japan Airlines | JAL | 747 747 | 400 (GE) 400D (GE) | All Passenger All Passenger | CF6 CF6 | 80C2B1F 80C2B1F | 8 5 <u>3</u> |
| Japan Airlines | JAL | 767 | 200 (P&W) | All Passenger | JT9D | 7R4D | с О |
| Japan Airlines | JAL | 767 767 767 | 300 (P&W) 300 (GE) 300 (GE) | All Passenger All Passenger All Passenger | JT9D CF6 CF6 | 7R4D 80C2B4F 80C2B2 | 1 4 - |
| Japan Airlines | JAL | 777 | 200 (P&W) | All Passenger | PW4000 | 4077 | ى |
| Japan Airlines | JAL | <i>717</i> | 300 (P&W) | All Passenger | PW4000 | 4090 | 4 |
| Japan Airlines | JAL | DC-10 DC-10 | 40I 40D | All Passenger All Passenger | JT9D JT9D | 59A 59A | 04 |
| Japan Airlines | JAL | MD-11 | Passenger (P&W) | All Passenger | PW4000 | 4460 | 10 |
| | | | | | | | |

1 Appendix A – Samnle Airclaims Fleet

Appendix B – Airplane/Engine Substitution Tables for 1999 Emissions Inventory Calculations

This Appendix contains a list of each aircraft/engine combination listed in the filtered OAG flight schedule and the performance aircraft and emissions engine that was used to model it. Each emissions engine name has a prefix that represents its unique ID number in the ICAO Engine Emissions Databank. Some emissions data used in the creation of the 1999 inventory had not been published as of the writing of this report and was obtained directly from the engine companies. These emissions engines are listed with the internal Boeing prefix of the form "PREXXX_".

| Schedule Airplane | Schedule Engine | Performance Airplane | Performance Engine | Emissions Engine |
|----------------------|-----------------|-------------------------|-----------------------|-----------------------|
| 100-* | DD 100 600 1F | | | |
| 100-* | | FUKKEH-100 | TAY-650 | 1RR020_TAYMk620-15 |
| | | FUKKEH-100 | TAY-650 | 188021 TAVMLGED 15 |
| 140-100 | ALF502-R-5 | BAE146-200 | ALF502R-5 | |
| 146-200 | ALF502-R-5 | BAE146-200 | ALF502B-5 | |
| 146-300 | ALF502-R-5 | BAE146-200 | | |
| 146-300 | LF507-1H | B.I-100 | | 11LUU3_ALF502H-5 |
| 146-300QT_FRT | ALF502-R-5 | BAF146-300 | LI 30/ Al Ernadi F | 11L004_LF507-1F-1H |
| 318 | Blank-Blank | 737-500 | | 11L003_ALF502R-5 |
| *-02 | BB 183-620-15 | | UTIVID0-3-B1-18.5 | 1CM004_CFM56-3-B1 |
| 707-320C | | | MAHK-620-15 | 1RR020_TAYMk620-15 |
| 707-320C AIL EDT | | /0/-320B-C | JT3D-3B | 1PW001_JT3D-3B |
| | 130-35 TER 2 | 707-320B-C | JT3D-3B | 1PW001 JT3D-3B |
| | J13D-/ | 707-320B-C | JT3D-3B | 1PW001 IT3D-3R |
| /U/-320C_FHI | JT3D-3B | 707-320B-C | JT3D-3B | |
| /07-320C_FRT | JT3D-7 | 707-320B-C | IT3D-3B | |
| ZOM | Blank-Blank | 707-320B-C | T3D-3E | |
| 717-200 | BR700-715C | MD-95-30 | | |
| 721 | Blank-Blank | 797-100 | | 4BH005_BH700-715A1-30 |
| 727-100 | ITAD-7 | 001-171 | 118U-7 | 1PW004_JT8D-7series |
| 727-100 | | 727 :20 | J18D-7 | 1PW004_JT8D-7series |
| 727-100 | | /2/-100 | JT8D-7 | 1PW004 JT8D-7series |
| 707 100 | J18D-9 | 727-100 | JT8D-9 | 1PW006 JT8D-9series |
| 001-121 202 - 202 | AB-18U-9A | 727-100 | JT8D-9 | 1PW006 .ITRD-0ceries |
| | J18D-9 | 727-100 | JT8D-9 | |
| 727-100C_CMB | JT8D-7 | 727-100 | .ITRD-7 | |
| 727-100C_CMB | JT8D-7B | 727-100 | | IP WUU4_J18U-7series |
| 727-100C FRT | JT8D-7 | 727 100 | | 1PW004_JT8D-7series |
| 727-100F FRT | ITRD-7R | 202 100 | | 1PW004_JT8D-7series |
| 727-100F FRT | TRD-9 | 101-121 | J18D-7 | 1PW004_JT8D-7series |
| 727-1000C FRT | ITBD-00 | 001-121 | J18L-9 | 1PW006_JT8D-9series |
| 727-100QF FRT | BB 183-651-54 | 100 - 727 | J18D-9 | 1PW006_JT8D-9series |
| 727-200 | JT8D-15 | 727-200 | J18D-7 | 1PW004_JT8D-7series |
| | | | A18U-15-75A | 1PW009_JT8D-15 |

| Airplane/Engine Substitution Tables for 1999 Emissions Inventory Calculations |
|---|
| Appendix B – Airplane/Er |

| Schedule Airplane | Schedule Engine | Perrormance Airplane | Performance Engine | Emissions Engine |
|-------------------|-----------------|-------------------------|--------------------|---------------------|
| | | | | |
| 727-200 | JT8D-17 | 727-200 | JT8D-15-15A | 1PW012_JT8D-17 |
| 727-200 | JT8D-17A | 727-200 | JT8D-15-15A | 1PW010_JT8D-15 |
| 727-200 | JT8D-17R | 727-200 | JT8D-15-15A | 1PW016_JT8D-17R |
| 727-200 | JT8D-7B | 727-200 | JT8D-9 | 1PW004 JT8D-7series |
| 727-200 | JT8D-9 | 727-200 | JT8D-9 | 1PW006 JT8D-9series |
| 727-200 | JT8D-9A | 727-200 | JT8D-9 | 1PW006_JT8D-9series |
| 727-200F_FRT | JT8D-15 | 727-200 | JT8D-15-15A | 1PW009_JT8D-15 |
| 727-200F_FRT | JT8D-17 | 727-200 | JT8D-15-15A | 1PW012_JT8D-17 |
| 727-200F_FRT | JT8D-17R | 727-200F | JT8D-15-15A | 1PW016_JT8D-17R |
| 727-200F_FRT | JT8D-7 | 727-200 | JT8D-9 | 1PW006_JT8D-9series |
| 727-200F_FRT | JT8D-9 | 727-200 | JT8D-9 | 1PW006_JT8D-9series |
| 727-200RE | JT8D-Two217C | 727-200 | JT8D-9 | 1PW006_JT8D-9series |
| 731 | Blank-Blank | 737-100 | JT8D-9 | 1PW006_JT8D-9series |
| 737-100 | JT8D-7A | 737-100 | JT8D-9 | 1PW016_JT8D-17R |
| 737-200 | JT8D-15 | 737-200 | JT8D-15 | 1PW009_JT8D-15 |
| 737-200 | JT8D-15A | 737-200 | JT8D-15 | 1PW011_JT8D-15A |
| 737-200 | JT8D-17 | 737-200 | JT8D-15 | 1PW012_JT8D-17 |
| 737-200 | JT8D-17A | 737-200 | JT8D-15 | 1PW014_JT8D-17A |
| 737-200 | JT8D-7 | 737-200 | JT8D-7 | 1PW004_JT8D-7series |
| 737-200 | JT8D-9 | 737-200ADV | JT8D-9-9A | 1PW006_JT8D-9series |
| 737-200 | JT8D-9A | 737-200ADV | JT8D-9-9A | 1PW006_JT8D-9series |
| 737-200C | JT8D-15 | 737-200 | JT8D-15 | 1PW009_JT8D-15 |
| 737-200C | JT8D-17 | 737-200 | JT8D-15 | 1PW012_JT8D-17 |
| 737-200C | JT8D-17A | 737-200 | JT8D-15 | 1PW014_JT8D-17A |
| 737-200C | JT8D-9A | 737-200ADV | JT8D-9-9A | 1PW006_JT8D-9series |
| 737-200C_CMB | JT8D-17 | 737-200 | JT8D-15 | 1PW012_JT8D-17 |
| 737-200C_CMB | JT8D-9A | 737-200ADV | JT8D-9-9A | 1PW006_JT8D-9series |
| 737-200C_QC | JT8D-15 | 737-200 | JT8D-15 | 1PW009_JT8D-15 |

| | | Performance | | |
|-------------------|-----------------|-------------|--------------------|----------------------|
| Schedule Airplane | Schedule Engine | Airplane | Performance Engine | Emissions Engine |
| | | | | |
| 737-200C_QC | JT8D-15A | 737-200 | JT8D-15 | 1PW011_JT8D-15A |
| 737-200C QC | JT8D-17A | 737-200 | JT8D-15 | 1PW014_JT8D-17A |
| 737-200C QC | JT8D-9 | 737-200 | JT8D-7 | 1 PW006_JT8D-9series |
| 737-200QC | JT8D-9A | 737-200 | JT8D-7 | 1PW006_JT8D-9series |
| 737-200QC_FRT | JT8D-15 | 737-200 | JT8D-15 | 1PW009_JT8D-15 |
| 737-200QC_FHT | JT8D-9A | 737-200ADV | JT8D-9-9A | 1PW006_JT8D-9series |
| 737-200QC_QC | JT8D-9A | 737-200ADV | JT8D-9-9A | 1PW006_JT8D-9series |
| 737-300 | CFM56-3B1 | 737-300 | CFM56-3-B1 | 1CM004_CFM56-3-B1 |
| 737-300 | CFM56-3B2 | 737-300 | CFM56-3-B1 | 1CM004_CFM56-3-B1 |
| 737-300 | CFM56-3C1 | 737-300 | CFM56-3-B1 | 1CM004_CFM56-3-B1 |
| 737-300QC_QC | CFM56-3C1 | 737-300 | CFM56-3-B1 | 1CM004_CFM56-3-B1 |
| 737-400 | CFM56-3B2 | 737-300 | CFM56-3-B1 | 1CM005_CFM56-3B-2 |
| 737-400 | CFM56-3C1 | 737-300 | CFM56-3-B1 | 1CM005_CFM56-3B-2 |
| 737-500 | CFM56-3B1 | 737-500 | CFM56-3-B1-18.5 | 1CM007_CFM56-3C-1 |
| 737-500 | CFM56-3C1 | 737-500 | CFM56-3-B1-18.5 | 1CM007_CFM56-3C-1 |
| 737-600 | CFM56-7B20 | 737-600 | CFM56-7B18 | 3CM029_CFM56-7B18 |
| 737-700 | CFM56-7B22 | 737-700 | CFM56-7B20 | 3CM030_CFM56-7B20 |
| 737-700 | CFM56-7B24 | 737-700 | CFM56-7B20 | 3CM030_CFM56-7B20 |
| 737-800 | CFM56-7B24 | 737-800 | CFM56-7B24 | 3CM032_CFM56-7B24 |
| 737-800 | CFM56-7B26 | 737-800 | CFM56-7B27 | 3CM034_CFM56-7B27 |
| 737-800 | CFM56-7B27 | 737-800 | CFM56-7B27 | 3CM034_CFM56-7B27 |
| 747-100 | JT9D-7 | 747-100-200 | JT9D-7A | 1PW021_JT9D-7A |
| 747-100 | JT9D-7A | 747-100-200 | JT9D-7A | 1PW021_JT9D-7A |
| 747-100B | RB211-524C2 | 747-200 | RB211-524C | 1RR006_RB211-524C2 |
| 747-100B_SR | JT9D-7A | 747-100-200 | JT9D-7A | 1PW021_JT9D-7A |
| 747-100F_FRT | JT9D-7A | 747-100F | JT9D-7F | 1PW021_JT9D-7A |
| 747-200B | CF6-50E2 | 747-100-200 | CF6-50E2 | 1GE009_CF6-50E2 |
| 747-200B | JT9D-70A | 747-100-200 | JT9D-7A | 1PW021_JT9D-7A |

| | | Performance | | |
|-------------------|-----------------|--------------|--------------------|--------------------|
| Schedule Airplane | Schedule Engine | Airplane | Performance Engine | Emissions Engine |
| 217 200B | IT9D-7A | 747-100-200 | JT9D-7A | 1PW021_JT9D-7A |
| 747-200B | .179D-7AW | 747-100-200 | JT9D-7A | 1PW021_JT9D-7A |
| 747-200B | JT9D-7F | 747-200 | JT9D-7J | 1PW023_JT9D-7F |
| 747-200B | JT9D-7J | 747-200 | JT9D-7J | 1PW024_JT9D-7J |
| 747-200B | JT9D-7Q | 747-200B-C-F | JT9D-7Q | 1PW025_JT9D-7Q |
| 747-200B | JT9D-7Q3 | 747-200B-C-F | JT9D-7Q | 1PW025_JT9D-7Q |
| 747-200B | JT9D-7R4G2 | 747-200 | JT9D-7R4G2 | 1PW029_JT9D-7R4G2 |
| 747-2008 | RB211-524D4 | 747-200 | RB211-524D4U | 1RR007_RB211-524D4 |
| 747-200B CMB | CF6-50E | 747-100-200 | CF6-50E2 | 1GE009_CF6-50E2 |
| 747-200B CMB | CF6-50E2 | 747-100-200 | CF6-50E2 | 1GE009_CF6-50E2 |
| 747-200B CMB | JT9D-7Q | 747-200B-C-F | JT9D-7Q | 1PW025_JT9D-7Q |
| 747-200C F FRT | CF6-50E2 | 747-300F | CF6-50E2 | 1GE009_CF6-50E2 |
| 747-200C OC | CF6-50E2 | 747-100-200 | CF6-50E2 | 1GE009_CF6-50E2 |
| 747-200F FRT | CF6-50E2 | 747-300F | CF6-50E2 | 1GE009_CF6-50E2 |
| 747-200F FRT | JT9D-7F | 747-200F | JT9D-7J | 1PW024_JT9D-7J |
| 747-200F FRT | JT9D-7J | 747-200F | JT9D-7J | 1PW024_JT9D-7J |
| 747-200F FRT | JT9D-7Q | 747-200F | JT9D-7J | 1PW024_JT9D-7J |
| 747-200F FRT | JT9D-7R4G2 | 747-200F | JT9D-7J | 1PW024_JT9D-7J |
| 747-200F FRT | RB211-524D4 | 747-200F | RB211-524D4 | 1RR008_RB211-524D4 |
| 747-200SF FRT | CF6-50E2 | 747-300F | CF6-50E2 | 1GE009_CF6-50E2 |
| 747-200SF FRT | JT9D-7J | 747-200F | JT9D-7J | 1PW024_JT9D-7J |
| 747-200SF FRT | JT9D-7Q | 747-200F | JT9D-7J | 1PW024_JT9D-7J |
| 747-200SF FRT | JT9D-7R4G2 | 747-200F | JT9D-7J | 1PW024_JT9D-7J |
| 747-200SF FRT | RB211-524D4 | 747-200F | RB211-524D4 | 1RR007_RB211-524D4 |
| | CF6-50E2 | 747-300 | CF6-50E2 | 1GE009_CF6-50E2 |
| 747-300 | CF6-80C2B1 | 747-300 | CF6-80C2B1 | 1GE022_CF6-80C2B1 |
| 747-300 | JT9D-7R4G2 | 747-300 | JT9D-7R4G2 | 1PW029_JT9D-7R4G2 |
| 747-300 | RB211-524C2 | 747-300 | RB211-524D4UP | 1RR008_RB211-524D4 |

| | | Performance | | |
|-------------------|-----------------|---------------|--------------------|---|
| Schedule Airplane | Schedule Engine | Airplane | Performance Engine | Emissions Engine |
| 006 247 | | | | |
| | 4042C-112GH | /4/-300 | RB211-524D4UP | 1RR007 RB211-524D4 |
| /4/-300_CMB | CF6-50E2 | 747-300 | CF6-50E2 | 1GE009 CF6-50F2 |
| 747-300_CMB | CF6-80C2B1 | 747-300 | CF6-80C2B1 | |
| 747-300_CMB | JT9D-7R4G2 | 747-300 | JT9D-7R4G2 | |
| 747-300_SR | JT9D-7R4G2 | 747-300 | JT9D-7R4G2 | 1 1 1 1 1 2 1 3 1 3 1 4 5 2 1 2 1 2 2 1 2 1 2 2 1 2 2 1 2 2 2 2 |
| 747-400 | CF6-80C2B1F | 747-400 | CF6-80C2-B1F | |
| 747-400 | PW4000-4056 | 747-400 | PW4056 | 1PW041 PW4056 |
| 747-400 | RB211-524G | 747-400 | RB211-524G | 188010 BB211-524G |
| | RB211-524H2 | 747-400 | RB211-524G | 188011 88211-524H |
| 747-400F_FRT | CF6-80C2B1F | 747-400F | CF6-80C2B1F | 2GE045 CE6-80C2B1E |
| 747-400F_FRT | PW4000-4056 | 747-400F | PW4056 | 1PW041 PW4056 |
| 747-400F_FRT | RB211-524H2 | 747-400F | RB211-524H | 18B011 8B011-60AH |
| 747-400_CMB | CF6-80C2B1F | 747-400 | CF6-80C2-B1F | |
| 747-400_CMB | PW4000-4056 | 747-400 | PW4056 | |
| 747-SP | JT9D-7A | 747SP | JT9D-7A | |
| 747-SP | JT9D-7F | 747SP | JT9D-7A | |
| 747-SP | JT9D-7FW | 747SP | A7-06TL | |
| 747-SP | JT9D-7J | 747SP | AT9D-7A | |
| 747-SP | RB211-524D4 | 747SP | RB211-524C2 | |
| 747-SR-100B | CF6-45A2 | 747-100-100SR | CF6-45A2 | 16F005 CF6-45A2 |
| 757-200 | PW2000-2037 | 757-200 | PW2037 | PBE113 PW2037 |
| 757-200 | PW2000-2040 | 757-200 | PW2040 | PBE114 PW2040 |
| 757-200 | RB211-535C | 757-200 | RB211-535C | 18010 00011 FOED |
| 757-200 | RB211-535E4 | 757-200 | BB211-535E4 | 388008 00011 50554 |
| 757-200 | RB211-535E4B | 757-200 | RP11-535E4 | 388034 88344 53574 |
| | PW2000-2040 | 757-200 | PW2040 | |
| 757-200PF_FRT | RB211-535E4 | 757-200 | RP211-535F4 | 388038 88314 52554 |
| 767-200 | CF6-80A | 767-200 | CF6-80A | 166010 CF6-80A |
| | | | | |

| | | Performance | | |
|-------------------|-----------------|-------------|--------------------|------------------------|
| Schedule Airplane | Schedule Engine | Airplane | Performance Engine | Emissions Engine |
| | | 767-200 | .IT9D-7R4D | 1PW026 JT9D-7R4D-7R4D1 |
| /6/-200 | | 767 200 | CEGROA | 1GE010 CF6-80A |
| 767-200EM | CF6-8UAZ | | | |
| 767-200EM | JT9D-7R4D | 767-200 | J19D-/H4U | |
| 767-200ER | CF6-80A | 767-200ER | CF6-80C2B4F | 1GE028_CF6-80C2B4F |
| 767-200ER | CF6-80C2B2 | 767-200ER | CF6-80C2B4F | 1GE025_CF6-80C2B2 |
| 767-200FB | CF6-80C2B4 | 767-200ER | CF6-80C2B4F | 1GE027_CF6-80C2B4 |
| 767-200FR | CF6-80C2B4F | 767-200ER | CF6-80C2B4F | 1GE028_CF6-80C2B4F |
| 767-200FR | JT9D-7R4E | 767-200 | JT9D-7R4D | 1PW027_JT9D-7R4E-7R4E1 |
| 767-200FB | JT9D-7R4E4 | 767-200 | JT9D-7R4D | 1PW028_JT9D-7R4E4-E1 |
| 767-200ER | PW4000-4056 | 767-200ER | PW4056 | 1PW042_PW4056 |
| 767-200ER | PW4000-4060 | 767-200 | CF6-80A | 1GE010_CF6-80A |
| 767-200FBM | JT9D-7R4E | 767-200 | JT9D-7R4D | 1PW027_JT9D-7R4E-7R4E1 |
| 767-200PC FRT | CF6-80A | 767-200 | CF6-80A | 1GE010_CF6-80A |
| 1 | CF6-80C2B2 | 767-300 | CF6-80A2 | 1GE012_CF6-80A2 |
| 767-300 | CF6-80C2B2F | 767-300 | CF6-80A2 | 1GE012_CF6-80A2 |
| 767-300 | CF6-80C2B4F | 767-300 | CF6-80A2 | 1GE012_CF6-80A2 |
| 767-300 | JT9D-7R4D | 767-300 | JT9D-7R4E | 1PW027_JT9D-7R4E-7R4E1 |
| 767-300 | PW4000-4056 | 767-300 | CF6-80A2 | 1GE012_CF6-80A2 |
| 767-300FR | CF6-80C2B2 | 767-300ER | CF6-80C2B6F | 1GE025_CF6-80C2B2 |
| 767-300FR | CF6-80C2B4 | 767-300ER | CF6-80C2B6F | 1GE027_CF6-80C2B4 |
| 767-300FR | CF6-80C2B4F | 767-300ER | CF6-80C2B6F | 1GE028_CF6-80C2B4F |
| 767-300ER | CF6-80C2B6 | 767-300ER | CF6-80C2B6F | 1GE029_CF6-80C2B6 |
| 767-300FR | CF6-80C2B6F | 767-300ER | CF6-80C2B6F | 2GE048_CF6-80C2B6F |
| 767-300FB | CF6-80C2B7F | 767-300ER | CF6-80C2B6F | 2GE055_CF6-80C2B7F |
| 767-300FB | PW4000-4056 | 767-300ER | PW4060 | 1PW041_PW4056 |
| 767-300FB | PW4000-4060 | 767-300ER | PW4060 | 1PW041_PW4056 |
| 767-300FR | PW4000-4062 | 767-300ER | PW4060 | 1PW041_PW4056 |
| 767-300FR | RB211-524H2 | 767-300ER | RB211-524H | 1RR011_RB211-524H |
| 767-300ER | RB211-524H3 | 767-300ER | RB211-524H | 1RR011_RB211-524H |

| Schedule Airplane | Schedule Engine | Performance Airplane | Performance Engine | Emissione Envine |
|-------------------|-----------------|-------------------------|--------------------|--------------------|
| | | |) | |
| 767-300ERF_FRT | CF6-80C2B6F | 767-300ER | CF6-R0C2R6F | 1GEN30 CE6 SOCODOL |
| 767-300ERF_FRT | CF6-80C2B7F | 767-300ER | CF6-BOC2B6F | |
| 777-200 | PW4000-4074 | 777-200 | PW4084 | |
| 777-200 | PW4000-4077 | 777-200 | PWADBA | |
| 777-200 | Trent-875 | 777-200 | TRENT877 | |
| 777-200 | Trent-877 | 777-200 | TRENTR77 | |
| 777-200ER | GE90-85B | 777-200ER | GE90-85B | |
| 777-200ER | GE90-92B | 777-200ER | GE90-90B | 3GEDES GEOD ODD |
| 777-200ER | PW4000-4090 | 777-200ER | PW4084 | |
| 777-200ER | Trent-884 | 777-200ER | TRENT877 | 288025 Trant877 |
| 777-200ER | Trent-892 | 777-200ER | TRENT877 | 288025_11511077 |
| 777-300 | PW4000-4090 | 777-300 | PW4090 | |
| 777-300 | Trent-892 | 777-300 | TRENT892 | 2RR07 Trentago |
| A300-600 | CF6-80C2A3 | A300-600R | CF6-80C2 | |
| A300-600R | CF6-80C2A5 | A300-600R | CF6-80C2 | |
| | CF6-80C2A5F | A300-600R | CF6-80C2 | |
| A300-600_FRT | CF6-80C2A5F | A300-600R | CF6-80C2 | |
| A300-620 | JT9D-7R4H1 | A300-621R-ER | JT9D-7R4H1 | |
| A300-620 | PW4000-4158 | A300-622R-ER | PW4056 | 1PW048 PW4158 |
| A300-620R | PW4000-4158 | A300-622R-ER | PW4056 | 1PW048 PW4158 |
| A300-B2-100 | CF6-50C | A300-B2-B4 | CF6-50C2 | 1GF007 CF6-50C1-C2 |
| A300-B2-200 | CF6-50C2 | A300-B2-B4 | CF6-50C2 | 1GE007 CE6-5001-02 |
| A300-B2-200 | CF6-50C2R | A300-B2-B4 | CF6-50C2 | |
| A300-B2-200FF | CF6-50C2 | A300-B2-B4 | CF6-50C2 | |
| A300-B4-100 | CF6-50C2 | A300-B2-B4 | CF6-50C2 | |
| A300-B4-100 | CF6-50C2R | A300-B2-B4 | CF6-50C2 | 1GEND8 CES.ENCOD |
| A300-B4-120 | JT9D-59A | A300-621R-ER | JT9D-7R4H1 | 1PW033 .1T9D-594 |
| A300-B4-200 | CF6-50C2 | A300-B2-B4 | CF6-50C2 | 1GE007_CF6-50C1-C2 |

Appendix B – Airplane/Engine Substitution Tables for 1999 Emissions Inventory Calculations

| | | Performance | | |
|-------------------|-----------------|-------------|--------------------|------------------------|
| Schedule Airplane | Schedule Engine | Airplane | Performance Engine | Emissions Engine |
| A300-B4-200FF | CF6-50C2 | A300-B2-B4 | CF6-50C2 | 1GE007 CF6-50C1-C2 |
| A300-B4-200F FRT | CF6-50C2 | A300-B2-B4 | CF6-50C2 | 1GE007_CF6-50C1-C2 |
| A300-F4-200 FRT | CF6-50C2 | A300-B2-B4 | CF6-50C2 | 1GE007_CF6-50C1-C2 |
| | CF6-80A3 | A310-300 | CF6-80A3 | 1GE013_CF6-80A3 |
| A310-200 | CF6-80C2A2 | A310-300 | CF6-80C2A2 | 1GE016_CF6-80C2A2 |
| A310-220 | JT9D-7R4D1 | A310-300 | JT9D-7R4E1 | 1PW027_JT9D-7R4E-7R4E1 |
| A310-220 | JT9D-7R4E1 | A310-300 | JT9D-7R4E1 | 1PW027_JT9D-7R4E-7R4E1 |
| A310-300 | CF6-80C2A2 | A310-300 | CF6-80C2A2 | 1GE016_CF6-80C2A2 |
| A310-300 | CF6-80C2A8 | A310-300 | CF6-80C2A2 | 1GE021_CF6-80C2A8 |
| A310-320 | JT9D-7R4E1 | A310-300 | JT9D-7R4E1 | 1PW027_JT9D-7R4E-7R4E1 |
| A310-320 | PW4000-4152 | A310-300 | CF6-80C2A2 | 1GE016_CF6-80C2A2 |
| A310-320 | PW4000-4156A | A310-300 | CF6-80C2A2 | 1GE016_CF6-80C2A2 |
| A319-110 | CFM56-5A4 | A319-200 | CFM56-5-A1 | 1CM008_CFM56-5-A1 |
| A319-110 | CFM56-5A5 | A319-200 | CFM56-5-A1 | 1CM008_CFM56-5-A1 |
| A319-110 | CFM56-5B5_P | A319 | CFM56-5B3P-25 | 3CM027_CFM56-5B5/P |
| A319-110 | CFM56-5B6_2P | A319 | CFM56-5B3P-25 | 3CM028_CFM56-5B6/P |
| A319-110 | CFM56-5B6_P | A319 | CFM56-5B3P-25 | 3CM028_CFM56-5B6/P |
| A319-130 | V2500-2522-A5 | A319-200 | V2522-A5 | 3IA006_V2522-A5 |
| A319-130 | V2500-2524-A5 | A319-200 | V2522-A5 | 3IA007_V2524-A5 |
| A320-110 | CFM56-5A1 | A320-200 | CFM56-5-A1 | 1CM008_CFM56-5-A1 |
| A320-210 | CFM56-5A1 | A320-200 | CFM56-5-A1 | 1CM008_CFM56-5-A1 |
| A320-210 | CFM56-5A3 | A320-200 | CFM56-5-A1 | 1CM009_CFM56-5A3 |
| A320-210 | CFM56-5B4 | A320-200 | CFM56-5-A1 | 1CM008_CFM56-5-A1 |
| A320-210 | CFM56-5B4_2 | A320-200 | CFM56-5-A1 | 3CM026_CFM56-5B4/P |
| A320-210 | CFM56-5B4_2P | A320-200 | CFM56-5B3P-26.5 | 3CM026_CFM56-5B4/P |
| A320-210 | CFM56-5B4_P | A320-200 | CFM56-5B3P-26.5 | 3CM026_CFM56-5B4/P |
| A320-230 | V2500-2500-A1 | A320-200 | V2525-A5 | 11A001_V2500-A1 |
| A320-230 | V2500-2527-A5 | A320-200 | V2525-A5 | 1IA003_V2527-A5 |

| Schedule Airplane | Schedule Engine | Performance Airplane | Performance Engine | Emissions Engine |
|-------------------|-----------------|-------------------------|--------------------|-------------------|
| | | | | 0 |
| A321-110 | CFM56-5B1_2 | A321-100 | CFM56-5B1 | 20M012 CEM56-5R1 |
| A321-110 | CFM56-5B2 | A321-100 | CFM56-5B1 | 20M013 CEMERERO |
| A321-130 | V2500-2530-A5 | A321-100 | V2530-A5 | |
| A321-210 | CFM56-5B3_2P | A321-200 | V2533-A5 | 31A008 V2523_A5 |
| A321-210 | CFM56-5B3_P | A321-200 | V2533-A5 | 314008 V2532.A5 |
| A321-230 | V2500-2533-A5 | A321-200 | V2533-A5 | 31ADD8 V2533 A5 |
| A330-200 | CF6-80E1A4 | A330-200 | CF6-80E1A3 | 4GF080 CF6-80F1AA |
| A330-220 | PW4000-4168A | A330-200 | PW4168 | |
| A330-240 | Trent-772B-60 | A330-200 | TRENT72 | 288023 Trant772 |
| A330-300 | CF6-80E1A2 | A330-300 | CF6-80E1A1 | 1GF033 CF6-80F1A2 |
| A330-320 | PW4000-4164 | A330-300 | PW4164 | 1PW049 PW4164 |
| A330-320 | PW4000-4168 | A330-300 | PW4164 | |
| A330-340 | Trent-768-60 | A330-300 | TRENT768 | 2BB022 Trant768 |
| A330-340 | Trent-772-60 | A330-300 | TRENT768 | 2BB022 Trent768 |
| A330-340 | Trent-772B-60 | A330-300 | TRENT768 | 2BB022 Trant768 |
| A340-210 | CFM56-5C2 | A340-200 | CFM56-5C-2 | 1CM010 CEM56-5C2 |
| A340-210 | CFM56-5C2G | A340-200 | CFM56-5C-2 | 1CM010 CEM56-5C2 |
| A340-210 | CFM56-5C3_F | A340-200 | CFM56-5C-2 | 1CM010 CFM56-5C2 |
| A340-310 | CFM56-5C2 | A340-200 | CFM56-5C-2 | 1CM010 CFM56-5C2 |
| A340-310 | CFM56-5C3_F | A340-200 | CFM56-5C-2 | 1CM010_CFM56-5C2 |
| A340-310 | CFM56-5C4 | A340-200 | CFM56-5C-2 | 1CM010 CFM56-5C2 |
| AN4 | LGTURB | LGTURB | PW125B | PW125B |
| ANG | MDTURB | MDTURB | PW120 | PW120 |
| ANF | MDTURB | MDTURB | PW120 | PW120 |
| A14 | LGTURB | LGTURB | PW125B | PW125B |
| AT7 | LGTURB | LGTURB | PW125B | PW125B |
| AIP | LGTURB | LGTURB | PW125B | PW125B |
| AIR | LGTURB | LGTURB | PW125B | PW125B |

| | | Performance | | |
|-------------------|-----------------|-------------|--------------------|--------------------|
| Schedule Airplane | Schedule Engine | Airplane | Performance Engine | Emissions Engine |
| | | | | |
| An-124-*_FRT | D-18-T | 747-400F | CF6-80C2B1F | 1GE024_CF6-80C2B1F |
| BEI | SMTURB | SMTURB | PT6A | PT6A |
| BF9 | SMTURB | SMTURB | PT6A | PT6A |
| BEH | SMTURB | SMTURB | PT6A | PT6A |
| BFS | SMTURB | SMTURB | PT6A | PT6A |
| CD2 | SMTURB | SMTURB | PT6A | PT6A |
| CNC | SMTURB | SMTURB | PT6A | PT6A |
| CRJ-100ER | CF34-3A1 | CRJ | CF34-3A1 | 1GE035_CF34-3A1 |
| CR.J-100LR | CF34-3A1 | CRJ | CF34-3A1 | 1GE035_CF34-3A1 |
| CRJ-200ER | CF34-3B1 | CRJ | CF34-3A1 | 1GE035_CF34-3A1 |
| CRJ-200LR | CF34-3B1 | CRJ | CF34-3A1 | 1GE035_CF34-3A1 |
| CS5 | LGTURB | LGTURB | PW125B | PW125B |
| CV5 | LGTURB | LGTURB | PW125B | PW125B |
| CVF | LGTURB | LGTURB | PW125B | PW125B |
| Concorde-100 | Olympus-593-610 | Concorde | Olympus-593-610 | Olympus-593-610 |
| D28 | SMTURB | SMTURB | PT6A | PT6A |
| 138 | MDTURB | MDTURB | PW120 | PW120 |
| DC-10-10 | CF6-6D | DC10-10 | CF6-6D | 1GE001_CF6-6D |
| DC-10-10 | CF6-6K | DC10-10 | CF6-6D | 1GE001_CF6-6D |
| DC-10-10F FRT | CF6-6D | DC10-10F | CF6-6D | 1GE001_CF6-6D |
| DC-10-15 | CF6-50C2F | DC-10-30 | CF6-50C2 | 1GE007_CF6-50C1-C2 |
| DC-10-30 | CF6-50C | DC-10-30 | CF6-50C2 | 1GE006_CF6-50C |
| DC-10-30 | CF6-50C1 | DC-10-30 | CF6-50C2 | 1GE007_CF6-50C1-C2 |
| DC-10-30 | CF6-50C2 | DC-10-30 | CF6-50C2 | 1GE007_CF6-50C1-C2 |
| DC-10-30 | CF6-50C2R | DC-10-30 | CF6-50C2 | 1GE007_CF6-50C1-C2 |
| DC-10-30CF | CF6-50C2 | DC-10-30 | CF6-50C2 | 1GE007_CF6-50C1-C2 |
| DC-10-30F FRT | CF6-50C2 | DC-10-30F | CF6-50C2 | 1GE007_CF6-50C1-C2 |
| DC-10-30F_FRT | CF6-50C2B | DC-10-30F | CF6-50C2 | 1GE007_CF6-50C1-C2 |

| | | Performance | | |
|-------------------|-----------------|--------------|--------------------|----------------------|
| Schedule Airplane | Schedule Engine | Airplane | Performance Engine | Emissions Engine |
| DC-10-40 | JT9D-20 | DC10-40 | IT9D-20 | |
| DC-10-401 | JT9D-59A | DC10-40 | 119D-20 | |
| DC-8-54CF_FRT | JT3D-3B | DC-8-63-63CF | JT3D-7 | |
| DC-8-61C_FRT | JT3D-3B | DC8-55-55CF | JT3D-3B | |
| DC-8-62CF_FRT | JT3D-3B | DC8-55-55CF | JT3D-3B | |
| DC-8-62F_FRT | JT3D-3B | DC-8-63-63CF | JT3D-7 | 1PW002 .1730.7ceries |
| DC-8-63CF_FRT | JT3D-7 | DC-8-63-63CF | JT3D-7 | 1PW002 |
| DC-8-63C_FRT | JT3D-7 | DC-8-63-63CF | JT3D-7 | |
| DC-8-63_FRT | JT3D-7 | DC-8-63-63CF | JT3D-7 | 1PW002_102-135165 |
| DC-8-71F_FRT | CFM56-2C1 | DC-8-71-71CF | CFM56-1B | 10M03 CEMER-2.05 |
| DC-8-73CF_FRT | CFM56-2C1 | DC-8-71-71CF | CFM56-1B | |
| DC-8-73F_FRT | CFM56-2C1 | DC-8-71-71CF | CFM56-1B | |
| DC-9-15 | JT8D-7 | DC9-30 | JTBD-7 | |
| DC-9-15 | JT8D-7A | DC9-30 | JTBD-7 | |
| DC-9-15RC | JT8D-7B | DC9-30 | .ITRD-7 | |
| DC-9-15RC_FRT | JT8D-7B | DC9-30 | JTBD-7 | |
| DC-9-21 | JT8D-11 | DC9-31 | JT8D-15 | |
| DC-9-31 | JT8D-7A | DC9-30 | UTRD-7 | |
| DC-9-31 | JT8D-7B | DC9-30 | .IT8D-7 | |
| DC-9-31 | JT8D-9A | DC9-30 | JT8D-7 | |
| DC-9-31CF | JT8D-17 | DC9-31 | .ITRD-15 | |
| DC-9-32 | JT8D-11 | DC9-31 | UT8D-15 | |
| DC-9-32 | JT8D-15 | DC9-31 | .ITRD-15 | |
| DC-9-32 | JT8D-17 | DC9-31 | UT8D-15 | |
| DC-9-32 | JT8D-7 | DC9-30 | ITRD-7 | |
| DC-9-32 | JT8D-7A | DC9-30 | JT8D-7 | |
| DC-9-32 | JT8D-7B | DC9-30 | JT8D-7 | 1PW004_UT8D-7series |
| DC-9-32 | JT8D-9 | DC9-30 | JT8D-7 | |

| | | Performance | | |
|-------------------|-----------------|-------------|--------------------|---------------------|
| Schedule Airplane | Schedule Engine | Airplane | Performance Engine | Emissions Engine |
| DC-9-32 | Ag-08L | DC9-30 | JT8D-7 | 1PW006_JT8D-9series |
| DC-9-33CF | JT8D-9A | DC9-30 | JT8D-7 | 1PW006_JT8D-9series |
| DC-9-41 | JT8D-11 | DC9-50 | JT8D-15 | 1PW008_JT8D-11 |
| DC-9-41 | JT8D-15 | DC9-50 | JT8D-15 | 1PW009_JT8D-15 |
| DC-9-41 FRT | JT8D-11 | DC9-50 | JT8D-15 | 1PW008_JT8D-11 |
| I _ | JT8D-17 | DC9-50 | JT8D-15 | 1PW012_JT8D-17 |
| DC-9-51 | JT8D-17A | DC9-50 | JT8D-15 | 1PW014_JT8D-17A |
| DFL | Blank-Blank | CRJ | CF34-3A1 | 1GE034_CF34-3A |
| DH1 | MDTURB | MDTURB | PW120 | PW120 |
| DH3 | MDTURB | MDTURB | PW120 | PW120 |
| DH7 | LGTURB | LGTURB | PW125B | PW125B |
| DH8 | MDTURB | MDTURB | PW120 | PW120 |
| DHT | SMTURB | SMTURB | PT6A | PT6A |
| EM2 | SMTURB | SMTURB | PT6A | PT6A |
| EM3 | Blank-Blank | CRJ | CF34-3A1 | 1GE035_CF34-3A1 |
| EMB | SMTURB | SMTURB | PT6A | PT6A |
| I.M.I | Blank-Blank | CRJ | CF34-3A1 | 1GE035_CF34-3A1 |
| EB3 | Blank-Blank | CRJ | CF34-3A1 | 1GE035_CF34-3A1 |
| ER4 | Blank-Blank | CRJ | CF34-3A1 | 1GE035_CF34-3A1 |
| ERJ | Blank-Blank | CRJ | CF34-3A1 | 1GE035_CF34-3A1 |
| ERJ-145-EP | AE-A | CRJ | CF34-3A1 | 1GE035_CF34-3A1 |
| EB.J-145-EP | AE-A1 1 | CRJ | CF34-3A1 | 1GE035_CF34-3A1 |
| FR.I-145-FR | AE-A | CRJ | CF34-3A1 | 1GE035_CF34-3A1 |
| EB.I-145-FU | AE-A | CRJ | CF34-3A1 | 1GE035_CF34-3A1 |
| FR.I-145-LB | AE-A1 | CRJ | CF34-3A1 | 1GE035_CF34-3A1 |
| ERJ-145-LU | AE-A1 | CRJ | CF34-3A1 | 1GE035_CF34-3A1 |
| FB.I-145-MP | AE-A1 | CRJ | CF34-3A1 | 1GE035_CF34-3A1 |
| F.28-1000 | Spey-555-15 | F-28-4000 | MK555-15H | 1RR017_SPEYMk555 |

| | | Performance | | |
|-------------------|-----------------|---------------|--------------------|-------------------------|
| Schedule Airplane | Schedule Engine | Airplane | Performance Engine | Emissions Engine |
| E 28-2000 | • | | | |
| | | F-28-4000 | MK555-15H | 1RR017_SPEYMk555 |
| F.28-3000 | | F-28-4000 | MK555-15H | 1RR017 SPEYMk555 |
| F.28-4000 | Spey-555-15H | F-28-4000 | MK555-15H | 1RR017 SPEYMk555 |
| F.28-4000 | Spey-555-15P | F-28-4000 | MK555-15H | 1BB017 SPEYMk555 |
| F27 | LGTURB | LGTURB | PW125B | PW125B |
| F50 | LGTURB | LGTURB | PW125B | PW125B |
| FRJ | Blank-Blank | CRJ | CF34-3A1 | 1GE035 CF34-3A1 |
| HS7 | LGTURB | LGTURB | PW125B | PW125B |
| ILB | LGTURB | LGTURB | PW125B | PW125B |
| II-62-* | NK-8-4 | DC-8-63-63CF | JT3D-7 | 1PW004 JT8D-7series |
| II-62-M | D-30-KU | DC-8-63-63CF | JT3D-7 | 1PW004 .IT8D-7series |
| II-76-M_FRT | D-30-KP-2 | DC-8-63-63CF | JT3D-7 | 1PW004 .IT8D-7series |
| II-76-T_FRT | D-30-KP-2 | DC-8-63-63CF | JT3D-7 | 1PW004 .JT8D-7series |
| II-86-* | NK-86 | L-1011-1-100 | RB211-22B | 1RR002 RB211-22R |
| 1-86-* | NK-86-Blank | L-1011-1-100 | RB211-22B | 1RR002 RB211-22B |
| II-96-300 | PS-90-A | L-1011-1-100 | RB211-22B | 1RR003 RB211-22B |
| J31 | SMTURB | SMTURB | PT6A | PT6A |
| J41 | MDTURB | MDTURB | PW120 | PW120 |
| L-1011-1 | RB211-22B | L-1011-1-100 | RB211-22B | 1RR003 RB211-22B |
| L-1011-150 | RB211-22B | L-1011-1-100 | RB211-22B | 1RR003 RB211-22B |
| L-1011-200_FRT | RB211-524B | L-1011-1-100F | RB211-22B | 1RR003 RB211-22B |
| L-1011-200_FRT | RB211-524B4 | L-1011-1-100F | RB211-22B | 1RR003 RB211-22B |
| L-1011-50 | RB211-22B | L-1011-1-100 | RB211-22B | 1RR003 RB211-22B |
| L-1011-500 | RB211-524B4 | L1011-500AC | RB211-524B4 | 1RR004 RB211-524Bseries |
| L11 | Blank-Blank | L-1011-1-100 | RB211-22B | 1RR003 RR211-22R |
| L4T | SMTURB | SMTURB | PT6A | PT6A |
| LOE | LGTURB | LGTURB | PW125B | PW125B |
| LOF | LGTURB | LGTURB | PW125B | PW125B |

| | | Derformance | | |
|---------------------|-----------------|-------------|--------------------|-----------------------|
| Schedule Airplane | Schedule Engine | Airplane | Performance Engine | Emissions Engine |
| | Ē | | | DIMITOR |
| LOH | LGI UHB | LGIUND | | |
| LOM | LGTURB | LGTURB | PW125B | PW125B |
| B | Blank-Blank | CRJ | CF34-3A1 | 1GE034_CF34-3A |
| MD-11-CF OC | PW4000-4460 | MD-11ER | PW4460 | 1PW052_PW4460 |
| MD-11-CF OC | PW4000-4462 | MD-11ER | PW4460 | 1PW052_PW4460 |
| MD-11-Combi CMB | CF6-80C2D1F | MD-11 | CF6-80C2D1F | 2GE049_CF6-80C2D1F |
| MD-11-Freighter FRT | CF6-80C2D1F | MD-11F | CF6-80C2D1F | 2GE049_CF6-80C2D1F |
| MD-11-Freighter FRT | PW4000-4460 | MD-11F | PW4460 | 1PW057_PW4x60 |
| MD-11-Passenger | CF6-80C2D1F | MD-11 | CF6-80C2D1F | 2GE049_CF6-80C2D1F |
| MD-11-Passenger | PW4000-4460 | MD-11ER | PW4460 | 1PW052_PW4460 |
| MD-11-Passenger | PW4000-4462 | MD-11ER | PW4460 | 1PW058_PW4x62 |
| MD-80-81 | JT8D-217 | MD-82 | JT8D-217A | 1PW018_JT8D-217series |
| MD-80-81 | JT8D-217C | MD-82 | JT8D-217A | 1PW018_JT8D-217series |
| MD-80-82 | JT8D-217 | MD-82 | JT8D-217A | 1PW018_JT8D-217series |
| MD-80-82 | JT8D-217A | MD-82 | JT8D-217A | 1PW018_JT8D-217series |
| MD-80-82 | JT8D-217C | MD-82 | JT8D-217A | 1PW018_JT8D-217series |
| MD-80-82 | JT8D-219 | MD-83 | JT8D-219 | 1PW019_JT8D-219 |
| MD-80-83 | JT8D-217C | MD-83 | JT8D-219 | 1PW018_JT8D-217series |
| MD-80-83 | JT8D-219 | MD-83 | JT8D-219 | 1PW019_JT8D-219 |
| MD-80-87 | JT8D-217C | MD-87 | JT8D-217C | 1PW018_JT8D-217series |
| MD-80-87 | JT8D-219 | MD-87 | JT8D-217C | 1PW019_JT8D-219 |
| MD-80-88 | JT8D-219 | MD-83 | JT8D-219 | 1PW019_JT8D-219 |
| MD-90-30 | V2500-2525-D5 | MD90-30 | V2525-D5 | 11A002_V2525-D5 |
| MD-90-30 | V2500-2528-D5 | MD90-30 | V2525-D5 | 11A002_V2525-D5 |
| MU2 | SMTURB | SMTURB | PT6A | PT6A |
| ND2 | MDTURB | MDTURB | PW120 | PW120 |
| One-Eleven-200 | Spey-506-14A | BAC111-500 | MK512-14 | 1RR016_SPEYMk511 |
| One-Eleven-500 | Spey-512-14DW | BAC111-500 | MK512-14 | 1RR015_SPEYMk511 |

| Schedule Airplane | Schedule Engine | Performance Airplane | Performance Engine | Emissions Engine |
|-------------------|-----------------|-------------------------|--------------------|------------------------|
| One-Eleven-560 | Spey-512-14DW | BAC111-500 | MK512-14 | 1BB015 SPEVMk511 |
| PL2 | SMTURB | SMTURB | PT6A | PT6A |
| PLG | SMTURB | SMTURB | PT6A | PT6A |
| RJ-RJ100 | LF507-1F | RJ-100 | LF507 | 171 004 1 F507-1E-1H |
| RJ-RJ70 | LF507-1F | RJ-85 | LF507 | 11 004 I F507-1F-1H |
| RJ-RJ85 | LF507-1F | RJ-85 | LF507 | 1TI 004 I F507.1F.1H |
| S20 | LGTURB | LGTURB | PW125B | |
| SF3 | MDTURB | MDTURB | PW120 | PW120 |
| SH3 | MDTURB | MDTURB | PW120 | PW120 |
| SH6 | MDTURB | MDTURB | PW120 | PW120 |
| SHS | SMTURB | SMTURB | PT6A | PT6A |
| SWM | SMTURB | SMTURB | PT6A | PT6A |
| T20 | Blank-Blank | 757-200 | RB211-535F4 | 3RR028 RR011_535E1 |
| Tu-134-A | D-30-2 | DC9-30 | JT8D-7 | |
| Tu-134-A | D-30-3 | DC9-30 | JT8D-7 | 1 PW004_01 00-1 361165 |
| Tu-134-B | D-30-3 | DC9-30 | JT8D-7 | 1PW004 JT80-7ceriec |
| Tu-154-B | NK-8-2U | 727-200 | JT8D-15-15A | |
| Tu-154-M | D-30-KU-154-II | 727-200 | JT8D-15-15A | |
| Tu-204-100C_FRT | PS-90-AT | 757-200 | RB211-535C | 188010 88011.6350 |
| YN2 | SMTURB | SMTURB | PT6A | |
| YN7 | LGTURB | LGTURB | PW125B | PW125B |
| YS1 | LGTURB | LGTURB | PW125B | PW125B |
| | | | | |

| | | Performance | | |
|-------------------|-----------------|-------------|--------------------|---------------------|
| Schedule Airplane | Schedule Engine | Airplane | Performance Engine | Emissions Engine |
| Yak-40-* | AI-25 | 727-100 | JT8D-7 | 1PW002_JT3D-7series |
| Yak-40-* | AI-25-Blank | 727-100 | JT8D-7 | 1PW002_JT3D-7series |
| Yak-42-* | D-36 | 727-100 | JT8D-7 | 1PW002_JT3D-7series |
| Yak-42-* | D-36-Blank | 727-100 | JT8D-7 | 1PW002_JT3D-7series |
| Yak-42-D | D-36 | 727-100 | JT8D-7 | 1PW002_JT3D-7series |
| Yak-42-D | D-36-Blank | 727-100 | JT8D-7 | 1PW002_JT3D-7series |

Notes: SMTURB = Small Turboprop MDTURB = Medium Turboprop LGTURB = Large Turboprop

Table C-1. Fuel burned, emissions, cumulative fractions of emissions, and effective emission indices as a function of altitude (Summed over Latitude and Longitude) for scheduled air traffic in January 1999.

| Altitude Band | Fuel | cum fuel | NOX | cum NOx | Ĥ | cum HC | 00 | cum CO | cum CO El(NOx) | EI(HC) | EI(CO) |
|-----------------|-----------|--------------------|----------|--------------------|-------------|----------------|----------|----------------|----------------|--------|--------|
| (km) | (kg/day) | (%) | (kg/day) | (%) | (kg/day) | (%) | (kg/day) | (%) | | | |
| · | 2 26E 107 | 0 B0% | | %CU 6 | 1.83E+05 | 34.52% | 6.15E+05 | 32.93% | 12.09 | 5.46 | 18.35 |
| - | 0.000-106 | 0.00 Ct | 1 476+05 | 10 20% | 2 96F+04 | 40 10% | 1.04E+05 | 38.50% | 16.11 | 3.24 | 11.40 |
| N 0 - | 9.13E+U0 | 14.00% | | 15.51% | 2 43F+04 | 44.69% | 8.75E+04 | 43.19% | 16.93 | 2.85 | 10.25 |
| י מ י | 0.9351+00 | 17 06% | 1.70F105 | 10.40% | 2.30F+04 | 49 03% | 7.98E+04 | 47.47% | 18.14 | 2.33 | 8.09 |
| , , 4 n | 9.0000000 | 00 E 0% | 1 53F+05 | 22 BG% | 2.38F+04 | 53.52% | 7.98E+04 | 51.74% | 16.83 | 2.62 | 8.79 |
| 4 1 ' | 9.0/E+00 | 20.36./0 | 1 445+05 | 26.09% | 2 40F+04 | 58.05% | 7.96E+04 | 56.01% | 16.06 | 2.69 | 8.91 |
| י ס י ס | 0.345700 | 20.14 /0 DE 74% | 1 415+05 | 20.03% | 2 33F+04 | 62.45% | 7.41E+04 | 59.98% | 15.90 | 2.62 | 8.33 |
| ~ 0 ' 0 r | 0.905+00 | 28 55% | 1 44E+05 | 32.45% | 2.42E+04 | 67.01% | 8.06E+04 | 64.29% | 15.04 | 2.52 | 8.39 |
| • | 9.00CT00 | 31 24% | 1.31E+05 | 35.37% | 2.24E+04 | 71.23% | 7.53E+04 | 68.33% | 14.35 | 2.44 | 8.23 |
| - - | 3.10E+03 | 36 82% | 2 65E+05 | 41.28% | 2.51E+04 | 75.96% | 8.31E+04 | 72.78% | 13.91 | 1.31 | 4.36 |
| | 1 DELLOR | 67 74% | 1 25F+06 | 69.00% | 7.33E+04 | 89.79% | 3.18E+05 | 89.82% | 11.79 | 0.69 | 3.01 |
| | | 00 61% | 1 37F+06 | 00 57% | 5 33F+04 | 99.84% | 1.86E+05 | <u>99.79</u> % | 12.61 | 0.49 | 1.71 |
| | | 0/ 10.66 | | 00.81% | E ROFIO | 00 05% | 2 11F+03 | %06.66 | 13.94 | 0.73 | 2.64 |
| 12 - 13 | 8.U1E+U3 | 99.04 % | | 0/ 10.66 /00 00 | 0.05E10E | 00.00% | 9 11E+02 | 99 95% | 13.46 | 0.80 | 3.39 |
| 13 - 14 | 2.69E+05 | 99.92% | 3.02E+U3 | 99.09% 00.000% | 2.100-100 | 0/ 00 00 | 0.11L.02 | 00.00 | | 0.20 | 3.50 |
| 14 - 15 | 1.07E+04 | 99.93% | 1.92E+02 | 99.90% | 2.10E+00 | 88.88% | 0./4E+01 | 99.93./0 | | 0.50 | 2 20 |
| 15 - 16 | 1.07E+04 | 99.93% | 1.92E+02 | 60.90% | 2.10E+00 | 99.99% | 3./4E+U1 | %C6.66 | 18.00 | 0.20 | |
| 16 - 17 | 8 94F+04 | <u> 86.96%</u> | 1.61E+03 | 99.94% | 1.79E+01 | 66.66 % | 3.13E+02 | 99.97% | 18.00 | 0.20 | 00°.5 |
| | 1 19F+05 | %66.66 | 2.14E+03 | %66.66 | 2.38E+01 | 100.00% | 4.16E+02 | 66. 66% | 18.00 | 0.20 | 3.50 |
| 18 - 19 | 3.42E+04 | 100.00% | 6.16E+02 | 100.00% | 6.80E+00 | 100.00% | 1.20E+02 | 100.00% | 18.00 | 0.20 | 3.50 |
| | | | 105.00 | | 5 30E 105 | | 1 87E+06 | | 13.15 | 1.55 | 5.46 |
| Global Total | 3.42E+U8 | | 4.445+00 | | 0.001-100.0 | | | | | | |

| | UH | | | | | |
|--|---------------|---------------------------|----------------|---------|--------|--------------|
| 1 3.35E+07 9.85% 4.06E+05 9.06% 2 9.16E+06 12.54% 1.48E+05 12.36% 2 9.16E+06 12.54% 1.48E+05 12.36% 2 9.16E+06 12.54% 1.48E+05 12.36% 2 9.87E+06 17.95% 1.45E+05 19.61% 2 9.12E+06 20.63% 1.45E+05 23.03% 2 9.12E+06 20.63% 1.45E+05 23.03% 2 9.12E+06 20.63% 1.43E+05 29.41% 3 9.50E+06 31.42% 1.43E+05 26.23% 3 9.50E+06 31.42% 1.33E+05 29.41% 3 9.50E+06 31.42% 1.33E+05 35.62% 10 1.92E+07 37.07% 2.68E+05 31.56% 11 1.04E+08 67.62% 1.23E+05 99.85% 69.00% 13 8.64E+05 99.85% 1.21E+04 99.85% 69.00% 11 1.04E+05 99.85% 1.21E+04 99.85% 69.09% 13 8.64E+05< | (Å | cum HC CO (%) (kg/day) | cum CO (%) | EI(NOX) | EI(HC) | EI(CO) |
| - 2 9.16E+06 12.54% 1.48E+05 12.36% - 3 8.54E+06 15.05% 1.45E+05 15.60% - 4 9.87E+06 17.95% 1.45E+05 12.36% - 5 9.12E+06 20.63% 1.54E+05 23.03% - 6 8.88E+06 20.63% 1.54E+05 23.03% - 7 8.97E+06 23.24% 1.43E+05 26.23% - 9 9.060 1.43E+05 32.64% 35.62% - 10 1.92E+07 37.07% 2.68E+05 41.59% - 10 1.92E+07 37.07% 2.68E+05 41.59% - 10 1.92E+07 37.07% 2.68E+05 41.59% - 11 1.04E+08 67.62% 1.23E+06 69.09% | 1 825-05 24 | 04 70% 6 4 ET . OF | | | | |
| - 3 8.54E+06 15.05% 1.45E+05 15.60% - 4 9.87E+06 17.95% 1.79E+05 19.61% - 5 9.12E+06 20.63% 1.54E+05 23.03% - 6 8.88E+06 23.24% 1.43E+05 23.03% - 7 8.97E+06 23.24% 1.43E+05 23.03% - 7 8.97E+06 23.24% 1.43E+05 23.64% - 7 8.97E+06 23.24% 1.43E+05 23.64% - 9 9.60E+06 28.69% 1.43E+05 32.64% - 9 9.30E+06 23.142% 1.33E+05 32.64% - 10 1.92E+07 37.07% 2.68E+05 31.42% 1.33E+06 69.00% - 11 1.04E+08 67.62% 1.23E+05 39.62% 1.21E+04 99.85% 1.24E+05 <t< td=""><td>_</td><td></td><td>33.03%</td><td>12.11</td><td>5.44</td><td>18.35</td></t<> | _ | | 33.03% | 12.11 | 5.44 | 18.35 |
| - 4 9.87E+06 17.95% 1.79E+05 19.61% - 5 9.12E+06 20.63% 1.54E+05 23.03% - 6 8.88E+06 23.24% 1.43E+05 23.03% - 7 8.97E+06 17.95% 1.79E+05 23.03% - 7 8.97E+06 23.24% 1.43E+05 23.03% - 7 8.97E+06 23.24% 1.43E+05 23.64% - 9 9.60E+06 28.69% 1.43E+05 32.64% - 9 9.30E+06 21.42% 1.33E+05 35.62% - 10 1.92E+07 37.07% 2.68E+05 31.42% - 11 1.04E+08 67.62% 1.23E+06 69.00% - 12 1.02E+07 37.07% 2.68E+06 99.55% - 13 8.64E+05 99.85% 1.21E+04 99.82% - 13 8.64E+05 99.95% 1.21E+04 99.99% - 16 1.24E+06 99.95% 1.21E+04 99.99% <td></td> <td></td> <td>38.61%</td> <td>16.14</td> <td>3.21</td> <td>11.34</td> | | | 38.61% | 16.14 | 3.21 | 11.34 |
| - 0.0012400 1.000 19.61% - 5 9.12E+06 20.63% 1.54E+05 23.03% - 7 8.97E+06 23.24% 1.43E+05 23.03% - 7 8.97E+06 23.24% 1.43E+05 26.23% - 7 8.97E+06 23.24% 1.43E+05 26.23% - 9 9.60E+06 28.69% 1.45E+05 32.64% - 9 9.30E+06 21.42% 1.33E+05 35.62% - 10 1.92E+07 37.07% 2.68E+05 35.62% - 11 1.04E+08 67.62% 1.23E+05 35.62% - 11 1.04E+08 67.62% 1.23E+06 99.56% - 12 1.02E+07 37.07% 2.68E+06 99.55% - 12 1.04E+06 99.95% 1.21E+04 99.82% - 13 8.64E+05 99.95% 1.21E+04 99.99% - 16 1.24E+04 99.92% 2.24E+02 99.99% - 16 | | | 43.29% | 17.02 | 2.81 | 10.19 |
| 6 8.88E+06 23.24% 1.34E+05 23.03% 7 8.97E+06 25.87% 1.43E+05 29.41% 9 9.60E+06 28.69% 1.45E+05 32.64% 9 9.567% 1.45E+05 32.64% 9 9.30E+06 31.42% 1.33E+05 35.62% 10 1.92E+07 37.07% 2.68E+05 41.59% 11 1.04E+08 67.62% 1.23E+06 99.55% 12 1.09E+08 99.60% 1.37E+06 99.55% 13 8.64E+05 99.85% 1.21E+04 99.89% 14 2.18E+05 99.92% 2.96E+03 99.89% 15 1.24E+04 99.92% 2.96E+03 99.89% 16 1.24E+04 99.93% 2.24E+02 99.90% 17 9.40E+04 99.95% 1.69E+03 99.99% 18 1.24E+05 99.95% 1.69E+03 99.99% 19 3.58E+04 100.00% 6.44E+02 99.99% | | | 47.56% | 18.18 | 2.30 | 8.05 |
| 0 0.000E+00 23.24% 1.43E+05 26.23% - 7 8.97E+06 25.87% 1.43E+05 29.41% - 9 9.60E+06 28.69% 1.45E+05 32.64% - 9 9.60E+06 28.69% 1.45E+05 32.64% - 9 9.30E+06 28.69% 1.45E+05 32.64% - 10 1.92E+07 37.07% 2.68E+05 41.59% - 10 1.92E+07 37.07% 2.68E+05 41.59% - 11 1.04E+08 67.62% 1.23E+06 69.00% - 12 1.09E+08 99.60% 1.37E+06 99.82% - 13 8.64E+05 99.85% 1.21E+04 99.82% - 14 2.18E+05 99.92% 2.96E+03 99.89% - 15 1.24E+04 99.92% 2.24E+02 99.99% - 16 1.24E+04 99.93% 2.24E+02 99.99% - 16 1.24E+05 99.99% 2.24E+03 99.999% | | 53.82% 7.97E+04 | 51.84% | 16.85 | 2.58 | 8.74 |
| 0.97/E+00 25.87% 1.43E+05 29.60E+06 28.69% 1.45E+05 32.64% 9.30E+06 31.42% 1.33E+05 32.64% 9.30E+06 31.42% 1.33E+05 32.64% 9.30E+06 1.32E+05 37.07% 2.68E+05 37.07% 2.68E+05 37.07% 2.68E+05 37.07% 2.68E+05 37.07% 2.68E+05 99.56% 1.21E+04 99.99% 2.24E+02 99.99% 1.24E+04 99.92% 2.24E+02 99.99% 1.24E+04 99.93% 2.24E+02 99.99% 1.24E+04 99.95% 1.69E+03 99.99% 1.69E+03 1.24E+04 99.99% 2.24E+02 99.99% 1.0000% 6.44E+03 99.99% | _ | 58.35% 7.94E+04 | 56.10% | 16.13 | 2.67 | 8.94 |
| 9 9.300E+00 28.69% 1.45E+05 32.64% 9 9.30E+06 31.42% 1.33E+05 35.62% 10 1.92E+07 37.07% 2.68E+05 41.59% 11 1.04E+08 67.62% 1.23E+06 69.00% 12 1.09E+08 99.60% 1.37E+06 99.55% 13 8.64E+05 99.85% 1.21E+04 99.82% 13 8.64E+05 99.92% 2.96E+03 99.89% 15 1.24E+04 99.92% 2.24E+02 99.99% 16 1.24E+04 99.93% 2.24E+02 99.99% 17 9.40E+04 99.95% 1.69E+03 99.99% 18 1.24E+04 99.95% 1.69E+03 99.99% 19 3.58E+04 100.00% 6.44E+02 99.99% | | 62.74% 7.43E+04 | 60.10% | 15.90 | 2.57 | 8.29 |
| 9 9.30E+06 31.42% 1.33E+05 35.62% 10 1.92E+07 37.07% 2.68E+05 41.59% 11 1.04E+08 67.62% 1.23E+06 69.00% 12 1.09E+08 99.60% 1.37E+06 99.55% 12 1.09E+08 99.60% 1.37E+06 99.89% 13 8.64E+05 99.92% 2.96E+03 99.89% 14 2.18E+05 99.92% 2.96E+03 99.89% 15 1.24E+04 99.92% 2.24E+02 99.99% 16 1.24E+04 99.93% 2.24E+02 99.99% 17 9.40E+04 99.95% 1.69E+03 99.94% 18 1.24E+05 99.99% 2.24E+03 99.99% 19 3.58E+04 100.00% 6.44E+002 40.90% | | 67.30% 8.05E+04 | 64.42% | 15.08 | 2.49 | 8 39 |
| 10 1.9ZE+0/ 37.07% 2.68E+05 41.59% 11 1.04E+08 67.62% 1.23E+06 69.00% 12 1.09E+08 99.60% 1.37E+06 99.55% 13 8.64E+05 99.85% 1.21E+04 99.82% 14 2.18E+05 99.92% 2.96E+03 99.89% 15 1.24E+04 99.92% 2.24E+02 99.99% 16 1.24E+04 99.93% 2.24E+02 99.90% 17 9.40E+04 99.93% 2.24E+03 99.94% 18 1.24E+05 99.99% 2.24E+03 99.99% 19 3.58E+04 100.00% 6.44E+00 400.00% | | 71.51% 7.55E+04 | 68.48% | 14.34 | 237 | 8 12 |
| 11 1.04E+08 67.62% 1.23E+06 69.00% 12 1.09E+08 99.60% 1.37E+06 99.55% 13 8.64E+05 99.85% 1.21E+04 99.82% 14 2.18E+05 99.92% 2.96E+03 99.89% 15 1.24E+04 99.92% 2.24E+02 99.99% 16 1.24E+04 99.93% 2.24E+02 99.90% 17 9.40E+04 99.95% 1.69E+03 99.99% 18 1.24E+05 99.99% 2.24E+03 99.99% 19 3.58E+04 100.00% 6.44E+00 400.00% | 2.46E+04 76. | 76.20% 8.31E+04 | 72.94% | 13.92 | 1.28 | 4.32 |
| - 12 1.09E+08 99.60% 1.37E+06 99.55% - 13 8.64E+05 99.85% 1.21E+04 99.82% - 14 2.18E+05 99.92% 2.96E+03 99.89% - 15 1.24E+04 99.92% 2.24E+02 99.89% - 16 1.24E+04 99.93% 2.24E+02 99.90% - 17 9.40E+04 99.95% 1.69E+03 99.94% - 18 1.24E+05 99.99% 2.24E+03 99.99% - 19 3.58E+04 100.00% 6.44E+00 400.00% | 7.17E+04 89. | 89.88% 3.12E+05 | 89.73% | 11.81 | 0.69 | 3.01 |
| 13 8.64E+05 99.85% 1.21E+04 99.82% 14 2.18E+05 99.92% 2.96E+03 99.89% 15 1.24E+04 99.92% 2.24E+02 99.99% 16 1.24E+04 99.93% 2.24E+02 99.90% 17 9.40E+04 99.95% 1.69E+03 99.94% 18 1.24E+05 99.99% 2.24E+03 99.99% 19 3.58E+04 100.00% 6.44E+00 400.00% | 5.21E+04 99. | 99.83% 1.87E+05 | 99.78% | 12.57 | 0.48 | 1 7 0 |
| - 14 2.18E+05 99.92% 2.96E+03 99.89% - 15 1.24E+04 99.92% 2.24E+02 99.89% - 16 1.24E+04 99.93% 2.24E+02 99.90% - 17 9.40E+04 99.95% 1.69E+03 99.94% - 18 1.24E+05 99.99% 2.24E+03 99.99% - 19 3.58E+04 100.00% 6.44E+00 400.00% | 6.10E+02 99. | 99.95% 2.29E+03 | %06 66 | 13 08 | 140 | 1 I I I I |
| - 15 1.24E+04 99.92% 2.24E+02 99.89% - 16 1.24E+04 99.93% 2.24E+02 99.90% - 17 9.40E+04 99.95% 1.69E+03 99.94% - 18 1.24E+05 99.99% 2.24E+03 99.99% - 19 3.58E+04 100.00% 6.44E+00 100.00% | 2.03E+02 99. | | 00 02% | 12 55 | | |
| - 16 1.24E+04 99.93% 2.24E+02 99.90% - 17 9.40E+04 99.95% 1.69E+03 99.94% - 18 1.24E+05 99.99% 2.24E+03 99.99% - 19 3.58E+04 100.00% 6.44E+02 100.00% | | | 00 05% | | 0.90 | 4.15 7.15 |
| - 17 9.40E+04 99.95% 1.69E+03 99.94% 1 - 18 1.24E+05 99.99% 2.24E+03 99.99% 2 - 19 3.58E+04 100.00% 6.44E+02 100.00% 7 | | | 00.050 /0 | | 0.20 | 00.5 |
| 1.24E+05 99.99% 2.24E+03 99.99% 3.58E+04 100.00% 6.44E±03 100.00% | | | 99.90% | 18.00 | 0.20 | 3.50 |
| 3.58E+04 100 00% 6.44E±03 39.39% | | | 99.97% | 18.00 | 0.20 | 3.50 |
| | | 4 | 66.66 % | 18.00 | 0.20 | 3.50 |
| | /.20E+00 100. | 100.00% 1.25E+02 | 100.00% | 18.00 | 0.20 | 3.50 |
| GiobaiTotal 3.40E+08 4.48E+06 5.24E+05 | | | | | | |

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Table C-3. Fuel burned, emissions, cumulative fractions of emissions, and effective emission indices as a function of altitude (Summed over Latitude and Longitude) for scheduled air traffic in March 1999.

| Altitude Band | nd Fuel (kn/dav) | | cum fuel (%) | NOx (ka/dav) | cum NOx (%) | HC (kq/day) | cum HC (%) | CO (kg/day) | cum CO (%) | EI(NOx) | EI(HC) | EI(CO) |
|-----------------|---------------------------------|------|------------------|-----------------|----------------|----------------|---------------------|----------------|----------------|---------|--------|--------|
| | 22/201 | | | | | , , , | | | | | | |
| , , , | 3 38F+07 | _ | 9.84% | 4.09E+05 | 9.06% | 1.82E+05 | 34.95% | 6.18E+05 | 33.18% | 12.12 | 5.39 | 18.32 |
| · · · | 0 3F+06 | , | 12.53% | 1.49E+05 | 12.36% | 2.93E+04 | 40.58% | 1.05E+05 | 38.79% | 16.14 | 3.17 | 11.33 |
| - C | - <u>3.202100</u> 3 8.61F+06 | • | 15 04% | 1.47E+05 | 15.60% | 2.38E+04 | 45.15% | 8.76E+04 | 43.49% | 17.03 | 2.77 | 10.18 |
| 1 0 | | • | 17 94% | 1.81E+05 | 19.61% | 2.25E+04 | 49.47% | 8.00E+04 | 47.78% | 18.19 | 2.26 | 8.05 |
| , , , , | 0.00E+06 | • | 20.62% | 1 55F+05 | 23.04% | 2.33E+04 | 53.96% | 8.03E+04 | 52.09% | 16.86 | 2.54 | 8.73 |
| , , , , | | | 23.23% | 1.44E+05 | 26.24% | 2.35E+04 | 58.47% | 7.98E+04 | 56.37% | 16.14 | 2.63 | 8.93 |
| יי י | | | 25.87% | 1 44E+05 | 29.42% | 2.29E+04 | 62.88% | 7.48E+04 | 60.38% | 15.90 | 2.54 | 8.27 |
| | | | 28.68% | 1.46E+05 | 32.65% | 2.39E+04 | 67.47% | 8.11E+04 | 64.73% | 15.09 | 2.47 | 8.39 |
| - a | | | 31 40% | 1 34F+05 | 35.61% | 2.20E+04 | 71.70% | 7.58E+04 | 68.80% | 14.36 | 2.37 | 8.15 |
| • | c | | 37.07% | 2 71F+05 | 41.61% | 2.45E+04 | 76.41% | 8.37E+04 | 73.29% | 13.92 | 1.26 | 4.30 |
| , , , , | 11 1 05F±08 | | 67.62% | 1.24E+06 | 69.05% | 7.12E+04 | 90.08% | 3.12E+05 | 90.03% | 11.83 | 0.68 | 2.98 |
| 2 7 | 10 1 10E 108 | | 00 65% | 1 38F+06 | 99.61% | 5.08E+04 | 99.84% | 1.82E+05 | 99.80 % | 12.56 | 0.46 | 1.66 |
| - ç | 12 1.10LT00 | | 00 BR% | 1 01E+04 | 99 83% | 5 61F+02 | 99.95% | 1.92E+03 | %06.66 | 13.74 | 0.76 | 2.62 |
| ' ' - * | | | 00.00% DO 00% | 2 87E±03 | 00 80% | 2 00F+02 | 66.66 % | 8.59E+02 | 99.95% | 13.50 | 0.94 | 4.05 |
| · · | | | 00.02 % | 1 92F+02 | %06.66 | 2.10E+00 | 66.66 | 3.74E+01 | 99.95% | 18.00 | 0.20 | 3.50 |
| , t 1 | 10 1.0/ ET01 | | 00.00% | 1 925+02 | %06.66 | 2.10E+00 | %66 [.] 66 | 3.74E+01 | 99.95% | 18.00 | 0.20 | 3.50 |
| י <u>ה</u> נ | - | | 00 00% | 1 61E+03 | 99 94% | 1.79E+01 | %66 [°] 66 | 3.13E+02 | 99.97% | 18.00 | 0.20 | 3.50 |
| | 1/ 0.34C+04 | | 00.00 PD | 2 14F+03 | %66 66 | 2.38E+01 | 100.00% | 4.16E+02 | <u>99.99</u> % | 18.00 | 0.20 | 3.50 |
| | | • | 100.00% | 6.16E+02 | 100.00% | 6.80E+00 | 100.00% | 1.20E+02 | 100.00% | 18.00 | 0.20 | 3.50 |
| Cichal Tatal | 3 13F108 | UR . | | 4.52F+06 | | 5.20E+05 | | 1.86E+06 | | 13.17 | 1.52 | 5.43 |

| Altitude Band | Fuel | cum fuel | XON | | Ċ | | ç | | | (| |
|---------------------|----------|----------------|----------|----------------|-----------|-----------------|----------|---------------|---------|-------------|--------------|
| (km) | (kg/day) | (%) | (kg/day) | (%) | (kg/day) | (%) | (kg/day) | cum cu (%) | EI(NOX) | EI(HC) | EI(CO) |
| 0 - 1 | 3.37E+07 | 9.76% | 4.08E+05 | 8.99% | 1 77F+05 | 34 62% | 6 12ELOS | 20 070/ | Ţ | r C L | |
| + • | 9.17E+06 | 12.42% | 1.48E+05 | 12.25% | 2.86F+04 | 40.20% | | 30.01 % | 1.1.1 | 17.0 | 18.1/ |
| 2 - 3 | 8.55E+06 | 14.90% | 1.45E+05 | 15 46% | 2 34F+04 | 44 77% | | 00.00% | 0.0 | 0. IZ | 97.11 97 |
| 4 | 9.88E+06 | 17.77% | 1 80F+05 | 19 42% | 2 20E+04 | 10,000/04 | | 40.04% | 00.71 | 2.74 | 10.14 |
| 4 - 5 | 9.13E+06 | 20.41% | 1 54F+05 | 22 BU% | 2 20E 104 | 40.00 /o | 7 011 01 | 47.01% | 18.18 | 2.23 | 8.00 |
| 5,6 | 8.89E+06 | 22.99% | 1.43E+05 | 25.96% | 2.31F+04 | 58 07% | 7 005-04 | %Z6.10 | 10.84 | 2.52 | 8.71 |
| 6 - 7 | 8.97E+06 | 25.60% | 1.43E+05 | 29.11% | 2 26F+04 | 60.00 60 40% | 7 425-04 | 00.207 | | 2.60 | 8.90 0.00 |
| 7 - 8 | 9.65E+06 | 28.39% | 1 45F+05 | 30 31% | 2 2551.04 | 67 000/ | | 00.21% | 60.01 | Z9.Z | 8.26 |
| , , , | 0 21E-06 | 21 07% | | 07.01 /0 | | 0/ .U8% | 8.U5E+04 | 64.56% | 15.05 | 2.44 | 8.35 |
| | | | 1.325+03 | %77.CC | Z.1/E+04 | /1.32% | 7.51E+04 | 68.62% | 14.36 | 2.36 | 8.15 |
| | 1.925+07 | 30.04% | 2.085+05 | 41.12% | 2.42E+04 | 76.05% | 8.30E+04 | 73.11% | 13.93 | 1.26 | 4.32 |
| | 1.06E+08 | 67.41% | 1.26E+06 | 68.82% | 7.12E+04 | 89.95% | 3.11E+05 | 89.92% | 11.85 | 0.67 | 2.93 |
| 1 | 1.11E+08 | 99.66% | | 99.62% | 5.07E+04 | 99.85% | 1.83E+05 | 99.80% | 12.57 | 0.46 | 1.64 |
| - 71 - 71 | 6.84E+05 | 99.86% | | 99.83% | 5.40E+02 | 99.95% | 1.88E+03 | 66.90% | 13.76 | 0.79 | 2.75 |
| 13 - 14 | 2.09E+05 | 99.92% | 2.83E+03 | 99.89% | 1.90E+02 | 99.99% | 8.25E+02 | 99.95% | 13.52 | 0.91 | 7 0 T |
| | 1.11E+04 | 99.92% | | 99.89% | 2.20E+00 | 99.99% | 3.90E+01 | 99.95% | 18.00 | 0.20 | 05.6 |
| 15 - 16 | 1.11E+04 | 99.93% | 2.00E+02 | 80°.90% | 2.20E+00 | <u>99.99%</u> | 3.90E+01 | 99.95% | 18.00 | 0 20 | 3 50 |
| 16 - 17 | 9.34E+04 | 99.95% | 1.68E+03 | 99.94% | 1.87E+01 | 99.99% | 3.27E+02 | 99.97% | 18.00 | 0.20 | 3.50 |
| 1/ - 18 | | 66.66 % | 2.24E+03 | 66.66 % | 2.49E+01 | 100.00% | 4.36E+02 | 99.99% | 18.00 | 0.20 | 3.50 |
| 18 - 19 | 3.59E+04 | 100.00% | 6.45E+02 | 100.00% | 7.20E+00 | 100.00% | 1.26E+02 | 100.00% | 18.00 | 0.20 | 3.50 |
| Global Total | 3.45E+08 | | 4.54E+06 | | 5 125+05 | | 1 055,06 | | | | |
| | | | | | | | | | | | |

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Table C-5. Fuel burned, emissions, cumulative fractions of emissions, and effective emission indices as a function of altitude (Summed over Latitude and Longitude) for scheduled air traffic in May 1999.

| Altitude Band | land | Fuel | cum fuel | XON | cum NOx | НС | cum HC | 00 | cum CO | EI(NOx) | EI(HC) | EI(CO) |
|---------------|----------------|----------|----------------|----------|---------------------|----------|----------------|----------|----------------|---------|--------|--------|
| (km) | | (kg/day) | (%) | (kg/day) | (%) | (kg/day) | (%) | (kg/day) | (%) | | | |
| ' 0 | +- | 3.41E+07 | 9.82% | 4.14E+05 | 9.05% | 1.80E+05 | 35.00% | 6.20E+05 | 33.22% | 12.14 | 5.27 | 18.16 |
| י ד- (| · < | 9.28E+06 | 12.49% | 1.50E+05 | 12.33% | 2.91E+04 | 40.68% | 1.04E+05 | 38.82% | 16.18 | 3.14 | 11.26 |
| י - ת | I M | 8.64E+06 | 14.98% | 1.47E+05 | 15.55% | 2.35E+04 | 45.25% | 8.74E+04 | 43.50% | 17.05 | 2.72 | 10.12 |
| , I co |) 1 | 9.99E+06 | 17.85% | 1.82E+05 | 19.52% | 2.21E+04 | 49.56% | 7.98E+04 | 47.78% | 18.20 | 2.22 | 7.99 |
| , 1 | · LC | 9.24E+06 | 20.51% | 1.56E+05 | 22.93% | 2.30E+04 | 54.04% | 8.03E+04 | 52.09% | 16.89 | 2.49 | 8.69 |
| י ינת | ۍ د | 9.10E+06 | 23.13% | 1.47E+05 | 26.13% | 2.32E+04 | 58.56% | 8.04E+04 | 56.40% | 16.11 | 2.55 | 8.84 |
| י אנ |) r | 9.15F+06 | 25.76% | 1.45E+05 | 29.31% | 2.26E+04 | 62.97% | 7.52E+04 | 60.43% | 15.90 | 2.47 | 8.22 |
| , , | . œ | 9 88F+06 | 28.60% | 1.49E+05 | 32.56% | 2.35E+04 | 67.54% | 8.16E+04 | 64.81% | 15.04 | 2.38 | 8.26 |
| , . α | σ | 9.47F+06 | 31.33% | 1.36E+05 | 35.53% | 2.18E+04 | 71.79% | 7.63E+04 | 68.90% | 14.36 | 2.31 | 8.05 |
| י סס | , CF | 1.90E+07 | 36.79% | 2.62E+05 | 41.27% | 2.39E+04 | 76.45% | 8.29E+04 | 73.34% | 13.84 | 1.26 | 4.37 |
| - 1 - | ; = | 1.06E+08 | 67.26% | 1.26E+06 | 68.77% | 7.00E+04 | 90.07% | 3.11E+05 | 90.00% | 11.88 | 0.66 | 2.93 |
| ; ; , | : ^ | 1.13E+08 | %02 .66 | 1.41E+06 | 99 [.] 66% | 5.03E+04 | 99.86% | 1.83E+05 | 99.81% | 12.54 | 0.45 | 1.62 |
| - 67 | 1 <u>(</u> | 6.27E+05 | 99.88% | 8.66E+03 | 99.85% | 5.08E+02 | <u> 86.96%</u> | 1.92E+03 | 99.91% | 13.81 | 0.81 | 3.06 |
| 1 <u>6</u> | 44 | 1.45E+05 | 99.92% | 2.01E+03 | %06`66 | 1.53E+02 | 66.6 9% | 7.84E+02 | 99.95% | 13.88 | 1.06 | 5.42 |
| 14 - | 15 | 9.38E+03 | 99.93% | 1.69E+02 | %06.66 | 1.90E+00 | 66.99 % | 3.28E+01 | 99.95% | 18.00 | 0.20 | 3.50 |
| . t. | 16 | 9.38E+03 | 60.93% | 1.69E+02 | %06.66 | 1.90E+00 | 66.66 % | 3.28E+01 | 99.95% | 18.00 | 0.20 | 3.50 |
| 16 - | 17 | 8.88E+04 | <u>96.96</u> % | 1.60E+03 | 99.94% | 1.78E+01 | 66.66 % | 3.11E+02 | 99.97% | 18.00 | 0.20 | 3.50 |
| - 17 | 18 | 1.19E+05 | 99.99% | 2.14E+03 | 66.66 % | 2.38E+01 | 100.00% | 4.17E+02 | 66. 66% | 18.00 | 0.20 | 3.50 |
| 18 - | 19 | 3.43E+04 | 100.00% | 6.17E+02 | 100.00% | 6.90E+00 | 100.00% | 1.20E+02 | 100.00% | 18.00 | 0.20 | 3.50 |
| | | 0,176.00 | | A EREIDE | | 5 14E+05 | | 1 87F+06 | | 13.17 | 1.48 | 5.37 |
| GIODAI 101AI | otai | 3.4/E+U0 | | 4.001100 | | >>+ | | | | | 1 | |

| (km) | Altitude Band | Fuel | cum fuel | XON | cum NOx | Ċ | CH mit | 00 | | ELNOW | | |
|--------------------|---------------|----------|----------------|----------|----------------|----------|----------------|----------|----------------|-------|----------|---|
| | | (kg/day) | (%) | (kg/day) | (%) | (kg/day) | (%) | (kg/day) | (%) | | () | |
| ' 0 | - | 3.47E+07 | 9.72% | 4.21E+05 | 8.95% | 1.83E+05 | 34 89% | 6 29F405 | 33 00% | 1014 | 5 07 | |
| , - | 2 | 9.43E+06 | 12.36% | 1.53E+05 | 12.20% | 2.96E+04 | 40.54% | 1.06F+05 | 38.67% | 16.00 | 2.12 | 11.05 |
| - 2 | ო | 8.78E+06 | 14.82% | 1.50E+05 | 15.39% | 2.39E+04 | 45.10% | 8 89F+04 | 43.34% | 17.05 | 00 00 | C7.11 |
| ო | 4 | 1.02E+07 | 17.66% | 1.85E+05 | 19.32% | 2.26E+04 | 49.41% | 8.12E+04 | 47.61% | 18.21 | 2 20 0 | 00 2 |
| 4 | 5 | 9.39E+06 | 20.29% | 1.59E+05 | 22.69% | 2.34E+04 | 53.88% | 8.17E+04 | 51.90% | 16.90 | 2.50 | 02.4 07.8 |
| ى د | 9 | 9.24E+06 | 22.88% | 1.49E+05 | 25.86% | 2.36E+04 | 58.38% | 8.17E+04 | 56.20% | 16.13 | 2.55 | 8.84 |
| ' 9 | 7 | 9.29E+06 | 25.48% | 1.48E+05 | 29.01% | 2.30E+04 | 62.77% | 7.64E+04 | 60.21% | 15.92 | 2.47 | 8.22 |
| - 2 | æ | 1.00E+07 | 28.30% | 1.51E+05 | 32.22% | 2.39E+04 | 67.33% | 8.28E+04 | 64.56% | 15.06 | 2.38 | 8.25 |
| • ∞ | ග ් | 9.64E+06 | 31.00% | 1.39E+05 | 35.17% | 2.22E+04 | 71.57% | 7.75E+04 | 68.64% | 14.39 | 2.30 | 8.04 |
| י ס | 9 | 1.93E+07 | 36.42% | 2.68E+05 | 40.87% | 2.46E+04 | 76.26% | 8.46E+04 | 73.09% | 13.85 | 1.27 | 4.37 |
| 10 | ÷ | 1.09E+08 | 67.03% | 1.30E+06 | 68.52% | 7.18E+04 | 89.96% | 3.18E+05 | 89.82% | 11.90 | 0.66 | 2.91 |
| 11 - | 12 | 1.17E+08 | 99.70% | 1.46E+06 | 99.66 % | 5.18E+04 | 99.86% | 1.90E+05 | 99.81% | 12.56 | 0.44 | 1 63 |
| 12 | 13 | 6.65E+05 | 99.88% | 9.14E+03 | 99.85% | 5.19E+02 | <u> 86.96%</u> | 1.94E+03 | 99.91% | 13.75 | 0.78 | 66 C |
| 13 | 14 | 1.58E+05 | 99.93% | 2.21E+03 | 60.90% | 1.54E+02 | 66.66 % | 8.16E+02 | 99.95% | 13.97 | 0.97 | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 |
| 14 | 15 | 9.38E+03 | 99.93% | 1.69E+02 | <u> 80.90%</u> | 1.90E+00 | 66.66 % | 3.28E+01 | 99.95 % | 18.00 | 0.20 | 3.50 |
| 15 | 16 | 9.38E+03 | 99.93% | 1.69E+02 | 99.91% | 1.90E+00 | 66.66 % | 3.28E+01 | 66.96 % | 18.00 | 0.20 | 3.50 |
| 16 | 17 | 8.88E+04 | 66.96% | 1.60E+03 | 99.94% | 1.78E+01 | 66. 66% | 3.11E+02 | 99.97% | 18.00 | 0.20 | 3.50 |
| 17 - | 18 | 1.19E+05 | 66.66 % | 2.14E+03 | 99.99% | 2.38E+01 | 100.00% | 4.17E+02 | %66.66 | 18.00 | 000 | 3 50 |
| 18 - | 19 | | | | | | | | | 2000 | 0.4.0 | 0.00 |
| | | | | | | | | | | | | |
| Global Tota | | 3.57E+08 | | 4.70E+06 | | 5.24E+05 | | 1.90E+06 | | 13.17 | 1.47 | 5.33 |

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Table C-7. Fuel burned, emissions, cumulative fractions of emissions, and effective emission indices as a function of altitude (Summed over Latitude and Longitude) for scheduled air traffic in July 1999.

| Altitude Rand | Fuel | cum fuel | XON | cum NOX | Ŷ | cum HC | 00 | cum CO | EI(NOX) | EI(HC) | EI(CO) |
|---------------------------------|---------------------|---------------------|-----------|---------------------|----------|----------------|---|----------------|---------|--------|--------|
| (km) | (kg/day) | (%) | (kg/day) | (%) | (kg/day) | (%) | (kg/day) | (%) | | | |
| - | 3 4RF+07 | 9 63% | 4 23F+05 | 8.91% | 1.85E+05 | 35.00% | 6.34E+05 | 33.01% | 12.16 | 5.32 | 18.22 |
| - c - ' | 9.45F+06 | 12 25% | 1.53E+05 | 12.13% | 3.00E+04 | 40.68% | 1.07E+05 | 38.58% | 16.20 | 3.17 | 11.30 |
| - 0 ' ' | 8.80F+06 | 14.69% | 1.50E+05 | 15.29% | 2.42E+04 | 45.27% | 8.94E+04 | 43.24% | 17.06 | 2.75 | 10.17 |
| 1 C | 1 02F+07 | 17.51% | 1.85E+05 | 19.20% | 2.28E+04 | 49.58% | 8.17E+04 | 47.49% | 18.21 | 2.24 | 8.02 |
| | 9 40F+06 | 20 11% | 1.59E+05 | 22.55% | 2.36E+04 | 54.06% | 8.21E+04 | 51.77% | 16.92 | 2.52 | 8.74 |
| י ע ו ו ע | 9.75F-06 | 22.67% | 1.49E+05 | 25.69% | 2.38E+04 | 58.56% | 8.22E+04 | 56.06% | 16.13 | 2.57 | 8.88 |
| ר ה י י | 0.20270 0.20F706 | 25 24% | 1 48F+05 | 28.81% | 2.32E+04 | 62.95% | 7.68E+04 | 60.05% | 15.94 | 2.49 | 8.27 |
| - a | 3.20L100 | 28.02% | 1.51E+05 | 32.00% | 2.40E+04 | 67.50% | 8.32E+04 | 64.39% | 15.07 | 2.40 | 8.29 |
| ο σ | 9.66F+06 | 30.70% | 1.39E+05 | 34.93% | 2.24E+04 | 71.75% | 7.79E+04 | 68.45% | 14.40 | 2.32 | 8.07 |
| | 1.94F+07 | 36.08% | 2.69E+05 | 40.59% | 2.48E+04 | 76.45% | 8.57E+04 | 72.92% | 13.84 | 1.28 | 4.41 |
| - 11 - 11 | 1 11F+08 | 66.82% | 1.32E+06 | 68.34% | 7.20E+04 | 90.08% | 3.23E+05 | 89.77% | 11.87 | 0.65 | 2.91 |
| | 1 19F+08 | %69 66 | 1.49E+06 | <u>99.65%</u> | 5.16E+04 | 66% | 1.93E+05 | 99.81% | 12.52 | 0.44 | 1.62 |
| 10 - 13 | 6 77E+05 | 99,88% | 9.30E+03 | 99.85% | 5.26E+02 | <u>96.96</u> % | 1.95E+03 | 99.91% | 13.74 | 0.78 | 2.88 |
| 12 - 14 | 1 7RF+05 | %55 66 | 2.47E+03 | %06.66 | 1.60E+02 | %66`66 | 8.16E+02 | 99.95% | 13.88 | 06.0 | 4.59 |
| | 9 38F+03 | %86.66 | 1.69E+02 | 99.90% | 1.90E+00 | 66 .66% | 3.28E+01 | 99.95% | 18.00 | 0.20 | 3.50 |
| - 1 - 1 - 1 - 1 - 1 | 9.38F+03 | %86.66 | 1.69E+02 | 99.91% | 1.90E+00 | <u> 89.99%</u> | 3.28E+01 | <u>96.66</u> % | 18.00 | 0.20 | 3.50 |
| | B RRF+04 | %96 66 | 1.60E+03 | 99.94% | 1.78E+01 | 99.99% | 3.11E+02 | 99.97% | 18.00 | 0.20 | 3.50 |
| 17 - 18 | 1.19E+05 | %66 [.] 66 | 2.14E+03 | %66 ⁻ 66 | 2.38E+01 | 100.00% | 4.17E+02 | 99.99% | 18.00 | 0.20 | 3.50 |
| 18 - 19 | 3.43E+04 | 100.00% | 6.17E+02 | 100.00% | 6.90E+00 | 100.00% | 1.20E+02 | 100.00% | 18.00 | 0.20 | 3.50 |
| | | | | | 5 OREADS | | 1 92F+06 | | 13.15 | 1.46 | 5.32 |
| GIODAL LOTAL | 3.01E+U0 | | 4.1 JL100 | | 0.101 | | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | | 1 | | |

| | Altitude Band | Fuel | cum fuel | NOX | cum NOx | НС | cum HC | 8 | cum CO | EI(NOX) | EI(HC) | EI(CO) |
|---------------------|------------------|-----------|--------------------|---------------------|---------------|-------------|------------------|----------------------|-------------------|---------|--------|--------|
| | (km) | (kg/day) | (%) | (kg/day) | (%) | (kg/day) | (%) | (kg/day) | (%) | | | |
| 0 | . | 3.53E+07 | 9.70% | 4.31E+05 | 8 0R% | 1 005 05 | 76 A00/ | 10 LUT 0 | | | | |
| - | ۵ ۱ | 9.60E+06 | 12.33% | 1.56E+05 | 12.22% | 3 01 F + 04 | 41 10% | 0.40E+U5 | 33.23% | 12.19 | 5.38 | 18.28 |
| 2 | ო ' | 8.93E+06 | 14.78% | 1.53E+05 | 15.41% | 2.01LT04 | 41.10% | 0.06E+03 | 38./8% | 16.22 | 3.14 | 11.24 |
| ო | - 4 | 1.04E+07 | 17.63% | 1.89E+05 | 19.34% | 2.31F+04 | 49 99% | 9.00E+04 8.20E+04 | 43.45% | 17.10 | 2.74 | 10.14 |
| 4 | ۔ ۲ | 9.59E+06 | 20.26% | 1.62E+05 | 22 73% | 2 39F104 | EA 440/ | | 47.7170 70.000 | 10.23 | 2.23 | 8.00 |
| 5 | 9 | 9.34E+06 | 22.82% | 1.51E+0.5 | 25 A8% | 2 305 04 | 041.44 F0 040 | 0.336+04 | 52.00% | 16.92 | 2.49 | 8.68 |
| 9 | - 7 | 9.43E+06 | 25 41% | | 20.01% | | 00.91% | 8.28E+04 | 56.26% | 16.19 | 2.56 | 8.87 |
| 7 | 8 | 1 02F+07 | 28 20% | | ×10.62 | 2.34E+04 | 63.28% | 7.78E+04 | 60.27% | 15.95 | 2.48 | 8.25 |
| 8 | , o | 0 7READE | % 03.02 % 03.02 | | 32.22% | 2.44E+04 | 67.83% | 8.44E+04 | 64.61% | 15.10 | 2.40 | 8.29 |
| 0 | , e | 1 96F107 | 36 97% | 00+114-1 0 710 0 | 35.16% | 2.26E+04 | 72.05% | 7.88E+04 | 68.67% | 14.45 | 2.31 | 8.06 |
| 10 | ; ± | 1 10FT08 | 00.27 % | 2./1E+U3 | 40.82% | 2.4/E+04 | 76.67% | 8.63E+04 | 73.11% | 13.83 | 1.26 | 4.40 |
| : = | - - | 1 215,00 | % cc 00 | | 08.15% | 7.20E+04 | 90.11% | 3.22E+05 | 89.70% | 11.88 | 0.65 | 2.92 |
| - C - C | י ז ל | | 99.7.9% 00.000 | | 99.70% | 5.23E+04 | 99.87% | 1.97E+05 | 99.82% | 12.52 | 0.43 | 1.63 |
| ! <u>e</u> | - 4 | 1 REFLOS | 93.30% | · · | 99.88% | 4.94E+02 | 39.96% | 1.91E+03 | 99.92% | 13.91 | 0.78 | 3.04 |
| 4 | - - - | 6 32F103 | 00 0E% | 2.03E+U3 | 99.93% | 1.84E+02 | 99.99% | 8.82E+02 | 99.97% | 13.95 | 0.99 | 4.75 |
| - L - | , 1 1 1 | 6 32E 103 | 93.33 /o | | 99.94% | 1.30E+00 | 99.99% | 2.21E+01 | 99.97% | 18.00 | 0.20 | 3.50 |
| <u></u> | | | 99.90% | 1.14E+UZ | 99.94% | 1.30E+00 | 66.66 % | 2.21E+01 | 99.97% | 18.00 | 0.20 | 3.50 |
| | 2 9 | 0.03E+04 | 99.97% | 1.09E+03 | 80.96% | 1.21E+01 | 100.00% | 2.12E+02 | 99.98% | 18.00 | 0.20 | 3.50 |
| ά | 2 0 | | 99.99% 100.000 | 1.43E+03 | 66.66% 66% | 1.59E+01 | 100.00% | 2.79E+02 | 100.00% | 18.00 | 0.20 | 3.50 |
| 2 | 2 | Z.Z3C+04 | %nn.nn | 4.13E+02 | 100.00% | 4.60E+00 | 100.00% | 8.03E+01 | 100.00% | 18.00 | 0.20 | 3.50 |
| Global Total | Total | 3.64E+08 | | 4 80F+06 | | 10.100 | | | | | | |

Table Latituc

Table C-9. Fuel burned, emissions, cumulative fractions of emissions, and effective emission indices as a function of altitude (Summed over Latitude and Longitude) for scheduled air traffic in September 1999.

| Altitude Band (km) | Band | Fuel (kg/day) | cum fuel (%) | NO× (kg/day) | cum NOx (%) | HC (kg/day) | cum HC (%) | CO (kg/day) | cum CO (%) | cum CO El(NOx) (%) | EI(HC) | EI(CO) |
|-----------------------|------|------------------|-----------------|-----------------|---------------------|----------------|-----------------|----------------|----------------|-----------------------|--------|--------|
| | | | | 100 | | | 0.L T.0. | | | | | |
| 0 | • | 3.49E+07 | 9.76% | 4.23E+U5 | 9.01% | CU+308.1 | 30.00% | GU+365.0 | 07.2D% | 21.21 | 40.0 | 07.01 |
| • | 2 | 9.45E+06 | 12.41% | 1.53E+05 | 12.27% | 2.94E+04 | 41.18% | 1.06E+05 | 38.81% | 16.18 | 3.11 | 11.21 |
| ' N | ю | 8.81E+06 | 14.88% | 1.50E+05 | 15.46% | 2.39E+04 | 45.75% | 8.92E+04 | 43.49% | 17.01 | 2.72 | 10.13 |
| י רס | 4 | 1.02E+07 | 17.74% | 1.85E+05 | 19.40% | 2.26E+04 | 50.06% | 8.16E+04 | 47.76% | 18.15 | 2.21 | 7.99 |
| 4 | 5 | 9.48E+06 | 20.39% | 1.60E+05 | 22.81% | 2.33E+04 | 54.52% | 8.20E+04 | 52.06% | 16.86 | 2.46 | 8.65 |
| ۲ ک | 9 | 9.26E+06 | 22.98% | 1.49E+05 | 25.98% | 2.34E+04 | 58.98% | 8.17E+04 | 56.35% | 16.12 | 2.52 | 8.83 |
| ' 9 | 7 | 9.33E+06 | 25.60% | 1.48E+05 | 29.14% | 2.29E+04 | 63.36% | 7.68E+04 | 60.37% | 15.89 | 2.46 | 8.23 |
| - 2 | 80 | 1.01E+07 | 28.41% | 1.51E+05 | 32.36% | 2.38E+04 | 67.91% | 8.31E+04 | 64.73% | 15.04 | 2.36 | 8.26 |
| , 80 | ი | 9.67E+06 | 31.12% | 1.39E+05 | 35.32% | 2.21E+04 | 72.13% | 7.78E+04 | 68.80% | 14.40 | 2.29 | 8.04 |
| י ס | 10 | 1.95E+07 | 36.57% | 2.70E+05 | 41.06% | 2.42E+04 | 76.76% | 8.55E+04 | 73.28% | 13.84 | 1.24 | 4.39 |
| 10 | 1 | 1.08E+08 | 66.90% | 1.29E+06 | 68.44% | 7.01E+04 | 90.16% | 3.16E+05 | 89.82% | 11.88 | 0.65 | 2.91 |
| + + | 12 | 1.17E+08 | 69.69 % | 1.47E+06 | 99.65% | 5.07E+04 | 99.86% | 1.90E+05 | 99.80 % | 12.52 | 0.43 | 1.63 |
| 12 | 13 | 6.60E+05 | 99.88% | 9.17E+03 | 99.85% | 5.32E+02 | <u>96.96</u> % | 2.09E+03 | 99.91% | 13.90 | 0.81 | 3.18 |
| 13 - | 14 | 1.78E+05 | <u>99.93%</u> | 2.47E+03 | %06.66 | 1.64E+02 | %66.66 | 8.33E+02 | 99.95% | 13.88 | 0.92 | 4.69 |
| 14 - | 15 | 9.38E+03 | <u>99.93%</u> | 1.69E+02 | %06 [.] 66 | 1.90E+00 | 99.99% | 3.28E+01 | 99.95% | 18.00 | 0.20 | 3.50 |
| 15 - | 16 | 9.38E+03 | 99.93% | 1.69E+02 | 99.91% | 1.90E+00 | 99. <u>9</u> 9% | 3.28E+01 | <u>96.96</u> % | 18.00 | 0.20 | 3.50 |
| 16 - | 17 | 8.88E+04 | 66% | 1.60E+03 | 99.94% | 1.78E+01 | 66. 66% | 3.11E+02 | 99.97% | 18.00 | 0.20 | 3.50 |
| 17 - | 18 | 1.19E+05 | 66.66 % | 2.14E+03 | 66.66 % | 2.38E+01 | 100.00% | 4.17E+02 | %66 .66 | 18.00 | 0.20 | 3.50 |
| 18 | 19 | 3.43E+04 | 100.00% | 6.17E+02 | 100.00% | 6.90E+00 | 100.00% | 1.20E+02 | 100.00% | 18.00 | 0.20 | 3.50 |
| | | 1 | | | | | | L | | | 1 | |
| Global Total | otal | 3.57E+08 | | 4.70E+06 | | 5.23E+05 | | 1.91E+06 | | 13.16 | 1.4/ | 5.34 |

| Altitude Band | Band | Fuel | cum fuel | NOX | cum NOX | HC | | C | | EVNOVI | | |
|--------------------|----------|----------|----------------|----------|----------------|----------|----------------|----------|----------------|--------|---------------|-------|
| (km) | | (kg/day) | (%) | (kg/day) | (%) | (kg/day) | (%) | (kg/day) | (%) | | | |
| , 0 | - | 3.46E+07 | 9.76% | 4.20E+05 | 9.01% | 1.81E+05 | 35 26% | 6 25F105 | 33 17% | 1015 | л ОО | 10.07 |
| - | N | 9.38E+06 | 12.41% | 1.52E+05 | 12.27% | 2.88E+04 | 40.89% | 0.05F+05 | 38 73% | 16.10 | 0.2.0 2.07 | 10.0/ |
| ' 2 | e | 8.74E+06 | 14.88% | 1.49E+05 | 15.46% | 2.34E+04 | 45.46% | 8.81E+04 | 43.41% | 17 01 | 268 | |
| י רי | 4 | 1.01E+07 | 17.74% | 1.84E+05 | 19.40% | 2.22E+04 | 49.79% | 8.08E+04 | 47.70% | 18.14 | 010 | 7 97 |
| 4 | ъ | 9.41E+06 | 20.40% | 1.59E+05 | 22.81% | 2.29E+04 | 54.26% | 8.11E+04 | 52.01% | 16.85 | 2.43 | 8.62 |
| م | 9 | 9.20E+06 | 23.00% | 1.48E+05 | 25.98% | 2.30E+04 | 58.75% | 8.09E+04 | 56.31% | 16.11 | 2.50 | 8.79 |
| ' 9 | 7 | 9.26E+06 | 25.61% | 1.47E+05 | 29.14% | 2.25E+04 | 63.14% | 7.60E+04 | 60.34% | 15.88 | 2.43 | 8.20 |
| - 2 | ω | 9.98E+06 | 28.43% | 1.50E+05 | 32.36% | 2.34E+04 | 67.70% | 8.23E+04 | 64.71% | 15.04 | 2.34 | 8.24 |
| • ∞ | 6 | 9.56E+06 | 31.13% | 1.38E+05 | 35.31% | 2.17E+04 | 71.94% | 7.67E+04 | 68.78% | 14.41 | 2.27 | 8.02 |
| י ס | 10 | 1.92E+07 | 36.54% | 2.65E+05 | 41.00% | 2.39E+04 | 76.60% | 8.43E+04 | 73.26% | 13.83 | 1.25 | 4.40 |
| - | F | 1.08E+08 | 66.95% | 1.28E+06 | 68.46% | 6.91E+04 | 90.08% | 3.12E+05 | 89.80% | 11.89 | 0.64 | 2.89 |
| - | 12 | 1.16E+08 | 99.71% | 1.45E+06 | 99.67% | 5.00E+04 | 99.84% | 1.88E+05 | 99.78% | 12.54 | 0.43 | 1.62 |
| - 12 | 13 | 6.18E+05 | 99.88% | 8.52E+03 | 99.85% | 5.97E+02 | 99.95% | 2.24E+03 | 60.90% | 13.78 | 0.97 | 3.62 |
| - - | 14 | 1.62E+05 | 99.93% | 2.25E+03 | 66.90% | 1.85E+02 | 99.99% | 9.02E+02 | 99.95% | 13.93 | 1.14 | 5.58 |
| 44 | 15 | 9.38E+03 | 99.93% | 1.69E+02 | 80°.90% | 1.90E+00 | 99.99% | 3.28E+01 | 99.95% | 18.00 | 0.20 | 3.50 |
| 15 | 16 | 9.38E+03 | 99.93% | 1.69E+02 | 99.91% | 1.90E+00 | 66.66 % | 3.28E+01 | 66.96% | 18.00 | 0.20 | 3.50 |
| 16 1 | 17 | 8.88E+04 | 66.96% | 1.60E+03 | 99.94% | 1.78E+01 | 66.66 % | 3.11E+02 | 99.97% | 18.00 | 0.20 | 3.50 |
| - 17 | 18 | 1.19E+05 | 66.66 % | 2.14E+03 | 66.66 % | 2.38E+01 | 100.00% | 4.17E+02 | 66.66 % | 18.00 | 0.20 | 3.50 |
| 18 - | 19 | 3.43E+04 | 100.00% | 6.17E+02 | 100.00% | 6.90E+00 | 100.00% | 1.20E+02 | 100.00% | 18.00 | 0.20 | 3.50 |
| Global Tota | tal | 3.54E+08 | | 4.66E+06 | | 5.13E+05 | | 1.88E+06 | | 13.16 | 1 45 | 5.32 |
| | | | | | | | | | | 2 | > | 1 |

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Table C-11. Fuel burned, emissions, cumulative fractions of emissions, and effective emission indices as a function of altitude (Summed over Latitude and Longitude) for scheduled air traffic in November 1999.

Appendix C – Altitude Distribution of Fuel Burn and Emissions for Each Month of 1999

| Altitude Band (km) | Band | Fuel (ka/dav) | cum fuel (%) | NOX (ka/dav) | cum NOx (%) | HC (ka/dav) | cum HC (%) | CO (ka/dav) | cum CO (%) | EI(NOx) | EI(HC) | EI(CO) |
|-----------------------|------|------------------|-----------------|-----------------|---------------------|----------------|----------------|----------------|---------------|---------|--------|--------|
| | | | | | | | | 16 6-1 | | | | |
| - 0 | - | 3.36E+07 | 9.70% | 4.11E+05 | 8.97% | 1.69E+05 | 34.60% | 6.01E+05 | 33.09% | 12.24 | 5.05 | 17.89 |
| - | N | 9.11E+06 | 12.34% | 1.49E+05 | 12.21% | 2.73E+04 | 40.17% | 1.01E+05 | 38.66% | 16.31 | 3.00 | 11.09 |
| ح | ო | 8.51E+06 | 14.80% | 1.46E+05 | 15.39% | 2.27E+04 | 44.81% | 8.56E+04 | 43.37% | 17.12 | 2.67 | 10.06 |
| ღ | 4 | 9.88E+06 | 17.65% | 1.80E+05 | 19.33% | 2.16E+04 | 49.21% | 7.83E+04 | 47.68% | 18.24 | 2.18 | 7.93 |
| 4 | 5 | 9.18E+06 | 20.30% | 1.56E+05 | 22.73% | 2.23E+04 | 53.75% | 7.87E+04 | 52.02% | 16.96 | 2.43 | 8.57 |
| ء ع | 9 | 8.98E+06 | 22.90% | 1.45E+05 | 25.90% | 2.24E+04 | 58.31% | 7.84E+04 | 56.33% | 16.18 | 2.49 | 8.73 |
| 9 | 7 | 9.07E+06 | 25.52% | 1.45E+05 | 29.06% | 2.18E+04 | 62.77% | 7.35E+04 | 60.39% | 15.94 | 2.41 | 8.10 |
| - 2 | 8 | 9.80E+06 | 28.35% | 1.48E+05 | 32.29% | 2.27E+04 | 67.40% | 7.95E+04 | 64.76% | 15.10 | 2.31 | 8.11 |
| 8 | 6 | 9.33E+06 | 31.05% | 1.35E+05 | 35.24% | 2.10E+04 | 71.68% | 7.38E+04 | 68.83% | 14.51 | 2.25 | 7.91 |
| 6 | 10 | 1.85E+07 | 36.41% | 2.59E+05 | 40.90% | 2.27E+04 | 76.33% | 8.03E+04 | 73.25% | 13.97 | 1.23 | 4.33 |
| 10 - | 11 | 1.04E+08 | 66.48% | 1.25E+06 | 68.10% | 6.63E+04 | 89.85% | 2.97E+05 | 89.63% | 11.98 | 0.64 | 2.86 |
| + | 12 | 1.15E+08 | 99.72% | 1.45E+06 | 69.69 % | 4.92E+04 | 99.89% | 1.85E+05 | 99.84% | 12.58 | 0.43 | 1.61 |
| 12 - | 13 | 5.63E+05 | 99.89% | 7.66E+03 | 99.85% | 3.43E+02 | <u>96.96</u> % | 1.38E+03 | 99.91% | 13.62 | 0.61 | 2.46 |
| 13 - | 14 | 1.22E+05 | 99.92% | 1.71E+03 | 66.89 % | 1.21E+02 | 66.66 % | 6.40E+02 | 99.95% | 14.02 | 0.99 | 5.25 |
| 14 - | 15 | 1.11E+04 | 99.92% | 2.00E+02 | %06 .66 | 2.20E+00 | 66 .66% | 3.90E+01 | 99.95% | 18.00 | 0.20 | 3.50 |
| 15 - | 16 | 1.11E+04 | 99.93% | 2.00E+02 | %06 [.] 66 | 2.20E+00 | <u>99.99%</u> | 3.90E+01 | 99.95% | 18.00 | 0.20 | 3.50 |
| 16 - | 17 | 9.34E+04 | 99.95% | 1.68E+03 | 99.94% | 1.87E+01 | 99.99% | 3.27E+02 | 99.97% | 18.00 | 0.20 | 3.50 |
| 17 - | 18 | 1.24E+05 | 66.66 % | 2.24E+03 | %66 .66 | 2.49E+01 | 100.00% | 4.36E+02 | 99.99% | 18.00 | 0.20 | 3.50 |
| 18 - | 19 | 3.59E+04 | 100.00% | 6.45E+02 | 100.00% | 7.20E+00 | 100.00% | 1.26E+02 | 100.00% | 18.00 | 0.20 | 3.50 |
| Clobal Total | ļ | 2 465,00 | | | | | | 1 875,06 | | 10.01 | CV F | R OR |
| | (a) | 0.400+00 | | 4.300+00 | | 4.300+00 | | 1.025+00 | | 13.24 | 1.46 | 1 |

| Altitude | Altitude Band | Fuel | cum fuel | Ň | cum NOx | 오 | cum HC | 8 | cum CO | EI(NOX) | EI(HC) | EI(CO) |
|-------------|---------------|----------|----------------|----------|----------------|----------|----------------|----------|----------------|---------|--------|--------------|
| (km) | Ê | (kg/day) | (%) | (kg/day) | (%) | (kg/day) | (%) | (kg/day) | (%) | | | |
| 0 | - | 3.37E+07 | 9.62% | 4.13E+05 | 8.90% | 1.70E+05 | 34.44% | 6.03E+05 | 32.99% | 12.26 | 5.04 | 17.93 |
| - | ∾. | 9.15E+06 | 12.23% | 1.49E+05 | 12.12% | 2.74E+04 | 40.00% | 1.02E+05 | 38.56% | 16.32 | 2.99 | 11.13 |
| N | ი | 8.56E+06 | 14.68% | 1.47E+05 | 15.28% | 2.28E+04 | 44.63% | 8.63E+04 | 43.28% | 17.13 | 2.66 | 10.08 |
| ღ | 4 | 9.91E+06 | 17.51% | 1.81E+05 | 19.18% | 2.16E+04 | 49.01% | 7.88E+04 | 47.58% | 18.27 | 2.18 | 7.95 |
| 4 | ۍ | 9.20E+06 | 20.14% | 1.56E+05 | 22.55% | 2.23E+04 | 53.54% | 7.90E+04 | 51.90% | 16.98 | 2.42 | 8.59 |
| ص | 9 | 9.02E+06 | 22.71% | 1.46E+05 | 25.70% | 2.25E+04 | 58.10% | 7.88E+04 | 56.21% | 16.20 | 2.49 | 8.74 |
| 9 | - 7 | 9.11E+06 | 25.32% | 1.45E+05 | 28.84% | 2.19E+04 | 62.55% | 7.39E+04 | 60.25% | 15.95 | 2.40 | 8.11 |
| | 8 | 9.82E+06 | 28.12% | 1.49E+05 | 32.04% | 2.27E+04 | 67.16% | 7.99E+04 | 64.62% | 15.12 | 2.32 | 8.13 |
| œ | 6 | 9.39E+06 | 30.80% | 1.36E+05 | 34.99% | 2.11E+04 | 71.44% | 7.42E+04 | 68.68% | 14.53 | 2.25 | 7.90 |
| ი | -9 | 1.89E+07 | 36.19% | 2.65E+05 | 40.71% | 2.30E+04 | 76.12% | 8.07E+04 | 73.09% | 14.07 | 1.22 | 4.28 |
| 10 | ÷ | 1.05E+08 | 66.30% | 1.26E+06 | 67.96% | 6.69E+04 | 89.70% | 3.00E+05 | 89.49% | 11.99 | 0.63 | 2.85 |
| ÷ | 12 | 1.17E+08 | 69.69 % | 1.47E+06 | 66% | 5.00E+04 | 99.84% | 1.88E+05 | 99.79% | 12.57 | 0.43 | 1.61 |
| 12 | - 13 | 6.29E+05 | 99.87% | 8.66E+03 | 99.84% | 4.97E+02 | 99.94% | 1.91E+03 | 99.89% | 13.75 | 0.79 | 3.04 |
| 13 | - 14 | 1.81E+05 | 99.93% | 2.52E+03 | %06.66 | 2.44E+02 | 66.66 % | 1.08E+03 | 99.95% | 13.89 | 1.35 | 5.95 |
| 14 | . 15 | 1.42E+04 | 99.93% | 2.55E+02 | 60.90% | 2.80E+00 | 66.66 % | 4.96E+01 | 66.95% | 18.00 | 0.20 | 3.50 |
| 15 | . 16 | 1.42E+04 | 99.93 % | 2.55E+02 | 99.91% | 2.80E+00 | 66. 99% | 4.96E+01 | 66.06% | 18.00 | 0.20 | 3.50 |
| 16 | - 17 | 8.71E+04 | 66.96% | 1.57E+03 | 99.94% | 1.74E+01 | 66.66 % | 3.05E+02 | 99.97% | 18.00 | 0.20 | 3.50 |
| 17 | - 18 | 1.13E+05 | 66.66% | 2.03E+03 | <u> 39.99%</u> | 2.25E+01 | 100.00% | 3.94E+02 | 66.66 % | 18.00 | 0.20 | 3.50 |
| 18 | . 19 | 3.24E+04 | 100.00% | 5.83E+02 | 100.00% | 6.50E+00 | 100.00% | 1.13E+02 | 100.00% | 18.00 | 0.20 | 3.50 |
| Global Tota | otal | 3.50E+08 | | 4 64F+06 | | 4 93E+05 | | 1 83F±06 | | 13 OF | 1 41 | л <u>9</u> 3 |
| | | | | >> | | >> | | >> | | 01.01 | - + - | 2.50 |

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| | | | 5 | 0/ 24 | 1-0 kr | 1-0 km Altitude Band | and | 9-131 | 9-13 km Altitude Band | Band | Fuel | Fuel |
|----------|---------------------------|---------|--------|-----------------|--------|----------------------|------------------|----------------|-----------------------|----------------|----------|-----------|
| | | Ľ | | | 2 | | | | | | (1000 | (1000 |
| - | | 11000 | Friel | within | Ξ | Ē | Ξ | Ξ | Ξ | Ξ | kg/day) | kg/day) |
| Generic | 0AG Aimlana/annina | ka/dav) | Burned | Type | (XON) | (co) | (HC) | (NOX) | (co) | (HC) | (1-9 km) | (9-13 km) |
| I ype | | | | | | | | | | | ~ | - |
| Airbus A | Airbus A300-600 | 6,397.3 | 1.8% | | 17.8 | 10.1 | 2.0 | 12.2 | 1.7 | 0.3 | 1,675.9 | 3,953.9 |
| | | | | | | (| יי נ | • C | 00 | с U | 973.0 | 1 436.2 |
| | A300-620B PW4000-4158 | 2,854.1 | | 44.6% | 17.3 | 7.6 | 0./ | 13.1 | 0 I V | , , , | 1 2 2 0 | 1 BEF B |
| | | 2,419,1 | | 37.8% | 18.2 | 17.6 | 5.5 | 11.2 | 1.5 | <u>0.</u> 4 | 1./00 | 0.000,1 |
| | | 151 5 | | 7 1% | 17.7 | 12.4 | 3.6 | 13.0 | 1.3 | 0.3 | 142.4 | 11.062 |
| | A300-600_CF6-80CZA3 | | | √0∠ V | 211 | 52 | 0.7 | 13.1 | 2.0 | 0.4 | 121.3 | 134.9 |
| | A300-620_JT9D-7H4H1 | 239.0 | | 20 V | 17.0 | 99 | 0.7 | 13.1 | 1 2 | 0.3 | 52.9 | 174.3 |
| | A300-600_FRT_CF6-80C2A5F | 8.502 | | ° ° ° ° | | | σ | 13.0 | 1.9 | 0.1 | 10.7 | 46.7 |
| | A300-620_PW4000-4158 | 62.8 | | 0.0.1 | | | o c | 6 F F | e. F | 0.3 | 8.5 | 45.8 |
| | A300-600R_CF6-80C2A5F | 56.0 | | 0.9% | 10.9 | 10.0 | 2.0 | 2 | 2 | | | |
| | | | | | 1 | | 6 | 4 | 10 | 1 0 | 523.6 | 1.273.5 |
| Airbus | Airbus A300-B2/B4/F4 | 2,004.3 | 0.6% | | 22.2 | 13.1 | Z.C | 14.0 | <u>.</u> | <u>!</u> | | |
| | | | | 701 00 | 23.3 | 1 1 | 4.5 | 14.9 | 1.8 8 | 1.2 | 136.9 | 441.6 |
| | A300-B4-200_CF6-50C2 | 049.2 | | 0/ 1.30 | | | 57 | 14.5 | 2.0 | 1.2 | 91.1 | 182.2 |
| | A300-B2-100_CF6-50C | 316.1 | | 0.0.01 | | 0.01 | י ע - ע | 871 | 5.0 | 1.2 | 68.9 | 140.0 |
| | A300-B2-200_CF6-50C2R | 225.2 | | 0/2/11 20/20 | | | 0 0 | 101 | 16 | 1.4 | 41.8 | 152.3 |
| | A300-B4-120_JT9D-59A | 213.8 | | 10.7% | 19.7 | |) - - | | - C | 12 | 63.9 | 76.8 |
| | A300-B2-200FF_CF6-50C2 | 163.5 | | 8.2% | 21.4 | 10. r | - c | t . | | ! . | 77.5 | |
| | A300-B2-200_CF6-50C2 | 143.1 | | 7.1% | 21.0 | 15.4 15.4 | 0 0 | - + + u | - ト J Ŧ | | 19.6 | Ŧ |
| | A300-B4-200F_FRT_CF6-50C2 | 133.9 | | 6.7% | 23.5 | 10./ | 4 v. o | | | | 0.41 | 0.89 |
| | A300-F4-200 FRT_CF6-50C2 | 115.0 | | 5.7% | 24.6 | 10.6 | 4 201 | - L | > c | | | 16.8 |
| | A300-B4-200FF CF6-50C2 | 24.9 | | 1.2% | 24.4 | 11.7 | 4./ | 0.4 | 2 T | 4 C | | 116 |
| | A300-B4-100 CF6-50C2 | 19.5 | | 1.0% | 24.4 | 12.0 | 4.8 | 14.4 | 2.1 | <u>י</u> | r r | |
| | | | | | | | | | | | | |

| Generic OAG Fuel Generic OAG (1000 Type Airplane/engine kg/day) Airbus A310 5,297.5 Airbus A310 5,297.5 Airbus A310 5,297.5 A310-300_CF6-80C2A2 1,583.2 A310-300_CF6-80C2A2 1,583.2 A310-200_CF6-80C3A8 1,022.6 A310-200_CF6-80A3 576.6 | Global Fuel 1.5% | Total within Type | ū | Ē | | 2 | | | Luel | Fuel |
|---|-------------------------------|-------------------------|-------|--------------|--------------|-------------|------------|------|-------------------|-----------|
| Airplane/engine Airplane/engine A310-300_CF6-80C2A2 A310-300_CF6-80C2A8 A310-200_CF6-80C2A8 A310-200_CF6-80A3 A310-200_CF6-80A3 | | within Type | Ū | ī | | | | | | 00017 |
| Anplane/engine s A310 A310-300_CF6-80C2A2 A310-320_PW4000-4152 A310-200_CF6-80A3 A310-200_CF6-80A3 | | Type | ł | Ū | Ξ | Ē | ũ | ū | (1000) ka/dav) | (1000 |
| 10-300_CF6-80C2A2 10-320_PW4000-4152 10-300_CF6-80C2A8 10-200_CF6-80A3 | | | (XON) | (co) | (HC) | (NOX) | (co) | (HC) | (1-9 km) | (9-13 km) |
| 2 | | | 18.5 | 15.3 | 4.7 | 11.3 | 2.2 | 0.6 | 793.8 | 4,091.6 |
| N | | 29.9% | 17.2 | 16.7 | с Ч | , , , | 0 | 1 | | |
| | | 25.2% | 17.9 | 17.7 | י ע ע ע | | 2.2 | 0.5 | 255.8 | 1,203.4 |
| | | 10 3% | 17.0 | | | N | 22 | 0.5 | 177.1 | 1,057.2 |
| | | | 0.7 | 0.12 0.12 | 0.0 | 10.2 | 2.0 | 0.5 | 119.7 | 841.0 |
| | | %.D.1 | 19.2 | 5.8 | ເ | 12.8 | 2.9 | 0.7 | 114.5 | 408.5 |
| | | 5.5% | 18.4 | 20.2 | 6.6 | 11.1 | 2.7 | 0.8 | 45.9 | 219.9 |
| | | 3.7% | 28.6 | 3.9 | 0.6 | 14.4 | 1.4 | 0,3 | 34.3 | 140 5 |
| | | 3.4% | 17.6 | 18.1 | 5.6 | 11.2 | 2.1 | 0.5 | 24.4 | |
| 112.1 112.1 | | 2.1% | 27.2 | 3.7 | 0.6 | 14.4 | 1.4 | 0.3 | 22.2 | 2.77 |
| Airbus A319 2.048.1 | 0.6% | | 116 | ł | | | | | | |
| | 2 | | 0.4 | 1.6 | ~~~ ^ | 10.9 | 2.5 | 0.3 | 655.4 | 1,164.9 |
| A319-130_V2500-2522-A5 622.2 | | 30.4% | 15.9 | ц С | • | | u c | | | - |
| A319-110_CFM56-5A5 582.2 | | 28.4% | 14.0 | 0.0 | | 0.0 1 | C 7 | 0.1 | 132.6 | 447.9 |
| A319-110_CFM56-5B6_P | | 13 60/ | 0.4 | 4 0 0 0 | 0.0 | 2.0L | 2.1 | 0.5 | 190.0 | 330.2 |
| | | 0.0.C | | 8.8 0 | 1.6 | 11.7 | 2.5 | 0.5 | 65.1 | 182.8 |
| ٩ | | 8 - 10 - 10 | 12.3 | 3.9 | 0.5 | 9.8 | 2.4 | 0.4 | 147.8 | 0.4 |
| n | | 9.1% | 16.5 | 9.0 | 1.9 | 11.5 | 3.1 | 0.7 | 49.5 | 110.8 |
| | | 5.9% | 16.0 | 8.5 | 1.7 | 11.3 | 2.9 | 0.6 | 48.2 | 50.2 |
| | | 3.5% | 15.1 | 5.0 | 0.1 | 10.7 | 2.5 | 0.1 | 22.2 | 42 F |

| | | % of | % of | 1-9 | 1-9 km/ltitude Band | Band | 9-1 | 9-13 kmAltitude Band | e Band | Fuel | Fuel |
|-------------------------|----------|---------|-----------------|--------------|---------------------|-------|------|----------------------|------------------|---------|---------|
| | Fuel | Global | Total | | | | | | | (1000 | (1000 |
| Generic OAG | (1000 | Fuel wi | within H | | Ξ | Ξ | Ξ | Ξ | l kg/day) | kg/day) | |
| Type Airplane/engine | kg/day) | Burned | Type | (NOX)(CO) | (HC) | (NOX) | (co) | (HC) | (1-9 km) (9-13 l | tm) | |
| Airbus A320 | 11,883.6 | 3.4% | | 17.5 | 5.6 | 0.5 | 12.0 | 2.0 | 0.4 | 3,233.9 | 7,284.7 |
| A320-210 CFM56-5A1 | 5,882.1 | | 49.5% | 16.7 | 5.4 | 0.6 | 11.0 | 2.1 | 0.5 | 1,690.7 | 3,409.0 |
| A320-230_V2500-2527-A5 | 1,943.2 | - | 16.4% | 16.6 | 6.2 | 0.1 | 11.5 | 2.1 | 0.1 | 412.6 | 1,373.1 |
| A320-230_V2500-2500-A1 | 1,927.9 | • | 16.2% | 21.4 | 4.8 | 0.2 | 15.9 | 1.5 | 0.3 | 507.2 | 1,259.7 |
| A320-210_CFM56-5A3 | 791.1 | | 6.7% | 16.9 | 5.2 | 0.5 | 11.0 | 2.1 | 0.4 | 200.4 | 498.0 |
| A320-230_V2500-2527E-A5 | 344.6 | | 2.9% | 15.0 | 6.2 | 0.1 | 11.6 | 2.1 | 0.1 | 90.8 | 234.2 |
| A320-210_CFM56-5B4_2 | 327.8 | | 2.8% | 18.5 | 7.8 | 1.5 | 12.6 | 2.4 | 0.5 | 113.8 | 160.8 |
| A320-210_CFM56-5B4_P | 281.9 | 2 | 2.4% | 6.9 | 7.8 | 1.5 | 12.6 | 2.7 | 0.6 | 81.0 | 160.2 |
| A320-210_CFM56-5B4_2P | 161.7 | - | 1.4% | 5.9 (| 6.7 | 1.3 | 12.6 | 2.8 | 0.6 | 64.9 | 73.4 |
| A320-210_CFM56-5B4 | 120.2 | | 1.0% | 16.7 | 5.4 | 0.6 | 11.0 | 2.2 | 0.5 | 34.4 | 69.3 |
| A320-110_CFM56-5A1 | 103.1 | | 0.9% | 16.7 | 5.5 | 0.6 | 11.3 | 2.4 | 0.5 | 38.0 | 47.0 |
| Airbus A321 | 1,405.1 | 0.4% | | 17.5 | 6.4 | 0.6 | 13.3 | 1.7 | 0.2 | 591.8 | 588.2 |
| A321-110_CFM56-5B2 | 409.9 | | 29.2% | 18.2 | 11.2 | 1.4 | 13.5 | 1.8 | 0.3 | 129.7 | 226.3 |
| A321-210_CFM56-5B3_P | 288.8 | й | 20.6% | 7.4 | 3.6 | 0.1 | 3.4 | 1.9 | 0.1 | 162.7 | 74.2 |
| A321-130_V2500-2530-A5 | 229.9 | • | 16.4% | 16.1 | 4.3 | 0.1 | 12.5 | 1.8 | 0.1 | 118.7 | 60.2 |
| A321-110_CFM56-5B1_2 | 228.8 | | 16.3% | 17.6 | 10.1 | 1.4 | 13.4 | 1.6 | 0.3 | 84.4 | 110.7 |
| A321-230_V2500-2533-A5 | 203.0 | | 14.4% | 17.7 | 3.7 | 0.1 | 13.4 | 1.7 | 0.1 | 86.0 | 86.7 |
| A321-210_CFM56-5B3_2P | 44.8 | n | 3.2% | 20.1 20.1 | 4.5 | 0.1 | 3.2 | 1.8 | 0.1 | 10.2 | 30.1 |
| | | | | | | | | | | | |

| | | | % of | % of | 1-9 kr | 1-9 km Altitude Band | Band | 9-13 k | 9-13 km Altitude Band | Band | File | End |
|-----------------|--|--------------|--------|----------------|--------------|----------------------|--------------|--------------|-----------------------|------------|--------------|-----------|
| | | Fuel | Global | Total | | | | | | 5 | (1000 | (1000 |
| Generic | OAG | (1000 | Fuel | within | ū | Ē | Ξ | Ξ | Ш | Ξ | kq/dav) | ka/dav) |
| Type | Airplane/engine | kg/day) | Burned | Type | (XON) | (co) | (HC) | (NOX) | (co) | (HC) | (1-9 km) | (9-13 km) |
| Airbus A | Airbus A330-200 | 847.9 | 0.2% | ······ | 24.3 | 6.5 | 1.0 | 16.3 | 1.6 | 0.3 | 109.4 | 691.8 |
| | A330-220_PW4000-4168A | 733.3 | | 86.5% | 24.5 | 6.7 | 1.0 | 16.9 | 1.8 | 0.1 | 98.5 | 593.9 |
| | A330-240_Trent-772B-60 | 108.7 | | 12.8% | 22.4 | 4.0 | 0.7 | 12.9 | 0.7 | 1.2 | 10.2 | 93.1 |
| | A330-200_CF6-80E1A4 | 5.8 | | 0.7% | 26.9 | 14.2 | 4.5 | 13.6 | 1.2 | 0.3 | 0.7 | 4.8 |
| Airbus A | Airbus A330-300 | 3,402.0 | 1.0% | | 23.0 | 7.0 | 1.5 | 14.5 | 1.3 | 0.5 | 690.4 | 2,387.9 |
| | A330-320_PW4000-4168 | 1,022.1 | | 30.0% | 24.2 | 6.9 | 1.2 | 16.1 | 1.8 | 0.2 | 202.6 | 719.2 |
| | A330-300_CF6-80E1A2 | 840.5 | | 24.7% | 21.8 | 12.8 | 3.5 | 13.9 | 1.1 | 0.2 | 136.7 | 645.7 |
| | A330-340_Trent-772-60 | 756.3 | | 22.2% | 22.1 | 3.6 | 0.7 | 13.0 | 0.8 | 1.1 | 172.3 | 499.0 |
| | A330-320_PW4000-4164 | 420.6 | | 12.4% | 23.5 | 6.8 | 1.2 | 16.0 | 1.9 | 0.2 | 135.1 | 228.1 |
| | A330-340_Trent-768-60 | 362.5 | | 10.7% | 23.7 | 3.6 | 0.6 | 13.3 | 0.7 | 1.1 | 43.6 | 295.9 |
| Airbus A340-200 | 1340-200 | 910.4 | 0.3% | | 23.1 | 11.2 | 4.6 | 13.7 | 1.8 | 0.1 | 68.4 | 815.5 |
| | A340-210_CFM56-5C2 | 601.2 | | 66.0% | 23.1 | 11.1 | 4.6 | 13.8 | 1.8 | 0.1 | 44.1 | 539.3 |
| | A340-210_CFM56-5C2G | 176.9 | | 19.4% | 23.0 | 10.5 | 4.2 | 13.6 | 1.6 | 0.1 | 11.7 | 161.3 |
| | A340-210_CFM56-5C3_F | 132.3 | | 14.5% | 22.8 | 12.1 | 5.0 | 13.7 | 1.9 | 0.2 | 12.6 | 114.9 |
| Airbus A340-300 | 1340-300 | 8,242.4 | 2.4% | | 23.0 | 11.3 | 4.7 | 13.7 | 1.7 | 0.2 | 706.4 | 7,228.7 |
| | A340-310_CFM56-5C4 | 4,989.6 | | 60.5% | 23.1 | 11.6 | 4.8 | 13.7 | 1.8 | 0.2 | 447.2 | 4,346.2 |
| | | 2,658.9 | | 32.3% | 23.2 | 10.8 | 4.4 | 13.7 | 1.7 | 0.1 | 188.1 | 2,391.6 |
| | A340-310_CFM56-5C3_F | 594.0 | | 7.2% | 21.6 | 11.1 | 4.4 | 13.7 | 1.9 | 0.2 | 71.1 | 490.8 |
| BAC111 | | 157.7 | 0.0% | | 14.4 | 25.5 | 15.1 | 10.1 | 14.7 | 6.0 | 57.9 | 73.1 |
| | One-Eleven-500_Spey-512-14DW One-Eleven-560_Spey-512-14DW | 98.9 58.9 | | 62.7% 37.3% | 14.1 15.1 | 26.2 23.8 | 15.4 14.5 | 10.2 10.0 | 14.9 14.4 | 6.2 6.2 | 39.2 18.6 | 43.6 |
| | | | | | | | |).). | | > |))) | 5.54 |

| 1999 Aircraft |
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| Indices 1 |
| Emissions |
| Global |
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| Appendix D |

| | | | % of | % of | 1-9 k | 1-9 km Altitude Band | Band | 9-13 k | 9-13 km Altitude Band | Band | Fuel | Fuel |
|------------|-----------------------------|---------|--------|------------|-------|----------------------|--------|--------|-----------------------|------|----------|-----------|
| | | Fuel | Global | Total | | | | | | | (1000 | (1000 |
| Generic | OAG | (1000 | Fuel | within | Ш | Ξ | ū | Ξ | Ξ | Ξ | kg/day) | kg/dav) |
| Type | Airplane/engine | kg/day) | Burned | Type | (NOX) | (co) | (HC) | (NOX) | (co) | (HC) | (1-9 km) | (9-13 km) |
| BAE 146 | 9 | 2.329.6 | %L U | | 0 | 2 | и С | 0 2 | 4 | č | C 100 | |
| | | | 2 | | - | 2.0 | 2 | 0. | <u>.</u> | | 921.3 | C'NCR |
| | 146-200_ALF502-R-5 | 1,555.3 | | 66.8% | 9.1 | 5.0 | 0.4 | 7.7 | 1.6 | 0.1 | 624.1 | 616.3 |
| | 146-300_ALF502-R-5 | 432.9 | | 18.6% | 9.2 | 4.6 | 0.4 | 7.7 | 1.6 | 0.1 | 185.5 | 157.2 |
| | 146-100_ALF502-R-5 | 183.3 | | 7.9% | 9.1 | 4.9 | 0.4 | 7.8 | 1.6 | 0.1 | 57.7 | 98.7 |
| | 146-300_LF507-1H | 137.6 | | 5.9% | 9.5 | 6.3 | 0.6 | 8.1 | 1.5 | 0.0 | 52.6 | 69.2 |
| | 146-300QT_FRT_ALF502-R-5 | 20.5 | | 0.9% | 9.1 | 4.6 | 0.4 | 7.7 | 1.6 | 0.1 | 7.4 | 9.0 |
| Boeing 707 | 707 | 606.8 | 0.2% | | 8.4 | 31.6 | 39.4 | 5.4 | 17.9 | 8.5 | 103.5 | 448.0 |
| | 707-320C_FRT_JT3D-3B | 482.8 | | 79.6% | 8.4 | 31.0 | 39.2 | 5.4 | 17.9 | 8.5 | 78.8 | 358.4 |
| | 707-320C_FRT_JT3D-7 | 77.1 | | 12.7% | 8.6 | 29.4 | 37.7 | 5.4 | 17.7 | 8.2 | 11.6 | 58.9 |
| | 707-320C_AII_FRT_JT3D-3B | 30.1 | | 5.0% | 7.7 | 35.9 | 38.0 | 5.5 | 16.1 | 7.0 | 7.1 | 21.1 |
| | 707-320C_JT3D-3B | 16.8 | | 2.8% | 7.7 | 39.8 | 46.2 | 5.3 | 22.0 | 12.0 | 6.0 | 9.7 |
| Boeing | Boeing 727-100 | 1,093.9 | 0.3% | 4 <u>4</u> | 10.8 | 14.8 | 5.7 | 7.1 | 10.2 | 2.1 | 374.7 | 485.8 |
| | 727-100_JT8D-7B | 462.6 | | 42.3% | 10.7 | 14.9 | 5.7 | 7.1 | 10.0 | 2.0 | 165.5 | 201.8 |
| | 727-100F_FRT_JT8D-7B | 223.3 | | 20.4% | 10.8 | 14.7 | 6.0 | 7.1 | 10.6 | 2.3 | 69.8 | 95.5 |
| | 727-100QF_FRT_RB.183-651-54 | 199.2 | | 18.2% | 10.8 | 14.8 | 6.1 | 7.1 | 10.8 | 2.4 | 65.1 | 80.4 |
| | 727-100_JT8D-7 | 87.7 | | 8.0% | 10.7 | 15.3 | 5.5 | 7.0 | 11.1 | 2.5 | 41.6 | 33.8 |
| | 727-100C_JT8D-9 | 53.5 | | 4.9% | 11.3 | 15.0 | 5.0 | 7.2 | 8.4 | 1.6 | 15.6 | 34.7 |
| | 727-100C_CMB_JT8D-7B | 35.0 | | 3.2% | 10.9 | 13.9 | 5.7 | 7.2 | 9.1 | 1.5 | 7.2 | 21.9 |
| | 727-100_JT8D-9 | 14.8 | | 1.4% | 11.9 | 14.4 | 5.0 | 7.2 | 8.9 | 1.8 | 4.5 | 8.4 |
| | 727-100F_FRT_JT8D-9 | 10.5 | | 1.0% | 12.2 | 14.1 | 5.2 | 7.1 | 9.5 | 2.0 | 2.9 | 5.4 |
| | 727-100C_CMB_JT8D-7 | 7.2 | | 0.7% | 10.7 | 15.0 | 5.6 | 7.2 | 9.7 | 1.9 | 2.4 | 3.9 |

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| Appendix |

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| | | | % of | % of | 1-9 k | 1-9 km Altitude Band | Band | 9-131 | 9-13 km Altitude Band | Band | Fuel | Fuel |
|----------------|-----------------------|----------|--------|--------|-------|----------------------|------|-------|-----------------------|------|----------|-----------|
| | | Fuel | Global | Total | | | | | | | (1000 | (1000 |
| Generic OAG | OAG | (1000 | Fuel | within | Ξ | Ξ | Ē | ш | Ξ | ш | kg/day) | kg/day) |
| Type | Airplane/engine | kg/day) | Burned | Type | (NOX) | (CO) | (HC) | (NOX) | (CO) | (HC) | (1-9 km) | (9-13 km) |
| Boeing 727-200 | 27-200 | 14,333.8 | 4.1% | | 11.9 | 9.6 | 3.1 | 8.3 | 5.4 | 1.0 | 4,477.8 | 7,593.6 |
| | 727-200_JT8D-15 | 8,271.9 | | 57.7% | 12.0 | 10.9 | 3.7 | 8.0 | 5.8 | 1.1 | 2,676.0 | 4,289.2 |
| | 727-200_JT8D-9A | 2,451.8 | | 17.1% | 11.4 | 9.1 | 2.7 | 8.4 | 5.8 | 1.0 | 676.8 | 1,366.0 |
| | 727-200_JT8D-17R | 1,546.4 | | 10.8% | 12.6 | 4.0 | 0.6 | 9.5 | 2.5 | 0.7 | 486.2 | 886.9 |
| | 727-200_JT8D-9 | 526.5 | | 3.7% | 11.4 | 9.3 | 2.7 | 8.5 | 6.2 | 1.1 | 203.3 | 199.1 |
| | 727-200F_FRT_JT8D-9 | 521.4 | | 3.6% | 11.3 | 9.3 | 2.7 | 8.4 | 5.9 | 1.0 | 159.5 | 261.5 |
| | 727-200F_FRT_JT8D-15 | 287.8 | | 2.0% | 12.1 | 10.6 | 3.6 | 8.0 | 5.6 | 1.1 | 81.3 | 164.9 |
| | 727-200F_FRT_JT8D-7 | 272.9 | | 1.9% | 11.3 | 9.4 | 2.8 | 8.4 | 5.8 | 1.0 | 78.7 | 151.3 |
| | 727-200_JT8D-17 | 181.4 | | 1.3% | 11.7 | 9.0 | 3.5 | 7.9 | 5.6 | 1.5 | 49.2 | 103.1 |
| | 727-200F_FRT_JT8D-17R | 135.9 | | 0.9% | 12.8 | 3.4 | 0.5 | 10.1 | 2.1 | 0.6 | 36.4 | 76.3 |
| | 727-200_JT8D-7B | 102.7 | | 0.7% | 11.4 | 8.9 | 2.6 | 8.4 | 6.0 | 0.9 | 20.8 | 71.8 |
| | 727-200F_FRT_JT8D-17 | 35.1 | | 0.2% | 11.6 | 10.7 | 4.0 | 7.9 | 5.7 | 1.5 | 9.6 | 23.5 |

13.8 7.8 8.5 11.0 4.9 7.8 5.0 48.5 19.1 8.1 636.5 538.0 570.4 335.6 84.1 5,429.2 1,083.3 2,043.6 (9-13 km) kg/day) (1000 Fuel 8.0 11.6 8.5 2.7 5.1 3.4 2.0 0.8 18.9 5 i 254.6 60.7 47.3 12.5 1,581.4 445.5 322.7 567.8 906.7 4,262.4 (1-9 km) kg/day) (1000 Fuel 2.6 0.7 1.2 1.5 1.2 0.9 1.8 2.6 1.2 0.9 1.2 (HC) 1.2 1.3 1.2 1.9 0.7 2.4 0.8 0.8 2.4 ū 9-13 km Altitude Band 10.5 8.9 7.9 7.9 7.8 3.2 9.5 2.4 7.7 8.2 7.9 8.3 3.0 З.1 шÔ 2.9 9.0 6.8 7.8 9.1 ດ (XOX) 6.9 7.6 6.8 7.0 7.0 7.0 7.5 7.1 7.1 œ 6.8 7.1 7.6 6.8 7.4 7.5 7.1 6.9 7.1 7.1 Ö Ξ 3.2 2.6 4.2 0.8 6.2 4.0 3.5 4 4.3 3.4 4.7 (HC) 4.3 2.5 2.6 4.2 4.1 3.5 4.3 0.8 3.3 α Ξ 1-9 km Altitude Band 12.0 10.8 11.4 11.4 20.7 10.9 13.9 11.0 14.2 10.7 5.2 17.1 11.2 11.6 12.5 4.7 10.0 5.0 5.0 00 4.8 $\overline{\mathbf{m}}$ 10.9 10.3 11.9 11.5 11.8 œ 11.0 10.8 11.0 11.5 11.4 11.4 10.0 10.8 9.7 (XOX) 11.6 11.6 11.3 11.2 10.7 Ę Ē 0.1% 0.1% 13.0% 0.2% 0.2% 0.2% 0.1% 0.1% 0.0% 0.0% 37.7% 20.6% 5.8% 1.5% 0.9% 0.3% 0.3% 9.9% 9.1% within Total Type % of Burned Global Fuel 3.5% % of 1,108.6 12,222.7 2,513.9 1,583.0 1,210.1 4,610.4 185.2 107.3 kg/day) 703.4 39.6 27.2 23.0 22.1 15.3 12.3 11.3 11.1 31.7 (1000 4.7 2.5 Fuel 737-200QC_FRT_JT8D-15 737-200QC_FRT_JT8D-9A 737-200C_CMB_JT8D-9A 737-200C_QC_JT8D-15A 737-200C_CMB_JT8D-17 737-200C_QC_JT8D-17A 737-200C_QC_JT8D-15 737-200C_QC_JT8D-9 737-200C_JT8D-17A 737-200C_JT8D-17 737-200C_JT8D-9A 737-200C_JT8D-15 737-200_JT8D-17A 737-200_JT8D-15A 737-200_JT8D-9A 737-200_JT8D-15 737-200_JT8D-17 737-200_JT8D-9 737-200_JT8D-7 Airplane/engine Boeing 737-100/200 OAG Generic Type

| | | | % of | % of | 1-9 ki | 1-9 km Altitude Band | Band | 0-131 | 9-13 km Altitude Dend | Puod | . . | |
|----------|--|------------------|----------------|----------------|------------|----------------------|----------------|----------|-----------------------|-------------|----------------|------------------|
| | | Fuel | Global | Total | | | | 2 | | Dariu | ruel (1990) | Fue |
| Type | UAG Airplane/engine | (1000 kg/day) | Fuel Burned | within Tvpe | UN EI | ШĈ | ШÇ | Ē | Шġ | Ξ | kg/day) | (1000 kg/day) |
| | | | | | 14241 | | () | | (<u>0</u> 0) | (HC) | (1-9 km) | (9-13 km) |
| Boeing 7 | Boeing 737-300/400/500 | 30,764.9 | 8.9% | | 13.2 | 11.5 | 0.9 | 9.6 | 3.5 | 0.2 | 9,640.1 | 16,223.6 |
| | 737-300_CFM56-3B1 | 14,158.7 | | 46.0% | 13.3 | 12.3 | | 0 9 | 2 | c c | | |
| | /3/-400_CFM56-3C1 | 5,961.3 | | 19.4% | 13 F | + + + | | | | 0.0 | 4,394.7 | 7,574.4 |
| | 737-500_CFM56-3C1 | 3.442.2 | | 11 2% | 40.0 | | | 0.0 1 | 3.5 | 0.2 | 1,745.8 | 3,218.5 |
| | 737-500_CFM56-3B1 | 21775 | | 7 10/0 | 0 r 0 c | ν. ο | 9.0 | 9.4 | 3.7 | 0.1 | 1,272.4 | 1,546.1 |
| | 737-300_CFM56-3C1 | 2 160 2 | | 2 i | 12.7 | 9.8 | 0.6 | 9.4 | 3.6 | 0.1 | 721.1 | · |
| | 737-300 CFM56-3B2 | 1 000 1 | | 1.1% | 13.3 | 12.5 | . | 9.6 | 3.5 | 0.3 | 676.7 | 1 173 7 |
| | 737-400 CFM56-3B2 | 1.026,1 | | 0.2% | 13.4 | 12.0 | 1.0 | 9.6 | 3.3 | 0.2 | 565.6 | 1 084 9 |
| | 737-3000C 0C CEM56-3C1 | 0.076 0.07 | | 3.0% | 13.5 | 11.2 | 0.8 | 9.6 | 3.6 | 0.2 | 258.2 | 518.7 |
| | | 7:7 | | 0.0% | 13.4 | 12.2 | . . | 9.9 | 7.1 | 0.7 | 5.6 | 3.3 |
| Boeing 7 | Boeing 737-600/700/800 | 3,218.7 | 0.9% | | 16.3 | 6.4 | 6.0 | 11.8 | 1.8 | 0.3 | 818.2 | 2.032.0 |
| | 737-800_CFM56-7B26 | 1,323.3 | | 41.1% | 18.4 | 5.6 | 0 E | 107 | c T | 0 | | |
| | /3/-/00_CFM56-7B22 | 832.1 | | 25.9% | 15.3 | 6.9 | , 1 | 11 1 | 0. C | τ τ τ | 278.8 200 5 | 911.3 |
| | /3/-/U0_CFM56-/B24 | 812.6 | | 25.2% | 15.4 | 6.9 | | 110 | 5 C 1 C | , t C | 5.852 | 507.5 |
| | /3/-600_CFM56-7B20 737 800_CFM56-7D24 | 217.1 | | 6.7% | 14.4 | 6.9 | 1.1 | 10.7 | 3 F 7 1 | 0 C | 209.602 | 511.8 |
| | 101-000-0LIM30-1024 | 33.5 | | 1.0% | 18.6 | 6.1 | 0.8 | 12.2 | ר די | 0.0 | | 0.7 |
| | | | | | | | | | 2 | 2.2 | 4 0 | 20.07 |

| | | | % of | % of | 1-9 ki | 1-9 km Altitude Band | Band | 9-13 k | 9-13 km Altitude Band | Band | Fuel | Fuel |
|----------|---------------------------|----------|--------|--------|--------|----------------------|------|--------|-----------------------|------|----------|-----------|
| | | Fuel | Global | Total | | | | | | | (1000 | (1000 |
| Generic | OAG | (1000 | Fuel | within | Ξ | Ш | Ξ | Ξ | Ξ | Ξ | kq/dav) | ka/dav) |
| Type | Airplane/engine | kg/day) | Burned | Type | (NOX) | (co) | (HC) | (NOX) | (co) | (HC) | (1-9 km) | (9-13 km) |
| Boeing 7 | Boeing 747-100/200/300 | 30,638.2 | 8.8% | | 27.5 | 15.4 | 10.2 | 15.2 | 2.2 | + | 3.145.6 | 25 846 4 |
| | | | | | | | | | ! | | | 1.010.01 |
| | 747-200B_JT9D-7Q | 4,886.9 | | 16.0% | 23.6 | 14.7 | 7.1 | 12.7 | 0.7 | 0.7 | 406.5 | 29,978.8 |
| | 747-200SF_FRT_CF6-50E2 | 3,616.5 | | 11.8% | 27.2 | 14.6 | 10.2 | 16.1 | 1.7 | 1.5 | 351.6 | 21,530.8 |
| | 747-200F_FRT_CF6-50E2 | 3,061.5 | | 10.0% | 27.1 | 14.6 | 10.1 | 16.1 | 1.7 | 1.5 | 297.3 | 18,259.1 |
| | 747-200F_FRT_JT9D-7Q | 2,904.3 | | 9.5% | 30.3 | 14.4 | 10.1 | 17.7 | 2.3 | 0.2 | 363.8 | 16,670.6 |
| | 747-100F_FRT_JT9D-7A | 1,853.7 | | 6.1% | 26.6 | 15.3 | 10.0 | 15.2 | 0.6 | 0.8 | 254.5 | 10,340.6 |
| | 747-300_RB211-524D4 | 1,374.4 | | 4.5% | 31.4 | 24.4 | 22.5 | 15.8 | 8.3 | 2.6 | 132.4 | 8,262.5 |
| | 747-200B_CMB_CF6-50E2 | 1,293.0 | | 4.2% | 26.5 | 14.9 | 10.3 | 14.4 | 2.1 | 1.4 | 85.1 | 8, 144.4 |
| | 747-200B_CF6-50E2 | 1,047.3 | | 3.4% | 25.3 | 14.4 | 9.8 | 14.6 | 2.0 | 1.4 | 78.5 | 6,511.8 |
| | 747-300_JT9D-7R4G2 | 1,029.6 | | 3.4% | 26.9 | 3.5 | 0.5 | 14.8 | 1.3 | 0.3 | 94.0 | 6,267.7 |
| | 747-200B_JT9D-7J | 927.7 | | 3.0% | 28.1 | 20.2 | 13.7 | 16.1 | 3.1 | 0.6 | 120.9 | 5,308.3 |
| | 747-300_CF6-50E2 | 866.7 | | 2.8% | 27.3 | 14.5 | 10.1 | 14.9 | 1.9 | 1.4 | 60.1 | 5,430.1 |
| | 747-200F_FRT_JT9D-7J | 860.9 | | 2.8% | 30.2 | 14.8 | 10.4 | 17.7 | 2.4 | 0.3 | 113.2 | 4,879.7 |
| | 747-100_JT9D-7A | 722.9 | | 2.4% | 24.5 | 17.3 | 10.5 | 13.8 | 0.6 | 0.9 | 87.2 | 4,140.3 |
| | 747-200B_RB211-524D4 | 654.6 | | 2.1% | 31.0 | 24.6 | 22.9 | 15.0 | 9.2 | 2.8 | 57.5 | 3,963.4 |
| | 747-200F_FRT_RB211-524D4 | 641.0 | | 2.1% | 37.7 | 3.7 | 0.8 | 21.5 | 1.6 | 0.8 | 71.6 | 3,732.6 |
| | 747-300_CF6-80C2B1 | 600.0 | | 2.0% | 25.2 | 14.6 | 4.5 | 12.1 | 1.3 | 0.3 | 38.9 | 3,806.0 |
| | 747-200B_JT9D-7R4G2 | 534.8 | | 1.7% | 27.1 | 4.0 | 0.6 | 14.2 | 1.3 | 0.3 | 42.9 | 3,360.6 |
| | 747-200B_JT9D-7A | 443.4 | | 1.4% | 25.1 | 17.4 | 10.5 | 13.3 | 0.6 | 0.9 | 60.4 | 2,475.2 |
| | 747-100_JT9D-7 | 366.3 | | 1.2% | 25.1 | 15.1 | 9.2 | 13.3 | 0.4 | 0.7 | 33.6 | 2,219.4 |
| | 747-200SF_FRT_RB211-524D4 | 354.4 | | 1.2% | 32.8 | 21.2 | 19.3 | 18.0 | 6.3 | 2.0 | 37.5 | 2,096.2 |
| | 747-300_CMB_CF6-50E2 | 291.7 | | 1.0% | 26.2 | 16.4 | 11.1 | 14.7 | 2.1 | 1.6 | 30.1 | 1,734.3 |
| | 747-300_CMB_JT9D-7R4G2 | 249.4 | | 0.8% | 28.4 | 3.7 | 0.6 | 14.6 | 1.4 | 0.3 | 19.7 | 1,544.1 |
| | 747-SP_RB211-524D4 | 236.1 | | 0.8% | 28.2 | 24.6 | 21.1 | 15.2 | 9.3 | 3.1 | 22.7 | 1,086.4 |
| | 747-100B_SR_JT9D-7A | 199.8 | | 0.7% | 28.4 | 20.2 | 12.2 | 12.2 | 1.3 | 1.8 | 66.6 | 665.3 |
| | 747-200C_F_FRT_CF6-50E2 | 196.1 | | 0.6% | 26.9 | 15.5 | 10.7 | 15.8 | 1.9 | 1.6 | 22.1 | 1,132.2 |
| | 747-SP_JT9D-7F | 191.3 | | 0.6% | 25.1 | 29.9 | 20.7 | 15.6 | 3.8 | 1.6 | 28.7 | 629.7 |

| | | | % of | % of | 1-9 k | 1-9 km Altitude Band | Band | 6-13 | 9-13 km Altitude Band | Band | Fuel | Fuel |
|-----------------|------------------------------------|------------------|----------------|-------|-------|----------------------|-----------|-------|-----------------------|-----------|---------------------|----------------------|
| | | Fuel | Global | Total | í | i | i | i | i | i | (1000 | (1000 |
| Generic Type | OAG Airplane/engine | (1000 kg/day) | Fuel Burned | Type | (NOX) | ш () | HC) HC | (NOX) | ш () О | HC) HC | kg/day) (1-9 km) | kg/day) (9-13 km) |
| Boeina 7 | Boeina 747-100/200/300 (Continued) | | | | | | | | | | | |
| | | | | | | | | _ | | | | |
| | 747-200SF_FRT_JT9D-7J | 164.6 | | 0.5% | 30.2 | 14.8 | 10.4 | 17.4 | 2.4 | 0.3 | 21.1 | 938.6 |
| | 747-300_RB211-524C2 | 143.9 | | 0.5% | 33.7 | 4.8 | 0.8 | 18.4 | 2.0 | 0.9 | 32.1 | 651.7 |
| | 747-100B_RB211-524C2 | 131.5 | | 0.4% | 25.0 | 26.9 | 25.3 | 14.1 | 11.0 | 2.3 | 15.3 | 755.0 |
| | 747-200F_FRT_JT9D-7R4G2 | 127.1 | | 0.4% | 28.6 | 16.5 | 10.1 | 17.3 | 2.4 | 0.3 | 19.4 | 729.8 |
| | 747-SP_JT9D-7J | 109.7 | | 0.4% | 24.4 | 22.1 | 13.5 | 13.3 | 1.3 | 1.7 | 18.5 | 554.3 |
| | 747-SP_JT9D-7FW | 84.5 | | 0.3% | 25.9 | 29.3 | 20.3 | 16.2 | 2.8 | 0.6 | 6.6 | 476.3 |
| | 747-200B_CMB_CF6-50E | 84.0 | | 0.3% | 24.5 | 18.2 | 11.9 | 13.7 | 2.4 | 1.6 | 8.4 | |
| | 747-200B_JT9D-7Q3 | 82.7 | | 0.3% | 22.9 | 14.8 | 6.2 | 12.9 | 0.6 | 0.6 | 6.2 | |
| | 747-200B_CMB_JT9D-7Q | 72.8 | | 0.2% | 20.9 | 14.5 | 6.2 | 11.9 | 0.8 | 0.7 | 9.5 | |
| | 747-SR-100B_CF6-45A2 | 70.7 | | 0.2% | 24.1 | 12.9 | 10.1 | 14.2 | 2.8 | 1.6 | 5.5 | 436.5 |
| | 747-200C_QC_CF6-50E2 | 50.5 | | 0.2% | 26.6 | 14.2 | 9.9 | 14.6 | 2.0 | 1.4 | 3.1 | 320.8 |
| | 747-SP_JT9D-7A | 49.4 | | 0.2% | 24.2 | 22.8 | 13.9 | 13.8 | 4.1 | 4.4 | 9.3 | 104.8 |
| | 747-200B_JT9D-7F | 25.8 | | 0.1% | 27.0 | 21.9 | 13.8 | 16.2 | 2.6 | 0.5 | 3.5 | 150.5 |
| | 747-300_CMB_CF6-80C2B1 | 22.7 | | 0.1% | 20.4 | 20.2 | 6.3 | 11.5 | 2.1 | 0.5 | 3.0 | - |
| | 747-200B_JT9D-70A | 14.2 | | 0.0% | 22.0 | 26.3 | 13.7 | 13.2 | . - | 1.4 | 3.6 | 74.8 |
| Boeing | Boeing 747-400 | 59,837.4 | 17.2% | | 25.3 | 8.1 | 1.9 | 13.3 | 1.0 | 0.4 | 4,440.3 | 52,982.2 |
| | 747-400_CF6-80C2B1F | 20,215.2 | | 33.8% | 20.4 | 13.6 | 3.6 | 11.6 | 1.3 | 0.3 | 1,695.1 | 17,580.1 |
| | 747-400_PW4000-4056 | 15,590.5 | | 26.1% | 22.8 | 3.0 | 0.3 | 14.0 | 0.6 | 0.3 | 1,104.1 | 13,881.3 |
| | 747-400_RB211-524H2 | 11,341.7 | | 19.0% | 41.0 | 2.8 | 0.5 | 15.7 | 1.2 | 0.6 | 729.1 | 10,233.3 |
| - | 747-400_CMB_CF6-80C2B1F | 6,249.3 | | 10.4% | 21.0 | 13.7 | 3.7 | 11.6 | 1.3 | 0.3 | 446.8 | 5,566.3 |
| | 747-400_RB211-524G | 2,605.1 | | 4.4% | 39.2 | 2.9 | 0.5 | 15.1 | 0.9 | 0.6 | 150.5 | 2,371.8 |
| | 747-400F_FRT_PW4000-4056 | 1,428.0 | | 2.4% | 23.2 | 2.9 | 0.3 | 14.4 | 0.5 | 0.3 | 126.2 | 1,234.2 |
| | 747-400_CMB_PW4000-4056 | 1,234.9 | | 2.1% | 22.5 | 3.2 | 0.3 | 13.8 | 0.6 | 0.3 | 101.9 | 1,073.6 |
| | 747-400F_FRT_CF6-80C2B1F | 888.7 | | 1.5% | 20.0 | 1.5 | 0.2 | 13.1 | 0.5 | 0.1 | 62.5 | 794.3 |
| | 747-400F_FRT_RB211-524H2 | 284.0 | | 0.5% | 38.4 | 6.4 | 0.5 | 16.4 | 1.3 | 0.6 | 24.0 | 2473 |

| | | | ہر م | - <u>7</u> | 1-0 kn | 1-9 km Altitude Band | and | 9-13 ki | 9-13 km Altitude Band | Band | Fuel | Fuel |
|----------------|--|----------|---------|--|--------------|----------------------|----------|------------|-----------------------|----------------|---------------|------------|
| | | | IN % | 500 | | | - | • | | | /1000 | (1000 |
| | | Fuel | Global | Total | | i | ī | ī | ī | ū | ~ | ka/dav) |
| Generic | OAG | (1000 | Fuel | within | Ξ | ū | IJ | <u>п</u> ! | ΞÇ | | | (0 12 km) |
| | Airplane/engine | kg/day) | Burned | Type | (NOX) | (CO) | (HC) | (NOX) | (0) | (HC) | (II-9 KIII) (| (III) C1-A |
| | | | | | | | | | ļ | Ċ | | 10 010 7 |
| Boeing 757-200 | 57-200 | 19,716.7 | 5.7% | | 18.6 | 8.4 | 0.5 | 11.0 | 7.1 | 1.0 | 0,910.9 | 2.010.01 |
| | | 0 500 0 | | 73 2% | 17.3 | 6.7 | 0.6 | 12.1 | 1.6 | 0.1 | 1,850.0 | 5,841.9 |
| | 757-200_PW2000-2037 | 0.000.0 | | 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2 | 9.00 | 00 | 00 | 101 | 1.8 | 0.0 | 509.3 | 3,335.7 |
| | 757-200_RB211-535E4B | 4,1/1.6 | | 21.2% | 0.77 | 0 0 0 0 | , c | | - - | | 736.9 | 2.880.2 |
| | 757-200 RB211-535E4 | 4,054.2 | | 20.6% | 20.7 | 9.2 | 0.2 | 1.0.1 | p u |) , | | 748 5 |
| | 767.200 DW2000-2040 | 1.036.0 | | 5.3% | 18.1 | 7.2 | 0.6 | 12.1 | d.1 | 0.1 | 130.1 | 0.04 / |
| | 737-200_F W2000-2010 753 000 DD011 5350 | 960.9 | | 4.9% | 15.8 | 12.7 | 0.6 | 9.8 | 3.3 | 0.5 | 387.5 | 381.4 |
| | /5/-200_HDZ11-3330 | 0.000 | | 4 8% | 19.4 | 8.8 | 0.2 | 10.2 | 1.6 | 0.0 | 230.1 | 590.8 |
| | /5/-200PF_FH1_H5211-33354 | 275 | | 0.2% | 18.2 | 8.1 | 0.7 | 12.1 | 1.2 | 0.1 | 4.4 | 32.1 |
| | 757-200PF_FH1_FW2000-2040 | 5.50 | | 2 | | | | | | | | |
| Boeing 767-200 | 767-200 | 7,110.2 | 2.0% | | 22.6 | 6.6 | 1.6 | 11.1 | 2.0 | 0.3 | 959.5 | 5,693.3 |
| I | | 1 000 E | | 26 5% | 24.0 | 2.0 | 0.3 | 11.2 | 1.9 | 0.3 | 269.6 | 1,496.3 |
| | 767-200_J19D-/H4U | 0.000,1 | | 17 7% | 10.8 | 16.9 | 4.7 | 10.0 | 1.9 | 0.4 | 108.0 | 1,093.4 |
| | 767-200ER_CF6-80A | 0.002,1 | | 0/ 1.11 | | 2 2 2 2 | 4.8 | 10.0 | 1.8 | 0.4 | 71.8 | 723.8 |
| | 767-200ER_CF6-80C2B2 | 830.7 | | %_/.II | | 2 |) | 10.0 | 3.4 | 0.6 | 195.2 | 390.9 |
| | 767-200_CF6-80A | 678.8 | | 9.0% | 50.3 0 90 | ο ο τ | - C | 1 1 1 | | 0.3 | 49.6 | 491.9 |
| | 767-200EM_JT9D-7R4D | 566.7 | | 0.0.0 | | ה רי - ס | 6 C | 12.3 | 1.8 | 0.1 | 26.9 | 303.6 |
| | 767-200ER_PW4000-4056 | 330.1 | | 4.1./o | | 0.0 + 0 | 0 Q | 13.4 | 1.5 | 0.3 | 86.9 | 166.6 |
| | 767-200ER_JT9D-7R4E | 302.2 | | 4.0.4 | 101 | - 16.1 | 44 | 10.0 | 2.0 | 0.3 | 19.1 | 256.5 |
| | 767-200ER_CF6-80C2B4 | 1.682 | | 4.0.4 00.0 | a 66 | 3.7 | 80 | 11.4 | 1.7 | 0.4 | 51.1 | 189.2 |
| | 767-200ER_JT9D-7H4E4 | 7.002 | | | 27.2 27.2 | | 14 | 13.8 | 1.2 | 0.3 | 25.8 | 164.7 |
| | 767-200ERM_JT9D-7R4E | 0.791 | | %,0,7 | N | , u 107 | - c | 0.01 | 50 | 0.6 | 25.1 | 124.8 |
| | 767-200_CF6-80C2B2F | 164.9 | | 2.3% | - 1-0 | 0.0 | 4 C | 101 | | 0.6 | 8.9 | 111.0 |
| | 767-200EM_CF6-80A2 | 123.8 | | 1.7% | 7.72 | 4 1 4 1 | <u> </u> | | | 0.6 | 15.7 | 6.06 |
| | 767-200PC_FRT_CF6-80A | 114.8 | | 1.6% | 22.1 | ۲. ۲. | <u>-</u> | | | | - Y | 898 |
| | 767-200ER_CF6-80C2B4F | 98.5 | | 1.4% | 20.3 | 14.8 | 4.1 | 10.3 | 0. | | | |
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| r 1999 Aircraft |
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| 1999 |
| <u>9</u> |
| Indices |
| Emissions |
| Global |
| - Effective |
| Appendix D - |

| | | | 0/ 04 | 90 DF | | | | | | | | |
|----------------|---|----------|--------|---------|----------------|---------------------|-----------------------|-------------|-----------------------|----------|-------------|-----------|
| | | L. | | 5 | -9 KI | 1-9 km Airiude band | Band | 9-13 k | 9-13 km Altitude Band | Band | Fuel | Fuel |
| | 0.00 | Fuel | Global | Total | | | | - | | | (1000 | (1000 |
| Generic | UAG | (1000 | Fuel | within | Ξ | Ξ | ū | ⊡ | Ξ | Ц | ka/dav) | haldar) |
| l ype | Airplane/engine | kg/day) | Burned | Type | (NOX) | (co) | (HC) | (XON) | i () | (HC) | (1-9 km) | (9-13 km) |
| Boeing 767-300 | .67-300 | 22.152.7 | 6.4% | | 21.3 | 0 | 4 - | L | | | | |
| | | | 2 | | 2 | | 4. | C.21 | 1.2 | 0.3 | 3,207.2 | 17,470.8 |
| | 767-300ER_PW4000-4060 | 9,192.1 | | 41.5% | 21.5 | 96 | 60 | 1 0 1 | ۲ د | c c | | |
| | 767-300ER_CF6-80C2B6 | 4.240.2 | | 10 1% | 0.01 | | | | 0.7 | 0.U | 1,008.1 | 7,743.6 |
| | 767-300ER CF6-80C2R6F | 0 505 F | | 0/ 1.01 | יי יי יי | 4.01 | 4 2) | 10.6 | 1.7 | 0.3 | 384.1 | 3,664.0 |
| | 767-300 CF6-R0C2R2 | 1 770 0 | | %/11 | 9.71 | 4.0 | 0.5 | 12.5 | 1.1 | 0.1 | 253.8 | 2,222.6 |
| | 767-300EB DD011 501U0 | 1,13.3 | | ۵.U% | 19.4 | 5.9 | 4 | 13.3 | 3.1 | 0.8 | 667.0 | 810.1 |
| | 767-300FDF EDT CER 8000065 | 965.4 | | 4.4% | 35.6 | 8.5 | 0.6 | 14.9 | 1.7 | 0.7 | 200.5 | 666.5 |
| | | 009.8 | | 3.0% | 19.1 | 16.6 | 4.4 | 10.8 | 2.1 | 0.5 | 112.1 | 491 7 |
| | 767 2005 DF6 2005 1 805 2 805 | 603.5 | | 2.7% | 24.2 | 2.4 | 0.4 | 14.7 | 1.4 | 0.3 | 243.3 | 253.8 |
| | 707-300FH_CF0-8UCZB4 | 588.7 | | 2.7% | 18.2 | 15.1 | 4.1 | 10.5 | 2.1 | 0.4 | 823 | 465.4 |
| | 707-500 CF5 2000-4056 | 374.1 | | 1.7% | 21.6 | 3.8 | 0.3 | 13.2 | 0.7 | 03 | 44 7 | 308.3 |
| | /6/-300_CF6-80C2B2F | 363.1 | | 1.6% | 18.8 | 5.6 | 1.3 | 13.2 | 2.8 | 2.0 | 101 | 242 6 |
| | /6/-300EH_CF6-80C2B7F | 226.9 | | 1.0% | 17.8 | 5.6 | 0.5 | 12.4 | 1.2 | - C | 1.101 | 0.012 |
| | /6/-300EH_CF6-80C2B2 | 224.0 | | 1.0% | 18.7 | 17.4 | 5.0 | 10.7 | 17 | | 2 I C | 4.00.4 |
| | /67-300ER_PW4000-4062 | 100.6 | | 0.5% | 22.0 | 3.7 | 0.3 | 13.0 | 2.0 | | | 0.00 |
| | 767-300ER_RB211-524H2 | 89.0 | | 0.4% | 33.8 | 10.2 | 0.6 | 14.9 | 0 | 2 0 | 7.01 200 | 04./ |
| | 767-300_PW4000-4056 | 52.7 | | 0.2% | 21.8 | 7 0 | α | | - c | | 20.3 | 04.0 |
| | 767-300_CF6-80C2B4F | 52.1 | | 7000 | 010 | 2.4 | - | 0.01 | 4.0 4. | 0.0 0 | 13.9 | 30.9 |
| | 767-300ERF FRT CF6-80C2R7F | AF O | | ° 4.0 | 2 1.4 | 0.9 | 1./ | 13.1 | 3.1 | 0.8 | 12.3 | 32.9 |
| | | 0.07 | | 0.2% | 19.7 | 16.3 | 4.3 | 10.8 | 1.8 | 0.4 | 5.6 | 36.4 |
| Boeing 777-200 | 77-200 | 11,260.1 | 3.2% | | 25.2 | 5.4 | 6.0 | 16.8 | 0.6 | 0.3 | 1 416 7 | 0 440 0 |
| | 777-200ER_PW4000-4090 | 3,183.9 | | 28.3% | 26.7 | ц Ц | | 0 1 | Ċ | | | 2.1 |
| | 777-200ER_GE90-92B | 26766 | | 22 00/ | |) • | | 0.01 | 0.0 | 0.2 | 306.7 | 2,766.0 |
| | 777-200EB Trent-892 | 0.010 6 | | 0/ 0.07 | 20.9 | | 0.2 | 20.3 | 0.8 | 0.1 | 320.2 | 2,209.3 |
| | 777-200FR GEQ0.85R | 2,010,0 | | 17.9% | 21.4 | 8.4 | 24.0 | 13.4 | 0.7 | 0.4 | 178.3 | 1,758.3 |
| | 777-200 DM4000 4074 | 1,392.7 | | 12.4% | 26.4 | 4.2 | 0.2 | 19.4 | 0.7 | 0.1 | 127.5 | 1.211.8 |
| | 777 200ED Troot 884 | 5/2/ | | 6.0% | 23.1 | 3.5 | 0.6 | 16.1 | 0.6 | 0.2 | 247.6 | 328.7 |
| | 777-200 Trant 075 | 642.0 | | 5.7% | 21.0 | 8.9 | 25.4 | 13.3 | 0.8 | 0.8 | 72.8 | 533.7 |
| | | 352.0 | | 3.1% | 21.0 | 9.9 | 28.6 | 13.4 | 1.3 | 1.6 | 66.5 | 251.6 |
| | / / 0+-000+14 J_00-1 / / | 321.6 | | 2.9% | 24.6 | 4.0 | 0.7 | 16.2 | 0.7 | 0.3 | 97.0 | 184 6 |
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| 999 Aircraft |
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| s for 19 |
| ndice |
| Emissions |
| e Global E |
| Effective |
| Appendix D - |

| | | | 40 % | %, nf | 1-0 km | 1-9 km Altitude Band | and | 9-13 kr | 9-13 km Altitude Band | Band | Fuel | Fuel |
|---------------|--|--------------------|--------|--------|--------|----------------------|------|---------|-----------------------|------|----------|-----------|
| | | - (; L | | | | | 5 | | | | (1000 | (1000 |
| | | 1000 | Firel | within | Ξ | Ũ | Ξ | Ш | Ш | Ξ | kg/day) | kg/day) |
| Generic | UAG Aimisme/ennine | ka/dav) | Burned | Type | (NOX) | (co) | (HC) | (NOX) | (co) | (HC) | (1-9 km) | (9-13 km) |
| adki | | 11-6- | | | | | | | | | _ | |
| Boeing | Boeing 777-300 | 1,131.0 | 0.3% | | 24.8 | 4.4 | 10.3 | 15.7 | 0.8 | 0.5 | 264.3 | 756.3 |
| | | 767 1 | | 67 8% | 24.8 | 6.8 | 23.6 | 15.3 | 0.8 | 0.7 | 115.9 | 597.8 |
| | 777-300_1rent-892 777-300_PW4000-4090 | 363.9 | | 32.2% | 24.7 | 2.5 | 0.0 | 17.2 | 6.0 | 0.0 | 148.4 | 158.5 |
| Concorde | ę | 351.2 | 0.1% | | 11.0 | 18.5 | 1.3 | 10.0 | 26.1 | 1.8 | 45.4 | 18.1 |
| | concorde | 351.2 | | 100% | 11.0 | 18.5 | 1.3 | 10.0 | 26.1 | 1.8 | 45.4 | 18.1 |
| | 000000 | | | | | | | | | | | |
| DC-10 | | 12,679.4 | 3.6% | | 24.2 | 7.5 | 2.8 | 14.9 | 2.0 | 6.0 | 1,558.1 | 10,454.0 |
| | | A 477 6 | | 35.3% | 24.6 | 10.2 | 4,1 | 12.9 | 2.7 | 1.3 | 382.4 | 3,899.4 |
| - | DC-10-30_CF6-50C2 | 4,477.0 0.007.0 | | 20.3% | 23.0 | 5.8 | 6. | 14.6 | 0.2 | 0.4 | 355.8 | 2,324.7 |
| | | 1 302 1 | | 10.3% | 29.4 | 7.0 | 2.6 | 20.5 | 2.2 | 0.7 | 160.0 | 1,070.2 |
| , | | RQ6.6 | | 7.1% | 23.4 | 10.5 | 4.2 | 13.0 | 3.3 | 1.4 | 104.7 | 740.7 |
| | | 745.9 | | 5.9% | 28.4 | 6.8 | 2.5 | 21.0 | 2.0 | 0.6 | 132.9 | 559.5 |
| | | 610.7 | | 4.8% | 17.3 | 4.0 | 1.0 | 12.0 | 0.7 | 0.4 | 120.5 | |
| | | 607.7 | | 4.8% | 28.9 | 8.6 | 3.1 | 20.1 | 2.4 | 0.8 | 100.8 | |
| | | 5915 | | 4.7% | 19.6 | 4.8 | 2.2 | 15.1 | 1.8 | 1.1 | 139.7 | |
| | | 507 5 | | 4.0% | 24.7 | 11.1 | 4.4 | 12.5 | 3.0 | 1.4 | 53.7 | 4 |
| | | 95.8 | | 0.8% | 25.2 | 9.4 | 3.8 | 13.0 | 2.6 | 1.3 | 6.5 | |
| | DC-10-30_CT 0-30021 | 16.8 | | 0.1% | 25.2 | 9.3 | 3.8 | 13.0 | 2.6 | 1.2 | | 15.1 |
| | UC-10-30_CF0-3001 | 2.2. | | | | | | | | | | |

| | | | % of | % of | 1-9 k | 1-9 km Altitude Band | Band | 0-12 | 0.12 km Altitude Dana | | | |
|------------|-------------------------|----------------|--------|-----------|---------------|----------------------|------------|-------|-----------------------|-----------|------------|-----------|
| | | Fuel | Global | Total | | | 5 | | אווי אווומספ | Dalla | Fuel | Fuel |
| Generic | OAG | (1000 | Fuel | within | Ē | ũ | ũ | ū | ū | ī | (1000 | (1000 |
| Type | Airplane/engine | kg/day) | Burned | Type | (NOX) | ; () () | (HC) | (NOX) | ы (ОО) | н Э (Э | (1-0 km) | kg/day) |
| | | | | | | | | | 1221 | 1011 | (1114 2-1) | (9-13 Km) |
| 8-00 00 | | 2,882.7 | 0.8% | | 11.2 | 16.3 | 11.2 | 8.6 | 7.2 | 1.4 | 645.0 | 1,962.5 |
| | DC-8-71F_FRT_CFM56-2C1 | 1,111.6 | | 38.6% | 12.9 | 8.4 | 0.5 | 10.0 | 00 | Ċ | | |
| | DC-8-63_FRT_JT3D-7 | 589.6 | | 20.5% | 82 | 32.0 | 28.6 | 10.5 | 0.7 | 2 C | 244.6 | 774.7 |
| | DC-8-73CF_FRT_CFM56-2C1 | 563 1 | | 10 50/ | 107 | 05.0 | 0.07 | 2.0 | 14.0 | 2.2 | 136.5 | 386.2 |
| | DC-8-73F FRT CFM56-2C1 | 188.0 | | %C.81 | 13.0 | 80 i N | 0.5 | 10.1 | 3.2 | 0.2 | 139.8 | 366.2 |
| | | 100.4 | | 0.0% | 13.3 | 7.3 | 0.4 | 10.3 | 2.4 | 0.2 | 28.1 | 149.5 |
| | | 142.1 | | 4.9% | 9.1 | 26.0 | 33.1 | 5.8 | 14.6 | 6.8 | 34.5 | 91.4 |
| | | 134.0 0 - 0 | | 4.7% | 7.5 | 30.9 | 33.9 | 5.0 | 23.3 | 7.0 | 35.8 | 80.2 |
| | DC-8-6205 EBT 1730 20 | 97.8 | | 3.4% | 8.3 | 30.4 | 27.0 | 5.7 | 13.1 | 1.8 | 18.3 | 71 0 |
| | | 54.9 | | 1.9% | 8.1 | 27.7 | 32.7 | 5.2 | 20.5 | 6.0 | 7.3 | 43.4 |
| 6-0Q | | 9,130.1 | 2.6% | | 11.0 | 11.8 | 4.2 | 7.6 | 6.7 | 1.0 | 3,910.8 | 3.619.6 |
| | DC-9-31_JT8D-7B | 2.496.5 | | 702 20 | 10.6 | с с т | | I | 1 | | | |
| | DC-9-32_JT8D-9A | 1 678 0 | | 10 10/ | 0.0 | 0.01 | 0.0 | 1.4 | 7.9 | 0.9 | 1,071.2 | 956.2 |
| | DC-9-31_JT8D-9A | 1 272 3 | | 12 00/ | | <u></u> | 4./ | 7.4 | 7.4 | | 655.6 | 759.6 |
| | DC-9-51_JT8D-17 | 1 080 7 | | 11 00/ | ה ה ה ה | 1.7 | 4 | 7.7 | 2.1 | 0.4 | 602.0 | 402.1 |
| | DC-9-41_FRT JT8D-11 | 557 0 | | 0/0.11 | | 9.9 | 4.0 | 8.1 | 5.8 | 1.6 | 492.9 | 356.7 |
| | DC-9-15 JT8D-7A | 8.100 BAAR | | 0.1% | 12.8 | 12.4 | 4.3 | 8.3 | 6.5 | 0.9 | 214.3 | 261.0 |
| | DC-9-41_JT8D-11 | 325.2 | | 4.2% | 4.04 | 16.5 | 6.1 | 7.4 | 7.8 | 0.9 | 157.6 | 191.8 |
| | DC-9-32_JT8D-7A | 249.8 | | 0.0.0 | 0.01 | 6.[[| 4 i | 8 | 6.7 | 0.9 | 142.4 | 121.7 |
| | DC-9-32_JT8D-7B | 247.9 | | 0/ 1·3 | 2.01 | 0.41 | 5.0 1 | 7.4 | 8.0 | 1.0 | 102.9 | 111.2 |
| | DC-9-32_JT8D-17 | 208.0 | | % / · · · | 0.0 | 0.0 | טיט איס | 7.4 | 7.9 | 6.0 | 108.8 | 96.8 |
| | DC-9-31_JT8D-7A | 173.1 | | | 4 C 7 d | 4 C | 0. G | 1.1 | 7.3 | 1.8 | 94.0 | 95.2 |
| | DC-9-51_JT8D-17A | 153.0 | | 0/ 2.1 | | 0.2 Z | 4.8 | 7.4 | 7.8 | 6.0 | 52.3 | 97.3 |
| | DC-9-41 JT8D-15 | 68.4 68.4 | | 0.79/ | 0.7 1 2 | 8 [.] | 2.8 | 8.6 | 2.4 | 0.6 | 76.7 | 42.7 |
| | DC-9-21_JT8D-11 | 67.6 | | 0.1% | / 2 | c.11 | 6 0 | 8.2 | 5.4 | 0.9 | 23.8 | 34.8 |
| | DC-9-15_JT8D-7 | 48.4 | | 0.1% | 0.0 0 | 13.4 | 5.4 | 7.2 | 7.4 | 1.3 | 26.3 | 30.6 |
| | DC-9-32_JT8D-11 | 41.2 | | 0.5% | 0.0 0.0 | 15.6 15.6 | \. | 4.7 | 8. Z | 1.0 | 27.8 | 17.8 |
| | DC-9-32_JT8D-9 | 34.7 | | 2/010 | 0.0 a 01 | | 1 1 | N 1 | 4. | 1.0 | 26.5 | 10.2 |
| | | | | 0/ + '> | 0.0 | 13.0 | 4./ | 7.5 | 7.5 | 1.2 | 17.0 | 10.1 |

| | | | % of | % of | 1-9 ki | 1-9 km Altitude Band | Band | 9-131 | 9-13 km Altitude Band | Band | Fuel | Fuel |
|------------------|----------------------------|---------|--------|----------|--------|----------------------|------|-------|-----------------------|-----------------|--------------|-----------|
| | | Fuel | Global | Total | | | | | | | (1000 | (1000 |
| Generic C | OAG | (1000 | Fuel | within | Ē | Ш | Ū | Ξ | Ξ | Ξ | kg/day) | kg/day) |
| | Airplane/engine | kg/day) | Burned | Type | (XON) | (CO) | (HC) | (XON) | (co) | (HC) | (1-9 km) | (9-13 km) |
| DC-9 (Continued) | tinued) | | | | | | | | | | | |
| | DC-9-31CF .IT8D-17 | 24.1 | | 0.3% | 8.8 | 15.8 | 5.7 | 7.2 | 6.9 | 1.7 | 8.6 | 14.6 |
| | DC-9-15RC FRT JT8D-7B | 11.4 | | 0.1% | 9.8 | 15.8 | 5.9 | 7.4 | 8.1 | 1.0 | 5.3 | |
| , <u> </u> | DC-9-33CF_JT8D-9A | 11.3 | | 0.1% | 10.7 | 12.7 | 4.5 | 7.4 | 7.6 | 1.2 | 4.7 | |
| Fokker 100 | | 3,444.1 | 1.0% | | 11.1 | 21.0 | 2.0 | 6.4 | 7.0 | 1.0 | 1,319.4 | 1,413.6 |
| - | 100-* BB_183-650-15 | 3,062.2 | | 88.9% | 10.8 | 21.7 | 1.9 | 6.2 | 7.3 | 1.0 | 1,170.2 | ÷ |
| - | 100-*_RB.183-620-15 | 381.8 | | 11.1% | 13.3 | 14.9 | 2.0 | 8.2 | 4.2 | 1.2 | 149.3 | 140.2 |
| Fokker 28 | | 1,210.7 | 0.3% | <u>,</u> | 10.5 | 13.5 | 7.8 | 7.4 | 7.2 | 2.7 | 601.0 | 362.1 |
| - | F.28-4000 Spev-555-15P | 994.7 | | 82.2% | 10.5 | 13.6 | 7.9 | 7.4 | 7.1 | 2.6 | 481.1 | 6) |
| | F 28-1000 Spev-555-15 | 110.8 | | 9.2% | 10.4 | 14.3 | 8.6 | 7.5 | 7.5 | 2.8 | 63.4 | |
| | F 28-3000 Spev-555-15H | 51.1 | | 4.2% | 10.4 | 12.4 | 6.8 | 7.5 | 6.8 | 2.6 | 24.6 | - |
| | F 28-2000 Spev-555-15 | 40.9 | | 3.4% | 10.6 | 12.0 | 5.2 | 7.7 | 8.4 | 3.3 | 24.9 | |
| | F.28-4000_Spey-555-15H | 13.2 | | 1.1% | 10.6 | 13.3 | 7.0 | 7.4 | 7.5 | 2.7 | 7.0 | 1.4 |
| Fokker 70 | | 452.5 | 0.1% | | 10.3 | 5.3 | 1.2 | 7.1 | 2.7 | 1.0 | 202.2 | 153.4 |
| - | 70-*_RB 183-620-15 | 452.5 | | 100.0% | 10.3 | 5.3 | 1.2 | 7.1 | 2.7 | 1.0 | 202.2 | 153.4 |
| Lockheed L-1011 | L-1011 | 2,415.5 | 0.7% | | 18.7 | 19.4 | 13.6 | 14.4 | 0.6 | 2.2 | 518.3 | 3 1,676.1 |
| | 1-1011-1 RB211-22R | 1.689.9 | | 70.0% | 18.3 | 18.6 | 13.7 | 14.7 | 6.8 | 1.8 | 409.1 | 1,115.8 |
| | L 1011-500 BB211-524B4 | 463.9 | | 19.2% | 20.5 | 24.9 | 13.0 | 12.8 | 17.4 | 3.8 | 67.5 | (7) |
| | 1-1011-200 FRT RB211-524B | 121.8 | | 5.0% | 20.8 | 17.8 | 14.2 | 15.3 | 6.0 | 1.4 | 20.8 | |
| | L-1011-50 RB211-22B | 108.7 | | 4.5% | 19.6 | 17.4 | 13.3 | 14.7 | 6.5 | 1.6 | 14.6 | |
| | L-1011-200 FRT RB211-524B4 | 23.7 | | 1.0% | 20.5 | 19.0 | 15.2 | 14.6 | 7.0 | 1 .9 | 5.3 | - |
| _ | 1 11 Diank Diank | 7.5 | | 0.3% | 21.6 | 18.0 | 14.4 | 14.8 | 6.5 | 1.6 | - | 0.9 6.0 |

| 1999 Aircraft |
|---------------|
| for |
| Indices |
| Emissions |
| Global |
| ffective |
| |
| Appendi |

| | | | % of | % of | 1-9 k | 1-9 km Altitude Band | Band | 9-13 4 | 9-13 km Altitude Band | Band | Fuel | |
|---------|---------------------------------|----------------|--------|--------|-------|----------------------|---------|--------|-----------------------|----------|----------|-----------|
| | | Fuel | Global | Total | | | | | | 5 | 1000 | |
| Generic | OAG | (1000 | Fuel | within | Ū | Ξ | Ξ | Ξ | Ξ | ū | ka/dav) | |
| Type | Airplane/engine | kg/day) | Burned | Type | (XOX) | (co) | (HC) | (NOX) | (CO) | (HC) | (1-9 km) | (9-13 km) |
| MD-11 | | 11,951.7 | 3.4% | | 19.0 | 5.9 | 0.5 | 12.9 | 1.2 | 0.1 | 1,003.6 | 10,448.6 |
| | MD-11-Passenger CF6-80C2D1F | A 268 A | | 26 70/ | | | | | | | | |
| | MD-11-Frainhter EDT CE 800001F | 1.003,1 | | %./.Co | 10.9 | 4.1 | 0.4 | 12.7 | 1.0 | 0.1 | 346.8 | 3,757.6 |
| | | 2,941.4 | | 24.6% | 17.5 | 5.0 | 0.5 | 13.6 | 0.8 | 0.1 | 278.5 | 2.515.7 |
| | MU-11-Passenger_PW4000-4460 | 2,293.2 | | 19.2% | 20.2 | 8.9 | 0.8 | 12.4 | 1.8 | 0.2 | 195.8 | 1 994 1 |
| | MD-11-Passenger_PW4000-4462 | 1,621.5 | | 13.6% | 20.4 | 8.3 | 0.7 | 12.5 | 1.8 | 0.2 | 120.5 | 1 446 5 |
| | MU-11-Combi_CMB_CF6-80C2D1F | 450.3 | | 3.8% | 17.4 | 3.9 | 0.4 | 12.8 | 1.0 | 0.1 | 28.6 | 409.6 |
| | MD-11-Freighter_FRT_PW4000-4460 | 310.5 | | 2.6% | 22.0 | 9.1 | 1.6 | 14.3 | | 5 | 28.1 | 266.7 |
| | MD-11-CF_QC_PW4000-4462 | 33.2 | | 0.3% | 20.8 | 8.0 | 0.7 | 12.4 | 1.7 | 0.1 | | 30.3 |
| | MD-11-CF_QC_PW4000-4460 | 33.0 | | 0.3% | 19.3 | 8.5 | 0.7 | 12.0 | 2.0 | 0.2 | 3.3 | 28.0 |
| | | | | | | | | | | | | |
| 08-0W | | 22,366.8 | 6.4% | | 16.0 | 4.2 | 1.2 | 10.6 | 4.4 | 1.6 | 6,712.7 | 12,352.9 |
| | MD-80-82_JT8D-217C | 8,751.6 | | 39.1% | 16.4 | 4 () | + + | 10.7 | с Т | ų T | | |
| | MD-80-83_JT8D-219 | 5,047.2 | | 22.6% | 15.6 | 4 2 | - r | 10.5 |) (t = | 0 U | 2,301.0 | 5,213.2 |
| | MD-80-88_JT8D-219 | 3,736.1 | | 16.7% | 15.4 | 1 6 |) (r. | 10.6 | , 4 0 0 | 0 u | 1.286,1 | 2./80.5 |
| | MD-80-82_JT8D-217A | 1,894.9 | | 8.5% | 16.4 | 4 1 | ; - | 0.0 | 0 = t = | 0. 4 | 1,348.8 | 1,84/.1 |
| | MD-80-81_JT8D-217C | 932.0 | | 4.2% | 16.4 | 4.1 | - Ci | 10.7 | 4 1 9 | 0 C | 3725 | 334 0 |
| | MD-80-87_JT8D-217C | 777.5 | | 3.5% | 15.6 | 4.5 | 1.3 | 9.7 | 5.2 | 6 | 2317 | 404.8 |
| | MD-80-81_JT8D-217 | 664.2 | | 3.0% | 16.4 | 4.0 | 1.1 | 10.6 | 4.5 | 1.6 | 200.3 | 351.2 |
| | MD-80-82_J18D-217 | 354.1 | | 1.6% | 16.3 | 4.1 | 1.2 | 10.6 | 4.4 | 1.6 | 89.7 | 217.1 |
| | MD-80-87_J18D-219 | 173.4 | | 0.8% | 15.3 | 4.9 | 1.4 | 9.8 | 5.0 | 6.1 | 54.4 | 94.5 |
| | MU-80-83_J18D-217C | 36.0 | | 0.2% | 14.4 | 4.1 | 1.3 | 10.4 | 4.5 | 1.7 | 18.8 | 7.6 |
| 06-OM | | 1,242.9 | 0.4% | | 16.4 | 5.2 | 0.1 | 11.9 | 1.8 | 10 | 510.4 | 543.0 |
| | MD-00-30 //2600 2626 DE | | | | | | | | ! | ; | | 1010 |
| | MD-60-30_V2000-2323-U3 | 637.5 887.9 | | 51.3% | 16.4 | 4.9 | 0.1 | 11.8 | 1.9 | 0.1 | 272.7 | 243.3 |
| | CU-02C2-00C2A_00-00-014 | 5.000 | | 48.7% | 16.5 | 5.6 | 0.1 | 11.9 | 1.8 | 0.1 | 237.7 | 299.8 |

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| | | | % of | % of | 1-9 kn | 1-9 km Altitude Band | Band | 9-13 k | 9-13 km Altitude Band | Band | Fuel | Fuel |
|--|-------------------------------------|---------|--------|--------|--------|----------------------|------|--------|-----------------------|------|----------|----------------|
| <u>. </u> | | Find | Global | Total | | | | | | | (1000 | (1000 |
| | | (1000 | Fuel | within | Ξ | Ξ | ū | Ξ | Ξ | Ū | kg/day) | kg/day) |
| Trime Aimls | OAG Airolane/engine | ka/dav) | Burned | Type | (XON) | (CO) | (HC) | (XON) | (co) | (HC) | (1-9 km) | (9-13 km) |
| edk - | | 6 | | | | | | | | | | |
| Miscellaneous | neous | 5.4 | %0.0 | | 8.6 | 15.8 | 2.3 | 7.3 | 0.8 | 0.2 | 2.3 | 2.3 |
| | DEI Blank-Blank | 3.8 | | 70.3% | 8.5 | 16.0 | 2.2 | 7.3 | 0.7 | 0.2 | 1.6 | 1.7 |
| | LRJ_Blank-Blank | 1.6 | | 29.7% | 8.9 | 15.3 | 2.4 | 7.3 | 1.2 | 0.2 | 0.7 | 0.6 |
| Regional Jets | al Jets | 4,479.0 | 1.3% | | 11.6 | 9.4 | 1.4 | 9.1 | 0.6 | 0.1 | 1,907.1 | 1,663.8 |
| | CD 1 100ED CE31.381 | 1 693 0 | | 37.8% | 8.7 | 13.4 | 2.0 | 7.3 | 0.7 | 0.2 | 724.3 | 639.7 |
| | | 905 9 | | 20.2% | 18.0 | 1.0 | 0.0 | 12.8 | 0.5 | 0.0 | 381.4 | 314.6 |
| | RJ-RJOJ_LTJU/-IF EMI Block Block | 5613 | | 12.5% | 8.7 | 13.0 | 2.0 | 7.3 | 0.6 | 0.2 | 238.8 | •• |
| | | 351.7 | | 7.9% | 17.8 | 1.0 | 0.0 | 13.9 | 0.4 | 0.0 | 163.9 | |
| | | 266.5 | | 6.0% | 8.8 | 13.8 | 2.1 | 7.3 | 0.7 | 0.2 | 102.6 | - |
| | | 216.9 | | 4.8% | 8.7 | 13.3 | 2.1 | 7.3 | 0.6 | 0.2 | 85.2 | 91.5 |
| | B.I.B.170 F507-1F | 149.2 | | 3.3% | 18.7 | 1.0 | 0.0 | 12.8 | 0.5 | 0.0 | 55.7 | |
| | | 144.9 | | 3.2% | 8.6 | 11.5 | 1.8 | 7.3 | 0.7 | 0.2 | 82.6 | |
| | | 92.9 | | 2.1% | 8.8 | 14.4 | 2.2 | 7.3 | 0.8 | 0.2 | 35.7 | |
| | | 65.0 | | 1.5% | 8.7 | 12.8 | 1.9 | 7.3 | 0.4 | 0.2 | 23.4 | ^(N) |
| | ER.1-145-EP AF-A1 1 | 24.1 | | 0.5% | 8.7 | 13.0 | 2.0 | 7.3 | 0.5 | 0.2 | 10.0 | |
| | EB.1-145-LB AE-A1 | 7.6 | | 0.2% | 8.6 | 12.3 | 1.9 | 7.3 | 0.7 | 0.2 | 3.6 | 2.5 |
| | | | | | | | | | | | | |

| | | | % of | % of | 1-9 k | 1-9 km Altitude Band | Band | 0.121 | Altitude | | | |
|---------|---------------------------|---------------|--------|---------|------------|----------------------|------------|-------|----------|------------|-------------|-----------|
| | | Fuel | Global | Total | | 5 | | 2 | | Dariu | Luel | Fuel |
| Generic | 04G | | | | | | | | | | (1000 | (1000 |
| Time I | | 0001) | Fuel | within | ū | Ξ | Ξ | Ξ | Ξ | Ш | ka/dav) | (veb/od |
| adkı | Airplarle/engine | kg/day) | Burned | Type | (NOX) | (CO) | (HC) | (NOX) | (co) | (HC) | (1-9 km) | (9-13 km) |
| 1 | ; | | | | | | | | | | | |
| Hussian | Russian Aircraft | 7,138.3 | 2.1% | | 12.3 | 15.5 | 9.0 | 9.2 | 8.4 | 1.5 | 1,351.6 | 5,045.7 |
| | Tu-154-B NK-8-2U | 1 954 E | | /07 /0/ | 0 | 0 | 1 | | | _ | | |
| | II-62-M D-30-KII | | | 21.4% | 2.21 | 9.6 | 9.9 9.9 | 8.2 | 5.2 | 0.0 | 385.7 | 1.353.8 |
| • | | 1,404.5 | | 19.7% | 15.5 | 7.8 | 2.3 | 9.5 | 4.8 | 0.8 | 139.4 | 1 204 8 |
| | 14-134-101_U-30-NU-134-11 | 1,008.6 | | 14.1% | 12.2 | 9.8 | 3.3 | 8.0 | 5.5 | 1.0 | 2241 | 657 4 |
| | 00-VN -00-II | 653.5 | | 9.2% | 19.5 | 30.6 | 26.4 | 14.3 | 13.3 | 50 | 105.0 | |
| | lu-134-A_D-30-3 | 534.5 | | 7.5% | 10.7 | 12.3 | 4.7 | 74 | 2.2. | | 0.001 1 | 2.044 |
| | II-76-T_FRT_D-30-KP-2 | 374.7 | | 5.2% | 15.2 | 9.2 | 27 | 7 8 | - 4 | | 0.761 | 0.115 |
| | II-96-300_PS-90-A | 240.4 | | 3.4% | 21.3 | 14.5 | 11.3 | 15.5 | - a | יים סיד | 00.4 0 | 287.7 |
| | Yak-40-*_Al-25 | 147.5 | | 2.1% | 5.7 | 37.1 | 29.1 | 4.0 | 46.7 | 104 | 21.0 | |
| | 1u-134-A_D-30-2 | 143.2 | | 2.0% | 10.7 | 12.4 | 4.8 | 7.4 | 7.8 | | | 1.00 |
| | Yak-42-*_D-36 | 124.3 | | 1.7% | 5.7 | 36.3 | 28.1 | 4 0 | 46.0 | ο α | | 0.00 |
| | Yak-40-*_AI-25-Blank | 92.7 | | 1.3% | 57 | 40 F | 30.3 | | | - 7 | 0.10 | 97.0 |
| | Yak-42-D_D-36 | 92.0 | | 1 3% | 56 | а. 26 г. | | | 40.4 | L.01 | 38.6 | 26.5 |
| | Yak-42-D_D-36 | 92.0 | | 1 3% | о и о и | 20.00 | t.07 | | 44.0 | 0.0 8 | 24.7 | 46.6 |
| | Yak-42-*_D-36-Blank | GR 7 | | 200 F | 5 r 5 u | 0.00 | 20.4 | 4 | 44.5 | 8.0 | 24.7 | 46.6 |
| _ | II-62-* NK-8-4 | 67.4 | | %.O. | | 30.0 | 27.8 | 4.1 | 43.8 | 7.0 | 14.8 | 42.5 |
| | An-124-* FRT D-18-T | 4. 70 4. 0 | | 0.9% | 5.01 | 8.7 | 2.6 | 8.8 | 5.5 | 0.8 | 9.0 | 54.4 |
| | IL-RG-* NK-RG-RISH | 2.80 | | 0.8% | 22.5 | 4.9 | 1.2 | 11.5 | 1.0 | 0.2 | 6.1 | 49.4 |
| | TII-134-B D-30-2 | 48.9 | | 0.7% | 19.8 | 28.5 | 24.3 | 14.5 | 12.7 | 2.0 | 6.1 | 39.9 |
| | | 10.3 | | 0.2% | 10.5 | 12.8 | 4.9 | 7.4 | 7.7 | 0.9 | 5.0 | 6 |
| | T20 Blank-Blank | 12.7 | | 0.2% | 15.2 | 8.9 | 2.7 | 8.7 | 5.6 | 0.9 | 1.7 | 101 |
| | | | | 0.0% | 22.8 | 10.2 | 0.2 | 10.0 | 1.5 | 0.0 | 03 | 00 |
| | | | | | | | | | | |);) | 1 |

| | | % of | % of | 1-9 k | 1-9 km Altitude Band | Band | 9-131 | 9-13 km Altitude Band | Band | Fuel | Fuel |
|----------------------|---------|--------|--------|-------|----------------------|------|----------|-----------------------|------|----------|-----------|
| | Fuel | Global | Total | | | | | | | (1000 | (1000 |
| Generic OAG | (1000 | Fuel | within | ū | Ξ | Ξ | Ξ | ū | Ū | kg/day) | kg/day) |
| Type Airplane/engine | kg/day) | Burned | Type | (NOX) | (CO) | (HC) | (XON) | (CO) | (HC) | (1-9 km) | (9-13 km) |
| Turboprops | 8,787.6 | 2.5% | | 11.9 | 3.8 | 0.2 | | | | 7,416.3 | |
| SF3 MDTURB | 1.266.2 | | 14.41% | 12.5 | 4.4 | 0.5 | | | | 1,074.6 | |
| DH8 MDTURB | 960.1 | | 10.93% | 12.8 | 4.3 | 0.6 | | | | 802.0 | |
| ATR_LGTURB | 797.2 | | 9.07% | 14.2 | 3.8 | 0.0 | | | | 679.4 | |
| BE1_SMTURB | 755.9 | | 8.60% | 8.8 | 3.1 | 0.1 | | | | 645.3 | - |
| EM2 SMTURB | 721.8 | | 8.21% | 8.8 | 3.0 | 0.1 | | | | 618.9 | |
| AT7 LGTURB | 529.3 | | 6.02% | 14.2 | 3.7 | 0.0 | | | | 443.3 | |
| F50 LGTURB | 527.5 | | 6.00% | 14.2 | 3.8 | 0.0 | | | | 450.8 | |
| J31 SMTURB | 358.0 | | 4.07% | 8.8 | 3.0 | 0.1 | | | | 295.7 | |
| DH1 MDTURB | 326.4 | | 3.71% | 12.5 | 4.4 | 0.5 | | | | 271.6 | |
| SWM SMTURB | 289.4 | | 3.29% | 8.7 | 3.1 | 0.1 | | | | 252.6 | |
| J41 MDTURB | 282.6 | | 3.22% | 12.2 | 4.5 | 0.5 | | | | 244.9 | |
| D38 MDTURB | 267.9 | | 3.05% | 11.6 | 4.6 | 0.5 | | | | 241.2 | |
| S20 LGTURB | 238.7 | | 2.72% | 13.7 | 3.8 | 0.0 | | | | 212.2 | |
| DH3_MDTURB | 217.1 | | 2.47% | 12.5 | 4.4 | 0.5 | - | | | 186.3 | |
| AT4 LGTURB | 187.8 | | 2.14% | 14.1 | 3.8 | 0.0 | | | | 160.3 | |
| DHT SMTURB | 176.1 | | 2.00% | 8.9 | 3.0 | 0.1 | | | | 113.9 | |
| ATP_LGTURB | 111.7 | | 1.27% | 14.4 | 3.6 | 0.0 | | | | 90.3 | |
| SH6_MDTURB | 95.7 | | 1.09% | 13.8 | 3.9 | 0.5 | | | | 70.3 | |
| EMB_SMTURB | 94.2 | | 1.07% | 8.9 | 3.0 | 0.1 | | | | 73.0 | |
| F27_LGTURB | 91.1 | | 1.04% | 14.1 | 3.8 | 0.0 | | | | C.C/ | |
| AN4_LGTURB | 88.1 | | 1.00% | 13.6 | 3.9 | 0.0 | | | | 79.2 | |
| BEH SMTURB | 73.2 | | 0.83% | 8.7 | 3.1 | 0.1 | | | | 61.3 | |
| DH7_LGTURB | 52.8 | | 0.60% | 14.4 | 3.7 | 0.0 | | | | 43.0 | _ |
| D28 SMTURB | 49.9 | | 0.57% | 8.9 | 3.0 | 0.1 | <u> </u> | | | 37.2 | |
| HS7_LGTURB | 46.8 | | 0.53% | 13.9 | 3.8 | 0.0 | | | | 40.5 | |
| YS1_LGTURB | 37.5 | | 0.43% | 14.2 | 3.6 | 0.0 | | | | 29.0 | _ |
| BE9 SMTURB | 30.8 | | 0.35% | 8.7 | 3.2 | 0.1 | | | | 27.4 | |
| YN7_LGTURB | 25.3 | | 0.29% | 14.0 | 3.9 | 0.0 | - | | | 22.5 | |

| | | | % of | % of | 1-9 ki | 1-9 km Altitude Band | Band | 9-13 k | 9-13 km Altitude Band | Band | Fuel | Filel |
|-----------|-------------------------|---------|--------|--------|--------|----------------------|------|--------|-----------------------|------|------------|-----------|
| | | Fuel | Global | Total | | | | | | | (1000 | (1000 |
| Generic | | (1000 | Fuel | within | Ξ | Ξ | Ξ | Ξ | Ē | Ξ | ka/dav) | ka/dav) |
| Type | Airplane/engine | kg/day) | Burned | Type | (NOX) | (co) | (HC) | (NOX) | (co) | (HC) | (1-9 km) | (9-13 km) |
| | : | | | · | | | | | | | | Ì |
| r urbopro | l urboprops (Continued) | | | | | | | | | | | |
| | L4T_SMTURB | 24.8 | | 0.28% | 8.8 | 3.0 | 0.1 | | | | 10 6 | |
| | BES_SMTURB | 9.8 | | 0.11% | 8.7 | 2.8 | 0.1 | | | | ο.α α | |
| | CVF_LGTURB | 9.0 | | 0.10% | 13.9 | 3.9 | 0.0 | | | | 00 | |
| | LOF_LGTURB | 8.1 | | 0.09% | 13.3 | 3.7 | 0.0 | | | | 8.7 | |
| | ANF_MDTURB | 6.1 | | 0.07% | 11.0 | 4.2 | 0.2 | | | | 2. L | |
| | LOM_LGTURB | 5.6 | | 0.06% | 13.3 | 3.9 | 0.0 | | | | - | |
| | SH3_MDTURB | 5.6 | | 0.06% | 13.2 | 4.2 | 0.5 | | | | 45.4 | |
| | IL8_LGTURB | 3.8 | | 0.04% | 13.3 | 3.8 | 0.0 | | | | | |
| | AN6_MDTURB | 3.7 | | 0.04% | 11.2 | 4.7 | 0.4 | | | | 9 C | |
| | CS5_LGTURB | 3.5 | | 0.04% | 13.0 | 3.5 | 0.0 | | | | 24 | |
| | CNC_SMTURB | 2.2 | | 0.03% | 9.1 | 2.5 | 0.1 | | | | | |
| | SHS_SMTURB | 2.0 | | 0.02% | 8.9 | 3.0 | 0.1 | | | | | |
| | ND2_MDTURB | 1.9 | | 0.02% | 14.9 | 3.4 | 0.3 | | | |) (°. | |
| | LOH_LGTURB | 1.4 | | 0.02% | 13.6 | 3.8 | 0.0 | | | | | |
| | CV5_LGTURB | 0.7 | | 0.01% | 14.9 | 3.6 | 0.0 | | | | 9 U 9 U | |
| | | | | | | | | | | | | |

| Generic OAG Airplane/Engine Distance % of Global Average Type 0 | ance % day) E 2,579 116 445 | % of Global Distance | Daily Departures | % of Global Departures | Average Route Distance (km) |
|---|---|-------------------------|---------------------|---------------------------|-----------------------------|
| IS A300-600 A300-620R_PW4000-4158 A300-600R_CF6-80C2A5 A300-600_CF6-80C2A3 A300-600_CF6-80C2A3 A300-620_JT9D-7R4H1 A300-620_PW4000-4158 A300-600R_CF6-80C2A5F A300-600R_CF6-80C2A5F A300-B2/B4/F4 | 2,579 ,116 ,445 | | | - | |
| 0R_PW4000-4158 0R_CF6-80C2A5 0_CF6-80C2A3 0_JT9D-7R4H1 0_FRT_CF6-80C2A5F 0_PW4000-4158 0R_CF6-80C2A5F 0R_CF6-80C2A5F | 2,579 ,116 ,445 | | | | |
| V4000-4158 -6-80C2A5 -80C2A5 -80C2A3 D-7R4H1 D-7R4H1 C_CF6-80C2A5F F6-80C2A5F F6-80C2A5F | ,116 ,445 | 1.4% | 825 | 1.2% | 1,228 |
| -6-80C2A5 -80C2A3 D-7R4H1 F_CF6-80C2A5F 4000-4158 F6-80C2A5F F6-80C2A5F | 445 | 43.3% | 474 | 57.5% | 925 |
| -80C2A3 D-7R4H1 F_CF6-80C2A5F 4000-4158 F6-80C2A5F | · · · | 39.8% | 193 | 23.4% | 2,092 |
| D-7R4H1 F_CF6-80C2A5F 4000-4158 F6-80C2A5F | 224 | 6.7% | 63 | 7.6% | 1,085 |
| CF6-80C2A5F 4000-4158 F6-80C2A5F | 405 | 4.1% | 58 | 7.0% | 719 |
| 4000-4158 F6-80C2A5F | 086 | 4.1% | 28 | 3.4% | 1,453 |
| | ,803 499 | 1.1% 0.9% | 9 6 | 0.7% 0.4% | 1,801 2,771 |
| | 1,690 | 0.4% | 199 | 0.3% | 1,377 |
| A300-R4-200 CF6-50C2 88.165 | .165 | 32.2% | 56 | 28.3% | 1,570 |
| <u>.</u> | 704 | 15.2% | 35 | 17.5% | 1,201 |
| | 972 | 12.4% | 20 | 10.3% | 1,663 |
| | 132 | 11.0% | 24 | 12.2% | 1,248 |
| 5 | ,841 | 7.6% | 22 | 10.9% | 096 |
| 0C2 | ,140 | 7.0% | 7 | 3.7% | 2,62/ |
| | ,244 | 6.3% | 24 | 12.1% | /18 |
| 50C2 | ,552 | 6.1% | 9 | 2.9% | 2,897 |
| A300-B4-200FF_CF6-50C2 3,402 | 402 539 | 1.2% 0.9% | 2 | 1.2% | 1,111 |
| 3000-0-10-001-40-0 | | 4 50/ | AGA | %L 0 | 2.251 |
| Airbus A310 Airbus A310 | 100,44 | % C -1 | 5 | | |
| A310-300 CF6-80C2A2 312,847 | 2,847 | 30.0% | 146 | 31.5% | 2,141 |
| | 5,031 | 25.4% | 109 | 23.6% | 2,425 |
| A310-300 CF6-80C2A8 | 6,423 | 19.8% | 71 | 15.2% | 2,919 |
| A310-200 CF6-80A3 107,586 | 7,586 | 10.3% | 29 | 12.8% | 1,810 |
| | 3,743 | 5.6% | 30 | 6.5% | 2000 L |
| | 36,845 | 3.5% | 51 | 4.5% | |
| 6A | 5,994 | 3.5% | 14 | 3.1% | 2,520 |
| | 20,889 | 2.0% | 13 | 2.8% | 685,1 |

| Type | Distance (km/day) | % of Global Distance | Daily Departures | % of Global Departures | Average Route Distance (km) |
|-------------------------|----------------------|-------------------------|--|---------------------------|-----------------------------|
| Airbus A319 | 692,169 | 1.0% | 537 | 0.8% | 1,289 |
| A319-110_CFM56-5A4 | 232,750 | 33.6% | 109 | 20 3% | c |
| A319-110_CFM56-5A5 | 193,924 | 28.0% | 151 | 28.1% 28.1% | Z, 138 |
| A319-110_CFM56-5B5_P | 94,740 | 13.7% | 65 | 12 0% | 1,200 |
| A319-110_CFM56-5B6_2P | 61,614 | 8.9% | 26 | 10.5% | 1014,1 |
| A319-110_CFM56-5B6_P | 48,724 | 7.0% | 86 | 16.0% | 260,1 |
| A319-130_V2500-2524-A5 | 35,150 | 5.1% | 52 | 9.6% | 000 |
| A319-130_V2500-2522-A5 | 25,266 | 3.7% | 19 | 3.5% | 1.330 |
| Airbus A320 | 3,818,451 | 5.4% | 3,071 | 4.4% | 1,243 |
| A320-110_CFM56-5A1 | 1,824,134 | 47.8% | 1 667 | 705 PS | |
| A320-210_CFM56-5B4 P | 673,556 | 17 6% | 375 | | 1,034 |
| | 653 320 | 17.1% | 064 | 12.2% | 1,798 |
| A320-210_CFM56-5A3 | 253 641 | 6.6% | 4.00 | 14.3% | 1,490 |
| A320-210 CFM56-5B4 | 117 499 | 0.0% | 19/ | 0.4% | 1,285 |
| A320-210_CFM56-5B4_2 | 95,698 | 00 2.5% | 2++ | 2.5% | 1,561 |
| A320-210_CFM56-5B4_2P | 85 472 | 0.0% | 0 | 0.0% 0.10% | 823 |
| A320-230 V2500-2527E-A5 | 48.379 | 1 20/ | 70 | 2.1% | 1,046 |
| A320-230_V2500-2500-A1 | 37 428 | 0/0-1 700 F | 5 5 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 | 1.0% | 966 |
| A320-230_V2500-2527-A5 | 29,316 | 0.8% | 38 | 1.1% | 1,110 774 |
| Airbus A321 | 361,687 | 0.5% | 448 | 0.6% | 807 |
| A321-110_CFM56-5B2 | 111,007 | 30.7% | 102 | 70/ Z0/ | COC + |
| A321-110_CFM56-5B1_2 | 71,275 | 19.7% | 108 | 24.0% | 560,1 660 |
| A321-130_V2500-2530-A5 | 59,509 | 16.5% | 67 | 14.9% | 890 |
| A321-210_CFM56-5B3_P | 53,446 | 14.8% | 62 | 13.7% | 868 |
| | 53,269 | 14.7% | 102 | 22.7% | 524 |
| GA-2522-UUC2V_UC2-126A | 13,180 | 3.6% | 6 | 2.0% | 1.488 |

| Generic OAG Airplane/Engine Type | Distance (km/day) | % of Global Distance | Daily Departures | % of Global Departures | Average Route Distance (km) |
|--|------------------------------|-------------------------|--|---------------------------|-----------------------------|
| Airbus A330-200 | 138,796 | 0.2% | 39 | 0.1% | 3,572 |
| A330-220_PW4000-4168A A330-240_Trent-772B-60 A330-200_CF6-80E1A4 | 119,770 18,068 958 | 86.3% 13.0% 0.7% | 34 4 | 88.2% 11.0% 0.7% | 3,493 4,216 3,353 |
| Airbus A330-300 | 510,219 | 0.7% | 250 | 0.4% | 2,044 |
| A330-320_PW4000-4168 A330-300_CF6-80E1A2 | 152,881 129,029 | 30.0% 25.3% | 78 47 | 31.1% 18.7% | 1,971 2,771 |
| A330-340_Trent-772-60 A330-320_PW4000-4164 A330-340_Trent-768-60 | 112,357 58,195 57,757 | 22.0% 11.4% 11.3% | 63 46 16 | 25.4% 18.3% 6.6% | 1,775 1,273 3,516 |
| Airbus A340-200 | 140,216 | 0.2% | 20 | 0.0% | 6,961 |
| A340-210_CFM56-5C2 A340-210_CFM56-5C2G A340-210_CFM56-5C3_F | 92,676 26,794 20,746 | 66.1% 19.1% 14.8% | τ 9 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 | 64.5% 15.6% 19.9% | 7,129 8,525 5,186 |
| Airbus A340-300 | 1,250,423 | 1.8% | 224 | 0.3% | 5,589 |
| A340-310_CFM56-5C4 A340-310_CFM56-5C2 A340-310_CFM56-5C3_F | 754,377 405,735 90,310 | 60.3% 32.5% 7.2% | 144 55 24 | 64.6% 24.8% 10.7% | 5,223 7,320 3,785 |

| Generic OAG Airplane/Engine Type | Distance (km/day) | % of Global Distance | Daily Departures | % of Global Departures | Average Route Distance (km) |
|--|----------------------|-------------------------|---------------------|---------------------------|-----------------------------|
| BAC111 | 45,221 | 0.1% | 57 | 0.1% | 797 |
| One-Eleven-500_Spey-512-14DW One-Eleven-560_Spey-512-14DW | 27,964 17,257 | 61.8% 38.2% | 37 20 | 64.7% 35.3% | 762 863 |
| BAE 146 | 630,398 | %6 .0 | 9 93 | 1.4% | 635 |
| 146-200_ALF502-R-5 146-300_ALF502-R-5 | 415,062 114,367 | 65.8% 18.1% | 686 195 | 69.1% 19.6% | 605 587 |
| 146-100_ALF502-R-5 146-300_LF507-1H | 53,409 41,890 | 8.5% 6.7% | 59 45 | 5.9% 4.6% | 910 922 |
| 146-300QT_FRT_ALF502-R-5 | 5,670 | 0.9% | 8 | 0.8% | 602 |
| Boeing 707 | 105,766 | 0.2% | 41 | 0.1% | 2,607 |
| 707-320C_JT3D-3B | 2,722 | 2.6% | 2 | 4.9% | 1,361 |
| 707-320C_FRT_JT3D-7 707-320C_FRT_JT3D-3B | 13,664 84,458 | 12.9% 79.9% | 31 5 | 11.3% 77.5% | 2,989 2,687 |
| 707-320C_All_FRT_JT3D-3B | 4,922 | 4.7% | e | 6.3% | 1,914 |
| Boeing 717 | 0 | 0.0% | o | 0.0% | o |
| | | | | | |

| Generic OAG Airplane/Engine Type | Distance (km/day) | % of Global Distance | Daily Departures | % of Global Departures | Average Route Distance (km) |
|-------------------------------------|----------------------|-------------------------|---------------------|---------------------------|-----------------------------|
| Boeing 727-100 | 205,915 | 0.3% | 261 | 0.4% | 789 |
| 727-100QF_FRT_RB.183-651-54 | 36,435 | 17.7% | 50 | 19.2% | 729 |
| 727-100F FRT JT8D-9 | 2,123 | 1.0% | 2 | 0.8% | 991 |
| 727-100F_FRT_JT8D-7B | 41,525 | 20.2% | 54 | 20.8% | 765 |
| 727-100C JT8D-9 | 11,797 | 5.7% | 80 | 3.2% | 1,400 |
| 727-100C_CMB_JT8D-7B | 7,668 | 3.7% | ъ | 2.0% | 1,451 |
| 727-100C_CMB_JT8D-7 | 1,491 | 0.7% | - | 0.6% | 1,044 |
| 727-100_JT8D-9 | 3,087 | 1.5% | ო | 1.1% | 1,080 |
| 727-100_JT8D-7B | 86,090 | 41.8% | 112 | 42.9% | 769 |
| 727-100_JT8D-7 | 15,700 | 7.6% | 25 | 9.5% | 635 |
| | | | | | |
| Boeing 727-200 | 2,532,550 | 3.6% | 2,353 | 3.4% | 1,077 |
| 727-200_JT8D-15 | 1,443,421 | 57.0% | 1,403 | 59.7% | 1,029 |
| 727-200_JT8D-9A | 449,984 | 17.8% | 360 | 15.3% | 1,248 |
| 727-200_JT8D-17R | 279,982 | 11.1% | 235 | 10.0% | 1,190 |
| 727-200F_FRT_JT8D-9 | 91,148 | 3.6% | 92 | 3.9% | 986 |
| 727-200_JT8D-9 | 84,997 | 3.4% | 116 | 4.9% | 734 |
| 727-200F_FRT_JT8D-15 | 51,931 | 2.1% | 42 | 1.8% | 1,236 |
| 727-200F_FRT_JT8D-7 | 49,592 | 2.0% | 42 | 1.8% | 1,185 |
| 727-200_JT8D-17 | 32,169 | 1.3% | 28 | 1.2% | 1,143 |
| 727-200F_FRT_JT8D-17R | 22,337 | 0.9% | 19 | 0.8% | 1,158 |
| 727-200_JT8D-7B | 20,257 | 0.8% | 10 | 0.4% | 2,085 |
| 727-200F_FRT_JT8D-17 | 6,733 | 0.3% | 4 | 0.2% | 1,625 |

| Generic OAG Airplane/Engine Type | Distance (km/day) | % of Global Distance | Daily Departures | % of Global Departures | Average Route Distance (km) |
|-------------------------------------|----------------------|-------------------------|---------------------|---------------------------|-----------------------------|
| Boeing 737-100/200 | 3,176,590 | 4.5% | 4,013 | 5.8% | 792 |
| 737-200_JT8D-9A | 1,215,577 | 38.3% | 1,528 | 38.1% | 796 |
| 737-200_JT8D-15 | 639,196 | 20.1% | 844 | 21.0% | 758 |
| 737-200_JT8D-15A | 393,614 | 12.4% | 552 | 13.8% | 713 |
| 737-200_JT8D-17 | 311,240 | 9.8% | 400 | 10.0% | 778 |
| 737-200C_QC_JT8D-17A | 302,133 | 9.5% | 307 | 7.7% | 984 |
| 737-200_JT8D-17A | 185,907 | 5.9% | 219 | 5.5% | 850 |
| 737-200C_CMB_JT8D-17 | 47,616 | 1.5% | 61 | 1.5% | 786 |
| 737-200_JT8D-9 | 28,804 | 0.9% | 36 | 0.9% | 794 |
| 737-200C_JT8D-9A | 10,874 | 0.3% | 12 | 0.3% | 928 |
| 737-200QC_FRT_JT8D-9A | 7,622 | 0.2% | 8 | 0.2% | 1,007 |
| 737-200C_JT8D-15 | 6,896 | 0.2% | 15 | 0.4% | 473 |
| 737-200C_JT8D-17 | 5,456 | 0.2% | 80 | 0.2% | 682 |
| 737-200C_JT8D-17A | 5,350 | 0.2% | 10 | 0.2% | 559 |
| 737-200C_QC_JT8D-15A | 4,781 | 0.2% | 2 | 0.1% | 2,092 |
| 737-200QC_FRT_JT8D-15 | 3,463 | 0.1% | 2 | 0.1% | 1,865 |
| 737-200C_QC_JT8D-9 | 3,280 | 0.1% | 5 | 0.1% | 717 |
| 737-200C_CMB_JT8D-9A | 2,875 | 0.1% | 4 | 0.1% | 719 |
| 737-200_JT8D-7 | 1,218 | 0.0% | 2 | 0.1% | 609 |
| 737-200C_QC_JT8D-15 | 688 | 0.0% | ••• | 0.0% | 963 |
| Boeing 737-300/400/500 | 9,147,802 | 13.0% | 10,224 | 14.7% | 895 |
| 737-300_CFM56-3B1 | 4,200,235 | 45.9% | 4,671 | 45.7% | 668 |
| 737-400_CFM56-3C1 | 1,769,552 | 19.3% | 1,932 | 18.9% | 916 |
| 737-500_CFM56-3C1 | 1,006,448 | 11.0% | 1,304 | 12.8% | 772 |
| 737-500_CFM56-3B1 | 662,492 | 7.2% | 728 | 7.1% | 911 |
| 737-300_CFM56-3C1 | 646,331 | 7.1% | 708 | 6.9% | 913 |
| 737-300_CFM56-3B2 | 580,178 | 6.3% | 593 | 5.8% | 978 |
| 737-400_CFM56-3B2 | 279,567 | 3.1% | 282 | 2.8% | 991 |
| /3/-300UC_UC_CFM56-3C1 | 2,998 | 0.0% | 9 | 0.1% | 477 |

| | Uistance (km/day) | % of Global Distance | Daily Departures | % of Global Departures | Average Route Distance (km) |
|---------------------------|----------------------|-------------------------|---------------------|---------------------------|-----------------------------|
| Boeing 737-600/700/800 | 1,047,151 | 1.5% | 127 | 1.1% | 1,357 |
| 737-R00 CFM56-7B26 | 418,237 | 39.9% | 260 | 33.7% | 1,611 |
| 737-700 CFM56-7B22 | 281,044 | 26.8% | 208 | 26.9% | 1,352 |
| 737-700 CFM56-7B24 | 274,064 | 26.2% | 203 | 26.3% | 1,351 |
| 737-600 CFM56-7B20 | 62,655 | 6.0% | 67 | 12.5% | 648 |
| 737-800_CFM56-7B24 | 11,150 | 1.1% | 4 | 0.6% | 2,518 |
| Boeing 747-100/200/300 | 2,573,174 | 3.7% | 570 | 0.8% | 4,517 |
| 747-200B, JT9D-7Q | 410,087 | 15.9% | 75 | 13.2% | 5,447 |
| 747-200SF FRT CF6-50E2 | 289,007 | 11.2% | 64 | 11.2% | 4,516 |
| 747-200F FRT CF6-50E2 | 244,817 | 9.5% | 54 | 9.4% | 4,570 |
| 747-200F FRT JT9D-7Q | 220,206 | 8.6% | 51 | 8.9% | 4,354 |
| 747-100F FRT_JT9D-7A | 150,102 | 5.8% | 43 | 7.6% | 3,491 |
| 747-300 BB211-524D4 | 124,189 | 4.8% | 27 | 4.7% | 4,600 |
| 747-200B CMB CF6-50E2 | 115,260 | 4.5% | 16 | 2.9% | 7,016 |
| 747-200B_CF6-50E2 | 92,295 | 3.6% | 15 | 2.6% | 6,212 |
| 747-300_JT9D-7R4G2 | 89,993 | 3.5% | 17 | 2.9% | 5,431 |
| 747-200B_JT9D-7J | 80,322 | 3.1% | 52 | 3.9% | 3,627 |
| 747-300_CF6-50E2 | 75,833 | 3.0% | 11 | 2.0% | 6,806 |
| 747-200F_FRT_JT9D-7J | 65,191 | 2.5% | 16 | 2.8% | 4,038 |
| 747-100_JT9D-7A | 65,143 | 2.5% | 17 | 3.0% | 3,832 |
| 747-200B_RB211-524D4 | 61,008 | 2.4% | 12 | 2.1% | 5,024 |
| 747-300 CF6-80C2B1 | 56,156 | 2.2% | 8 | 1.4% | 6,896 |
| 747-200F FRT RB211-524D4 | 51,559 | 2.0% | 13 | 2.3% | 4,010 |
| 747-200B JT9D-7R4G2 | 48,806 | 1.9% | 7 | 1.3% | 6,570 |
| 747-200B JT9D-7A | 39,446 | 1.5% | 12 | 2.1% | 3,327 |
| 747-100 JT9D-7 | 33,445 | 1.3% | 9 | 1.0% | 5,853 |
| 747-200SF FRT_RB211-524D4 | 28,566 | 1.1% | 9 | 1.1% | 4,444 |
| 747-SP RB211-524D4 | 25,712 | 1.0% | 9 | 1.0% | 4,500 |
| 747-300 CMB CF6-50E2 | 25,654 | 1.0% | 9 | 1.1% | 4,081 |

| | Ulstartce (km/day) | % of Global Distance | Daily Departures | % of Global Departures | Average Route Distance (km) |
|------------------------|-----------------------|-------------------------|---------------------|---------------------------|-----------------------------|
| | | | | | |
| | | | | | |
| /4/-300 CMB JI9D-/H4G2 | 22,234 | ~о 0 | ~ | /0£ 0 | |
| | 19 752 | 0.8% | r (1 | 0.1.% | 5,986 |
| CERENES | 101.0C | 0.0 200 | 5 · | 1.1% | 3,142 |
| | 10,744 | 0.0% | 4 | 0.8% | 3,674 |
| | 14,599 | 0.6% | 16 | 2.8% | 912 |
| 7 | 12,610 | 0.5% | e | 0.5% | 4 203 |
| | 12,268 | 0.5% | 8 | 1.5% | 1 481 |
| -524C2 | 12,124 | 0.5% | ю | 0.6% | 3 536 |
| - | 10,410 | 0.4% | S | 0.9% | 0000 |
| D-7R4G2 | 9,739 | 0.4% | 0 | 0.4% | 4 010 |
| | 8,388 | 0.3% | 2 | 0.4% | |
| -50E | 7,756 | 0.3% | | 0.3% | 4,134 |
| | 6,956 | 0.3% | - | 0.2% 0.2% | 2 - 1 C |
| <u>-</u> | 6,465 | 0.3% | - | 0.2% | 0, I - 3 6 465 |
| T9D-7Q | 6,128 | 0.2% | | 0.4% | 0,400 |
| | 4,929 | %0 0 | 1 0 | 0.4.0 | 2,000 |
| -6-50E2 | | 2,10 | , , | 0.0% | 1,917 |
| | 4,3UU | 0.2% | | 0.1% | 7,876 |
| | 2,328 | 0.1% | - | 0.1% | 4,074 |
| | 2,152 | 0.1% | - | 0.2% | 2,511 |
| /4/-2005_J19D-/0A 1,26 | 1,293 | 0.1% | - | 0.1% | 2.262 |

| Generic OAG Airplane/Engine Type | Distance (km/day) | % of Global Distance | Daily Departures | % of Global Departures | Average Route Distance (km) |
|-------------------------------------|----------------------|-------------------------|---------------------|---------------------------|-----------------------------|
| Boeing 747-400 | 5,664,264 | 8.1% | 1,006 | 1.4% | 5,632 |
| 747-400 CF6-80C2B1F | 1,924,604 | 34.0% | 398 | 39.6% | 4,830 |
| 747-400 PW4000-4056 | 1,474,135 | 26.0% | 246 | 24.5% | 5,982 |
| 747-400 BB211-524H2 | 1,072,744 | 18.9% | 158 | 15.7% | 6,783 |
| 747-400 CMB CF6-80C2B1F | 601,789 | 10.6% | 102 | 10.2% | 5,883 |
| 747-400 BB211-524G | 242,152 | 4.3% | 32 | 3.2% | 7,567 |
| 747-400F FRT PW4000-4056 | 125,433 | 2.2% | 25 | 2.5% | 4,933 |
| 747-400 CMB PW4000-4056 | 118,220 | 2.1% | 24 | 2.4% | 4,897 |
| 747-400F FRT CF6-80C2B1F | 79,428 | 1.4% | 14 | 1.4% | 5,673 |
| 747-400F_FRT_RB211-524H2 | 25,760 | 0.5% | 5 | 0.5% | 5,304 |
| Boeing 757-200 | 4,828,701 | 6.9% | 2,741 | 3.9% | 1,762 |
| 757-200 PW2000-2037 | 2,130,837 | 44.1% | 1,241 | 45.3% | 1,717 |
| 757-200 BB211-535E4B | 1,051,066 | 21.8% | 405 | 14.8% | 2,593 |
| 757-200 BB211-535E4 | 977,170 | 20.2% | 562 | 20.5% | 1,740 |
| 757-200 PW2000-2040 | 264,613 | 5.5% | 134 | 4.9% | 1,968 |
| 757-200PF FRT RB211-535E4 | 217,355 | 4.5% | 174 | 6.4% | 1,249 |
| 757-200 BB211-535C | 177,641 | 3.7% | 222 | 8.1% | 266 |
| 757-200PE FRT PW2000-2040 | 10.018 | 0.2% | ო | 0.1% | 3,896 |

| Generic OAG Airplane/Engine Type | Distance (km/day) | % of Global Distance | Daily Departures | % of Global Departures | Average Route Distance (km) |
|-------------------------------------|----------------------|-------------------------|---------------------|---------------------------|-----------------------------|
| Boeing 767-200 | 1,417,564 | 2.0% | 492 | 0.7% | 2,884 |
| 767-200_JT9D-7R4D | 373,990 | 26.4% | 119 | 24.2% | 3 150 |
| 767-200ER_CF6-80A | 267,474 | 18.9% | 61 | 12.5% | 4 354 |
| 767-200ER_CF6-80C2B2 | 173,046 | 12.2% | 39 | 7.9% | 4 470 |
| 767-200_CF6-80A | 118,609 | 8.4% | 110 | 22.4% | 1 077 |
| 767-200EM_JT9D-7R4D | 114,484 | 8.1% | 23 | 4.7% | 4.978 |
| 767-200ER_PW4000-4056 | 67,773 | 4.8% | 12 | 2.4% | 5.785 |
| 767-200ER_CF6-80C2B4 | 59,372 | 4.2% | 10 | 2.0% | 6.023 |
| 767-200ER_JT9D-7R4E | 51,047 | 3.6% | 48 | 9.9% | 1 054 |
| 767-200ER_JT9D-7R4E4 | 51,015 | 3.6% | 26 | 5.4% | 1.930 |
| 767-200ERM_JT9D-7R4E | 39,616 | 2.8% | 12 | 2.4% | 3.424 |
| 767-200_CF6-80C2B2F | 32,646 | 2.3% | 16 | 3.2% | 2 059 |
| 767-200EM_CF6-80A2 | 24,814 | 1.8% | 4 | 0.8% | 6.203 |
| 767-200PC_FRT_CF6-80A | 23,122 | 1.6% | 6 | 1.8% | 2.611 |
| 767-200ER_CF6-80C2B4F | 20,559 | 1.5% | ю | 0.6% | 7,196 |
| Boeing 767-300 | 4,043,356 | 5.8% | 1,533 | 2.2% | 2,638 |
| 767-300ER_PW4000-4060 | 1,686,367 | 41.7% | 477 | 31 1% | 2 E 2 E |
| 767-300ER_CF6-80C2B6 | 809,403 | 20.0% | 191 | 12.4% | 0,000 |
| 767-300ER_CF6-80C2B6F | 496,144 | 12.3% | 124 | 8.1% | 3 907 |
| 767-300_CF6-80C2B2 | 279,758 | 6.9% | 312 | 20.4% | 896 |
| /67-300EH_HB211-524H3 | 166,978 | 4.1% | 66 | 6.4% | 1.694 |
| 767-300EHF_FH1_CF6-80C2B6F | 123,009 | 3.0% | 60 | 3.9% | 2,050 |
| 76/-300EH_CF6-80C2B4 | 111,343 | 2.8% | 42 | 2.8% | 2.633 |
| /6/-300_J19D-7H4D | 92,559 | 2.3% | 101 | 6.6% | 918 |
| 767-300ER_PW4000-4056 | 69,406 | 1.7% | 22 | 1.5% | 3,095 |
| 707 000 CF6-80C2B2F | 60,661 | 1.5% | 49 | 3.2% | 1,242 |
| | 43,500 | 1.1% | 11 | 0.7% | 3,854 |
| /0/-300EH_CF6-80C2B2 | 42,449 | 1.1% | 12 | 0.8% | 3,496 |

| Appendix E – Departure | | ce Summarie | es for May 199 | and Distance Summaries for May 1999 Scheduled Air Traffic | r Traffic |
|-----------------------------|-----------|-------------|----------------|---|-----------------------------|
| Generic OAG Airplane/Engine | Distance | % of Global | Daily | % of Global | Average Route Distance (km) |
| Type | (km/day) | Distance | Departures | Departures | |
| | | | | | |
| Boeing 767-300 (Continued) | | | | | |
| 767-300ER PW4000-4062 | 19,138 | 0.5% | ß | 0.4% | 3,525 |
| 767-300ER RB211-524H2 | 15,996 | 0.4% | 6 | 0.6% | 1,750 |
| 767-300 CF6-80C2B4F | 8,989 | 0.2% | 7 | 0.5% | 1,284 |
| 767-300_PW4000-4056 | 8,950 | 0.2% | 8 | 0.5% | 1,119 |
| 767-300ERF_FRT_CF6-80C2B7F | 8,706 | 0.2% | Э | 0.2% | 2,902 |
| Boeing 777-200 | 1,583,564 | 2.3% | 473 | 0.7% | 3,345 |
| 777-200ER PW4000-4090 | 452,251 | 28.6% | 93 | 19.7% | 4,848 |
| 777-200ER GE90-92B | 371,319 | 23.5% | 112 | 23.6% | 3,324 |
| 777-200ER Trent-892 | 290,345 | 18.3% | 60 | 12.8% | 4,805 |
| 777-200ER GE90-85B | 204,362 | 12.9% | 42 | 8.8% | 4,899 |
| 777-200ER Trent-884 | 94,872 | 6.0% | 27 | 5.6% | 3,551 |
| 777-200_PW4000-4074 | 80,207 | 5.1% | 80 | 16.9% | 1,004 |
| 777-200 Trent-875 | 49,713 | 3.1% | 27 | 5.6% | 1,871 |
| 777-200_PW4000-4077 | 40,495 | 2.6% | 33 | 7.0% | 1,222 |
| Boeing 777-300 | 131,672 | 0.2% | 82 | 0.1% | 1,614 |
| 777-300 Trent-892 | 93,513 | 71.0% | 38 | 46.1% | 2,489 |
| 777-300 PW4000-4090 | 38,160 | 29.0% | 44 | 53.9% | 867 |
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| Generic OAG Airplane/Engine Tvpe | Distance (km/dav) | % of Global Distance | Daily | % of Global | Average Route Distance (km) |
|-------------------------------------|----------------------|-------------------------|----------|-------------|-----------------------------|
| | (formula) | DISIGNED | ncharmes | nepai tures | |
| DC-10 | 1,523,344 | 2.2% | 379 | 0.5% | 4,022 |
| DC-10-30_CF6-50C2 | 570,817 | 37.5% | 110 | 29.1% | 5 183 |
| DC-10-40_JT9D-20 | 312,347 | 20.5% | 29 | 20.8% | 3.968 |
| DC-10-10_CF6-6K | 160,953 | 10.6% | 40 | 10.6% | 3.995 |
| DC-10-30_CF6-50C | 112,142 | 7.4% | 31 | 8.2% | 3.634 |
| DC-10-10F_FRT_CF6-6D | 84,340 | 5.5% | 32 | 8.4% | 2.659 |
| DC-10-10_CF6-6D | 74,985 | 4.9% | 27 | 7.2% | 2.763 |
| DC-10-30CF_CF6-50C2 | 65,741 | 4.3% | 17 | 4.5% | 3.900 |
| DC-10-401_JT9D-59A | 65,671 | 4.3% | 28 | 7.3% | 2.382 |
| DC-10-30F_FRT_CF6-50C2 | 61,993 | 4.1% | 13 | 3.6% | 4.616 |
| DC-10-30_CF6-50C2R | 12,227 | 0.8% | 0 | 0.5% | 7,133 |
| DC-10-30_CF6-50C1 | 2,126 | 0.1% | 0 | 0.1% | 7,440 |
| | | | | | |
| DC-8 | 451,733 | 0.6% | 266 | 0.4% | 1,699 |
| DC-8-71F_FRT_CFM56-2C1 | 182,142 | 40.3% | 107 | 40.2% | 1.705 |
| DC-8-73CF_FRT_CFM56-2C1 | 90,719 | 20.1% | 62 | 23.2% | 1,473 |
| DC-8-63_FRT_JT3D-7 | 82,442 | 18.3% | 51 | 19.1% | 1.621 |
| DC-8-73F_FRT_CFM56-2C1 | 31,639 | 7.0% | 11 | 4.3% | 2.803 |
| DC-8-61C_FRT_JT3D-3B | 21,294 | 4.7% | 13 | 5.1% | 1.586 |
| DC-8-54CF_FRT_JT3D-3B | 19,964 | 4.4% | 13 | 4.7% | 1,588 |
| DC-8-63CF_FRT_JT3D-7 | 14,112 | 3.1% | 9 | 2.4% | 2,195 |
| DC-8-62CF_FRT_JT3D-3B | 9,420 | 2.1% | 3 | 1.1% | 3,297 |

| Generic OAG Airplane/Engine Type | Distance (km/day) | % of Global Distance | Daily Departures | % of Global Departures | Average Route Distance (km) |
|-------------------------------------|----------------------|-------------------------|---------------------|---------------------------|-----------------------------|
| DC-9 | 2,379,550 | 3.4% | 3,346 | 4.8% | 711 |
| DC-9-31_JT8D-7B | 669,058 | 28.1% | 965 | 28.9% | 693 |
| DC-9-32_JT8D-9A | 472,957 | 19.9% | 557 | 16.7% | 849 |
| DC-9-31_JT8D-9A | 328,957 | 13.8% | 530 | 15.8% | 621 |
| DC-9-51_JT8D-17 | 232,402 | 9.8% | 441 | 13.2% | 526 |
| DC-9-41_FRT_JT8D-11 | 132,692 | 5.6% | 167 | 5.0% | 296 |
| DC-9-15_JT8D-7A | 110,330 | 4.6% | 121 | 3.6% | 915 |
| DC-9-41_JT8D-11 | 73,398 | 3.1% | 113 | 3.4% | 651 |
| DC-9-32_JT8D-7A | 70,219 | 3.0% | 84 | 2.5% | 836 |
| DC-9-32_JT8D-7B | 67,205 | 2.8% | 92 | 2.7% | 734 |
| DC-9-32_JT8D-17 | 57,120 | 2.4% | <u>66</u> | 2.0% | 865 |
| DC-9-31_JT8D-7A | 51,878 | 2.2% | 44 | 1.3% | . 1,171 |
| DC-9-51_JT8D-17A | 32,469 | 1.4% | 62 | 1.9% | 522 |
| DC-9-21_JT8D-11 | 18,449 | 0.8% | 21 | 0.6% | 879 |
| DC-9-41_JT8D-15 | 16,761 | 0.7% | 18 | 0.5% | 924 |
| DC-9-15_JT8D-7 | 13,024 | 0.6% | 20 | 0.6% | 651 |
| DC-9-32_JT8D-11 | 10,691 | 0.5% | 15 | 0.5% | 693 |
| DC-9-32_JT8D-9 | 8,819 | 0.4% | 15 | 0.5% | 588 |
| DC-9-31CF_JT8D-17 | 6,950 | 0.3% | 9 | 0.2% | 1,081 |
| DC-9-15RC_FRT_JT8D-7B | 3,126 | 0.1% | 4 | 0.1% | 729 |
| DC-9-33CF_JT8D-9A | 3,045 | 0.1% | 4 | 0.1% | 688 |
| | | | | | |
| Fokker 100 | 1,079,091 | 1.5% | 1,697 | 2.4% | 636 |
| 100-*_RB.183-650-15 | 963,270 | 89.3% | 1,499 | 88.4% | 643 |
| 100-*_RB.183-620-15 | 115,820 | 10.7% | 198 | 11.6% | 586 |

| • | | | • | | • |
|-------------------------------------|----------------------|-------------------------|---------------------|---------------------------|-----------------------------|
| Generic OAG Airplane/Engine Type | Distance (km/day) | % of Global Distance | Daily Departures | % of Global Departures | Average Route Distance (km) |
| | | | | | |
| Fokker 28 | 358,254 | 0.5% | 626 | | 572 |
| F.28-4000_Spey-555-15P | 299,518 | 83.6% | 495 | %0.67 | 605 |
| F.28-1000_Spey-555-15 | 29,868 | 8.3% | 69 | 11.0% | 434 |
| F.28-3000_Spey-555-15H | 15,862 | 4.4% | 23 | 3.6% | 698 |
| F.28-2000_Spey-555-15 | 10,042 | 2.8% | 29 | 4.6% | 348 |
| F.28-4000_Spey-555-15H | 2,964 | 0.8% | . | 1.7% | 273 |
| Fokker 70 | 149,699 | 0.2% | 198 | 0.3% | 756 |
| 70-*_RB.183-620-15 | 149,699 | 100.0% | 198 | 100.0% | 756 |
| Lockheed L-1011 | 288,761 | 0.4% | 140 | | 2,058 |
| L-1011-1_RB211-22B | 197,439 | 68.4% | 106 | 75.8% | 1.858 |
| L-1011-500_RB211-524B4 | 60,864 | 21.1% | 22 | 15.5% | 2,803 |
| L-1011-200_FRT_RB211-524B | 13,561 | 4.7% | 9 | 4.1% | 2,373 |
| L-1011-50_RB211-22B | 13,309 | 4.6% | 5 | 3.4% | 2,823 |
| L-1011-200_FRT_RB211-524B4 | 2,647 | 0.9% | 2 | 1.1% | 1,685 |
| L11_Blank-Blank | 940 | 0.3% | 0 | 0.2% | 3,289 |
| MD-11 | 1,541,979 | 2.2% | 308 | 0.4% | 5,006 |
| MD-11-Passenger_CF6-80C2D1F | 555,776 | 36.0% | 105 | 34.2% | 5,279 |
| MD-11-Freighter_FRT_CF6-80C2D1F | 337,791 | 21.9% | 82 | 26.5% | 4,141 |
| MD-11-Passenger_PW4000-4460 | 317,609 | 20.6% | 66 | 21.5% | 4,792 |

| Generic Type | Generic OAG Airplane/Engine Type | Distance (km/day) | % of Global Distance | Daily Departures | % of Global Departures | Average Route Distance (km) |
|-----------------|-------------------------------------|----------------------|-------------------------|---------------------|---------------------------|-----------------------------|
| | | | | | | |
| | MD-11 (Continuea) | | | | | |
| | MD-11-Passenger PW4000-4462 | 224,607 | 14.6% | 38 | 12.2% | 5,955 |
| | MD-11-Combi CMB CF6-80C2D1F | 59,034 | 3.8% | 8 | 2.6% | 7,513 |
| | MD-11-Freighter FRT PW4000-4460 | 37,810 | 2.5% | 8 | 2.5% | 4,994 |
| | MD-11-CF_QC_PW4000-4460 | 4,701 4.551 | 0.3% | | 0.4% 0.2% | 4,114 8,139 |
| | MD-11-CF_QQ_FW4000-44402 | | 2/2/2 | | | |
| MD-80 | | 5,619,233 | 8.0% | 5,397 | 7.7% | 1,041 |
| | MD-80-82 .178D-217C | 2.223.295 | 39.6% | 1,907 | 35.3% | 1,166 |
| | MD-80-05-05 519 | 1,284,164 | 22.9% | 1,174 | 21.8% | 1,094 |
| | MD-80-88 JT8D-219 | 918,618 | 16.4% | 1,008 | 18.7% | 912 |
| | MD-80-82 JT8D-217A | 478,447 | 8.5% | 426 | 7.9% | 1,123 |
| | MD-80-87 JT8D-217C | 207,137 | 3.7% | 234 | 4.3% | 887 |
| | MD-80-81 JT8D-217C | 199,394 | 3.6% | 338 | 6.3% | 290 |
| | MD-80-81_JT8D-217 | 163,056 | 2.9% | 171 | 3.2% | 954 |
| | MD-80-82 JT8D-217 | 91,286 | 1.6% | 75 | 1.4% | 1,213 |
| | MD-80-87_JT8D-219 | 46,861 | 0.8% | 20 | 0.9% | 937 |
| | MD-80-83_JT8D-217C | 6,976 | 0.1% | 15 | 0.3% | 461 |
| 06-QM | a | 331,624 | 0.5% | 442 | 0.6% | 750 |
| | MD 60-30 V2500-2528-D5 | 168 019 | 50.7% | 188 | 42.4% | 895 |
| | MD-90-30_V2500-2525-D5 | 163,605 | 49.3% | 255 | 57.6% | 643 |
| | | | \000 C | u | 0.01% | 659 |
| Misce | Miscellaneous | 3,013 | ° |) | | 1 1 1 1 |
| | DFL Blank-Blank | 2,146 | 71.2% | n | 68.8% | 683 |
| | LRJ_Blank-Blank | 866 | 28.8% | | 31.3% | 606 |

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| Generic OAG Airplane/Engine Type | Distance (km/day) | % of Global Distance | Daily Departures | % of Global Departures | Average Route Distance (km) |
|-------------------------------------|----------------------|-------------------------|---------------------|---------------------------|-----------------------------|
| Regional Jets | 2,096,416 | 3.0% | 3,198 | 4.6% | 656 |
| CRJ-100ER_CF34-3A1 | 931,379 | 44,4% | 1 417 | 705 VV | ŬĽ |
| EMJ_Blank-Blank | 309,117 | 14.8% | 465 | 14 5% | 00/ |
| RJ-RJ85_LF507-1F | 258,052 | 12.3% | 434 | 13.6% | 000 707 |
| CRJ-100LR_CF34-3A1 | 151,954 | 7.3% | 202 | 6.3% | 750 |
| CRJ-200LR_CF34-3B1 | 123,117 | 5.9% | 166 | 5.2% | 740 |
| RJ-RJ100_LF507-1F | 97,273 | 4.6% | 162 | 5.1% | 500 600 |
| ERJ-145-ER_AE-A | 73,519 | 3.5% | 145 | 4.5% | 509 |
| CRJ-200ER_CF34-3B1 | 52,196 | 2.5% | 73 | 2.3% | 711 |
| RJ-RJ70_LF507-1F | 45,163 | 2.2% | 61 | 1.9% | 746 |
| ERJ-145-EP_AE-A | 37,098 | 1.8% | 48 | 1.5% | 775 |
| ERJ-145-EP_AE-A1_1 | 13,370 | 0.6% | 19 | 0.6% | 889 |
| ERJ-145-LR_AE-A1 | 4,178 | 0.2% | 9 | 0.2% | 665 |
| | | | | | |
| | 1,266,310 | 1.8% | 701 | 1.0% | 1,806 |
| Tu-154-B_NK-8-2U | 375,774 | 29.7% | 192 | 27.4% | 1 950 |
| II-62-M_D-30-KU | 199,657 | 15.8% | 37 | 5.3% | 5 334 |
| Tu-154-M_D-30-KU-154-II | 192,131 | 15.2% | 115 | 16.5% | 1.665 |
| 1u-134-A_D-30-3 | 161,969 | 12.8% | 129 | 18.4% | 1.253 |
| II-86-*_NK-86 | 80,838 | 6.4% | 33 | 4.7% | 2,482 |
| II-76-1_FRT_D-30-KP-2 | 55,117 | 4.4% | 20 | 2.8% | 2.776 |
| Iu-134-A_D-30-2 | 42,909 | 3.4% | 37 | 5.2% | 1.173 |
| II-96-300_PS-90-A | 29,432 | 2.3% | 5 | 0.7% | 6.438 |
| Yak-42-*_D-36 | 25,717 | 2.0% | 23 | 3.3% | 1,111 |
| Yak-40-"_AI-25 | 25,391 | 2.0% | 41 | 5.9% | 615 |
| Yak-42-U_U-36 | 18,436 | 1.5% | 19 | 2.7% | 666 |

| Generic OAG Airplane/Engine Type | Distance (km/day) | % of Global Distance | Daily Departures | % of Global Departures | Average Route Distance (km) |
|-------------------------------------|----------------------|-------------------------|---------------------|---------------------------|-----------------------------|
| Russian Aircraft (Continued) | | | | | |
| Vak-40-* AI-25-Rlank | 15.018 | 1.2% | 59 | 4.1% | 523 |
| Vak-42-* D-36-Blank | 14,974 | 1.2% | 1 | 1.5% | 1,417 |
| II-62-* NK-8-4 | 9,968 | 0.8% | ო | 0.4% | 3,489 |
| II-R6-* NK-R6-Blank | 6.107 | 0.5% | 2 | 0.2% | 3,563 |
| An-124-* FBT D-18-T | 5,416 | 0.4% | 2 | 0.2% | 3,446 |
| TI-134-B D-30-3 | 4.882 | 0.4% | 4 | 0.6% | 1,178 |
| II-76-M FRT D-30-KP-2 | 1,878 | 0.2% | - | 0.1% | 3,287 |
| T20_Blank-Blank | 695 | 0.1% | 0 | 0.0% | 2,433 |
| Concorde | 33,890 | 0.05% | Q | 0.01% | 5,648 |
| concorde_05_1999 | 33,890 | 100.0% | 9 | 100.0% | 5,648 |
| Turboprops | 6,608,584 | 9.4% | 21,296 | 30.6% | 310 |
| SE3 MDTUBB | 935,252 | 14.2% | 2,688 | 12.6% | 348 |
| DH8 MDTURB | 685,694 | 10.4% | 2,270 | 10.7% | 302 |
| BE1 SMTURB | 650,725 | 9.9% | 2,247 | 10.6% | 290 |
| EM2 SMTURB | 633,128 | 9.6% | 1,927 | 9.1% | 329 |
| ATR_LGTURB | 538,681 | 8.2% | 1,610 | 7.6% | 335 |
| AT7 LGTURB | 355,585 | 5.4% | 1,097 | 5.2% | 324 |
| F50_LGTURB | 355,384 | 5.4% | 1,078 | 5.1% | 330 |
| J31 SMTURB | 304,815 | 4.6% | 1,127 | 5.3% | 270 |
| SWM SMTURB | 253,832 | 3.8% | 761 | 3.6% | 333 |
| DH1 MDTURB | 238,445 | 3.6% | 753 | 3.5% | 317 |
| D38 MDTURB | 215,605 | 3.3% | 424 | 2.0% | 508 |
| .141 MDTUBB | 215,009 | 3.3% | 531 | 2.5% | 405 |
| | | | | | |

| Generic OAG Airplane/Engine | | | | | |
|-----------------------------|----------------------|-------------------------|------------|---------------------------|-----------------------------|
| Type | Distance (km/day) | % of Global Distance | Departures | % of Global Departures | Average Route Distance (km) |
| | | | | | |
| Turboprops (Continued) | | | | | |
| S20_LGTURB | 173.530 | 2.6% | 333 | 1 6% | C |
| DH3_MDTURB | 158,280 | 2.4% | 492 | 0.3% | 220 |
| DHT_SMTURB | 129,414 | 2.0% | 1,080 | 5.1% | 120 |
| AT4_LGTURB | 125,453 | 1.9% | 407 | 1.9% | 308 |
| EMB_SMTURB | 76,313 | 1.2% | 384 | 1.8% | 199 |
| AIP_LGIURB | 71,950 | 1.1% | 285 | 1.3% | 252 |
| AN4_LGTURB | 64,815 | 1.0% | 116 | 0.5% | 101 |
| BEH_SMTURB | 63,492 | 1.0% | 216 | 1.0% | 200 |
| F27_LGTURB | 61,075 | 0.9% | 205 | 1.0% | 208 |
| SH6_MDTURB | 59,446 | 0.9% | 345 | 1.6% | 172 |
| D28_SMTURB | 40,021 | 0.6% | 216 | 1.0% | 1.85 |
| DH7_LGTURB | 34,387 | 0.5% | 127 | 0.6% | 221 |
| HS7_LGTURB | 31,414 | 0.5% | 100 | 0.5% | 1 6 |
| BE9_SMTURB | 26,645 | 0.4% | 89 | 0.4% | 301 |
| | 23,575 | 0.4% | 113 | 0.5% | 602 |
| | 20,111 | 0.3% | 103 | 0.5% | 194 |
| YN/_LGIUHB | 17,525 | 0.3% | 43 | 0.2% | 404 |
| BES_SMTURB | 8,784 | 0.1% | 21 | 0.1% | 410 |
| | 6,600 | 0.1% | 4 | 0.0% | 1 711 |
| CVF_LGIUHB | 6,304 | 0.1% | 16 | 0.1% | 394 |

| Generic OAG Airplane/Engine | Distance | % of Global Distance | Departures | % of Global Departures | Average Route Distance (km) |
|-----------------------------|----------------|-------------------------|------------|---------------------------|-----------------------------|
| I ype | (from the last | | | | |
| Turboprops (Continued) | | | | | |
| ANE METIDE | 5 469 | 0.1% | ۍ | 0.0% | 1,196 |
| | 4 310 | 0.1% | 9 | 0.0% | 774 |
| | 3.755 | 0.1% | 16 | 0.1% | 239 |
| | 3 154 | 0.1% | 5 | 0.0% | 649 |
| | 2,944 | 0.0% | ო | 0.0% | 859 |
| | 2 100 | 0.0% | 15 | 0.1% | 139 |
| | 1.593 | 0.0% | თ | 0.0% | 186 |
| | 1.488 | 0.0% | 18 | 0.1% | 85 |
| | 1 044 | 0.0% | 6 | 0.0% | 112 |
| | 004 | 0.0% | 0 | 0.0% | 435 |
| | 446 | 0.0% | - | 0.0% | 312 |

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