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Research Needs in Fire Safety for the Human Exploration and Utilization of Space

Proceedings and Research Plan

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Preface

The purpose of the workshop documented in this publication was to bring together personnel responsible for the design and operations of the International Space Station (ISS) and the fire protection research community to review the current knowledge in fire safety relative to spacecraft. From this review, research needs were identified that were then used to formulate a research plan with specific objectives. The time and effort spent by the presenters, working group moderators, and participants to attend this workshop and share their knowledge in fire safety is greatly appreciated. I would also like to thank Ms. Christine Gorecki and Ms. Sandi Jones of the National Center for Microgravity Research in Fluids and Combustion for coordinating the local arrangements and travel of all the attendees. Their efforts ensured that participants arrived ready to address the significant concerns of fire safety in spacecraft.

In this document, I have attempted to capture the very informative and lively discussions that occurred in the plenary sessions and the working groups. I hope that it will be useful to readers and serve as a significant step in assuring fire protection for the crews of current and future spacecraft.

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Executive Summary

On June 25–26, 2001, 64 people representing combustion research and fire prevention professionals from NASA, industry, military, and academia met in Cleveland, Ohio, to participate in a workshop entitled “Research Needs in Fire Safety for the Human Exploration and Utilization of Space.” The objective of this workshop was to bring together experts in various disciplines related to spacecraft fire safety to (1) identify research needed to ensure fire safety in future shuttle and International Space Station (ISS) systems and payloads, (2) promote ISS fire safety through proposals for innovative designs, operations, and validation procedures, (3) identify areas of concern inherent to prolonged human-crew missions in Earth orbit and beyond, and (4) anticipate research required to plan and design spacecraft and habitats for long-duration space missions and planetary exploration. The outcome of this workshop was a list of immediate and long-term areas of concern regarding fire safety in manned spaceflight.

Workshop attendees participated in one of three working groups depending on their area of expertise and interest. These working groups had the following focus areas:

1. Fire Prevention and Material Flammability
2. Smoke and Fire Detection
3. Fire and Post-Fire Response

Each of the working groups began their deliberations by assessing the current knowledge and “state of the art” in their respective focus areas. At the discretion of the working group chairs, short presentations were made to review current research in the appropriate areas. Based on this assessment, topics requiring additional information and/or technical understanding to guide flight system design and flight procedures were identified. The working groups then suggested research directions and topics to obtain the required data. The findings of each working group were presented to the workshop attendees during the closing session and opened for discussion. The working group moderators provided written documentation of the conclusions of their group in addition to their presentations. After the workshop, a 10-year research plan was developed that incorporated the inputs provided during the workshop. The overall objective of the research conducted in this plan is to provide data for the rational design of fire safety systems for manned spacecraft and significantly improve crew and system safety from fires.

Introduction

Space travel is an inherently dangerous activity making crew health and safety of primary concern in the space program. The vehicle structure and the crew are exposed to high levels of stress, and the hostile external environment makes escape and rescue nearly impossible. Many potential hazards can arise in space operations, among which are fire, atmospheric contamination, injury, explosion, loss of pressure, and meteoroid and debris penetration. These are examples of prompt-effect hazards, that is, those requiring immediate response for alleviation. Space operations are also subject to delayed-effect hazards, which are those requiring less urgent or timely response, such as contamination, hidden damage, and corrosion. Fire is one of the foremost prompt-effect hazards, but it also contributes to the delayed-effect hazards. Hence, fire-protection strategies must cover the restoration, repair, and cleanup activities after a fire event in addition to the obvious prevention and control before and during a fire.

Probably the most important factor distinguishing spacecraft fire protection from terrestrial procedures in extreme environments (e.g., submarines and aircraft) is the strong influence of the low-gravity environment that dominates fire and particulate behavior and control in spacecraft. The substantial upward buoyant flow generated by large density gradients in fires at 1-g is practically eliminated in spacecraft. Heat and mass-transport rates – and consequently ignition, flammability, fire characteristics, and flame-spread rates – vary considerably from those experienced in conventional, terrestrial fires. At partial gravity levels, the effects of buoyancy, convection, and diffusion can combine to produce unique combustion results. Thus, fire prevention, detection, and suppression practices for spacecraft and extraterrestrial habitats must be developed specifically to respond to the unique aspects of microgravity combustion.

Synopses of Previous Workshops on Spacecraft Fire Safety

At least three workshops to assess existing knowledge in spacecraft fire safety and guide research efforts have been held in the last sixteen years. The participants of the current workshop did not specifically review the outcomes of these previous workshops, so comparison of the outcomes can be viewed as an evolution of the research needs brought about by continuing advances in knowledge and new mission objectives. In fact, some of the participants of the current workshop also attended one or more of the previous workshops and they have helped shape the spacecraft fire safety research that has been conducted over the last fifteen years. A short synopsis of these previous workshops is given below.

In 1986, a workshop entitled “Spacecraft Fire Safety” was held with the results published in NASA CP 2476 (Ref. 1) and a conference paper (Ref. 2). This workshop, held in Cleveland, Ohio and sponsored by NASA Lewis Research Center, began with a symposium with ten original survey papers on the following ten topics related to fire safety.

1. Techniques for fire detection
2. Fire-related standards and testing
3. Fire extinguishment and inhibition in spacecraft environments
4. Inerting and atmospheres
5. Fire-related medical science
6. Aircraft fire safety research
7. Space Station internal environmental and safety concerns
8. Microgravity combustion fundamentals
9. Spacecraft material flammability testing and configurations
10. Ignition and combustion of metals in oxygen

At the conclusion of these lectures, five forums were convened to develop recommendations for research and technology. These forums and the recommendations from each are given below:

Fire detection and ignition

- a. Study of detection of overheated and smoldering components, with emphasis on the development of heat-sensitive coatings
- b. Improvement of sensing systems, and incorporation of multiple fire-signature decision software
- c. Development of central detector systems for command of localized sensing stations
- d. Study of fire signatures expected in low gravity and nonstandard atmospheres
- e. Inventory of spacecraft equipment and procedures to anticipate hazards and locate sensors

Fire extinguishment

- a. Fundamental research on combustion and suppression in microgravity and space-unique environments
- b. Testing and evaluation of candidate suppressants
- c. Development of specific extinguishment and inerting techniques for hazardous areas of the spacecraft
- d. Planning for post-fire atmosphere cleanup
- e. Establishment of cooperative working groups to pursue analogies between space and submarine research

Human responses to combustion products and inert atmospheres

- a. Revision of material acceptance standards to test toxicology of emission products
- b. Emphasis on human responses in establishing fire safety policies
- c. Study of combustion, pyrolysis, and extinguishment products expected in microgravity
- d. Update of human tolerance limits to pollutants and reduced-oxygen atmospheres
- e. Designation and training of at least one spacecraft crew member as a fire marshal on each mission

Spacecraft materials and configurations

- a. Further flammability testing in low-gravity environments
- b. Further testing on overheating and product generation from common materials
- c. Further long-term material testing to include aging effects
- d. Establishment of data banks to share and correlate space, aircraft, and ground fire models

Selection of spacecraft atmospheres

- a. Research and technology programs on alternative spacecraft cabin atmospheres
- b. Research on combustion, pyrolysis, and smoldering in all atmospheres
- c. Establishment of data banks to collect knowledge on fire behavior in unusual environments
- d. Further research on atmospheric contamination by extinguishants

A second workshop was held at the University of California, Los Angeles, on October 31–November 1, 1991 to review progress and topics related to the Risk-Based Fire Safety Experiment Project. This project was sponsored the NASA In-Space Technology Experiment Program (IN-STEP) and its principal goal was to develop and perform experiments based on Probabilistic Risk Assessment needs that will be used in models to quantify fire risk in humans-crew spacecraft (Ref. 3). The presentations and subsequent discussions were intended to guide the UCLA and NASA investigators on the state of knowledge and perceived needs in spacecraft fire safety and its risk management. The workshop consisted of formal presentations on current safety practices related to design-to-preclude strategies and material selection, probabilistic risk assessments, combustion science in spacecraft environments, and the specific hazard of smoke in spacecraft. While hardcopies of the presentations can be found in the workshop report (Ref. 3), the general findings were (1) that Probabilistic Safety Assessment methods

would be a great value to the design and operation of future manned spacecraft, (2) the importance of understanding and testing of smoldering as a likely fire scenario in space, and (3) the need for smoke damage modeling to better predict damage by this mechanism.

A third workshop entitled “Research for Space Exploration: Physical Sciences and Process Technologies,” sponsored by the Microgravity Research Division of NASA was held in Cleveland in 1997. The broad research priorities for spacecraft fire safety developed in this workshop are documented in reference 4 and were as follows:

1. Research on electrical system diagnostics to provide an early, pre-incident warning to breakdowns, possibly resistivity or continuity checks.
2. Determination of flammability, flame spread, flame luminosity, limiting oxygen, and soot sizes under various atmospheres for thick materials and polymers at 1/3 g.
3. Determination of flame sizes, soot sizes, and flammability from thick materials with imposed heat flux under microgravity conditions.
4. Determination of combustion limits, ignitability, and flame luminosity of premixed methane and oxygen for propulsion and fire safety.
5. Research on fundamental behavior of various gaseous, liquid suppressants, and solid-surface fires at 1/3 g and microgravity with modeling and experiment verification.

While many of these remain as relevant research areas, the missions for which fire safety research is required are constantly evolving. Instead of developing knowledge of fire safety procedures and systems for the initial occupancy of the International Space Station, we are now concerned with maintaining, validating, and improving fire safety on the ISS throughout its lifetime while providing maximum flexibility in the types of experiments and operations that can be conducted. We must also look forward to the special fire safety requirements for travel to and habitation of the Moon and Mars. Research needs for these applications may include:

- Evaluation of fire initiation hazards arising from waste disposal, trash storage, laundry, household activities, and the storage of fuel gas and oxygen systems
- Development of technology for the efficient detection systems required for long-duration missions in terms of rapid response, discrimination, false-alarm rejection, multiple-sensor logic, etc.
- Identification and evaluation of new suppression agents and techniques required for long-range missions, Lunar or Martian habitation, and in-situ resource utilization (ISRU) extinguishment
- Identification of fire safety issues in ISRU operations such as operations at high temperature and pressures, oxygen handling, propellant storage, and safety in welding and thermal operations

Approach

To identify and address these issues, researchers and specialists from academia, industry, national laboratories, and NASA who work in the various theme areas of spacecraft fire safety such as applied combustion science and technology; environment control and life support; material flammability testing and fire prevention; spacecraft, habitat, and ISS design; and fire detection and suppression have been invited to this workshop. The workshop consisted of:

- Brief presentations reviewing spacecraft fire safety objectives in NASA’s Bio-Astronautics Initiative, current spacecraft fire safety research, and goals for the workshop
- Three simultaneous working groups each led by moderators who were responsible for directing and focusing the discussion on the theme area

- Presentation of the recommendations and prioritizations for future research by the discussion group leaders to the workshop participants

The three working groups had the following theme areas:

1. Fire Prevention and Material Flammability
2. Smoke and Fire Detection
3. Fire and Post-Fire Response

Group leaders and co-leaders for each group were identified prior to the workshop. In consultation with the workshop technical organizer, participants were placed into one of the three working groups to allow them to prepare for the discussions. All participants were notified of their assignments and fellow group members in advance of the workshop. The group leaders were tasked with moderating the discussion and providing a written synopsis of the discussion and findings of their group as well as copies of their oral presentation prior to leaving the workshop. These summaries were used to produce the reports presented in the next section.

Summary of the Working Groups

The summaries of the three working groups are presented in this section. These summaries have been developed from the written reports supplied by the working group leaders as well as the oral presentations of the findings delivered to all participants during the closing session of the workshop. The working groups had freedom in developing and evaluating topics during their deliberations. To ensure that no information or continuity of thought was lost while preparing these summaries, no effort was made to standardize the format of the results from the groups.

Smoke and Fire Detection

Moderators: Dr. David L. Urban, NASA Glenn Research Center
Dr. Tom Cleary, National Institute of Standards and Technology

This group consisted of 15 participants (see List of Attendees). The group began its work by brainstorming ideas for issues and concerns and, from these, identifying research areas. These were then sorted and presented to all workshop participants during the closing session.

By nature, smoke and fire detection is a technology-driven aspect of fire protection. Improvements in sensor technology can be implemented in a fire or smoke detector to allow them to respond faster and more reliably to a fire threat. However, advancement in technology is a necessary but not sufficient step for the improvement of smoke and fire detectors. Designers must also know what these sensors should be looking for. For example, the Comparative Soot Diagnostics (CSD) experiment that flew in the Glovebox on STS-75 demonstrated that the microgravity performance of the fire detectors could be different from their 1-g performance. This performance difference was attributed to the growth of larger smoke particles in 0-g because of the increased residence time in high smoke concentration regions (Ref. 5).

Issues and Concerns

The group began by formulating consensus statements and issues that served as a starting point for discussions. First, there was a generally recognized paucity of data to guide the development of fire detection systems in spacecraft. This was one of the greatest concerns of this working group. Therefore, the group focused on defining the issues and concerns related to the design and operation of fire detection

systems on spacecraft to identify data required to provide the needed data. This list of issues and concerns were postulated in the form of questions related to the operation of current systems and are identified in Table 1. They are divided into issues relating to the detector operation, crew response, and some general issues. These issues existed primarily because of the lack of knowledge of one or more fundamental aspects of fire behavior in a low-gravity, spacecraft environment.

Relationships between the identified issues and concerns were then examined to identify areas of research required to address these concerns. This analysis resulted in the identification of three major and three minor research areas, again posed as research questions. In these research areas, specific types of data or analyses were identified that would address the research question. Research that was most critical to address the issues was identified as near-term.

Table 1. Issues and Concerns for Smoke and Fire Detection Systems

Issue
<u>Smoke and Fire Detection</u>
1. What should we detect?
2. Where do we put the detectors?
3. Does the detector produce frequent nuisance alarms?
4. Will it detect all types of fires?
5. How does the sensor respond to reduced visibility?
<u>Crew Response</u>
6. Is detection quick enough to give crew adequate time to respond?
7. How does the crew know where the fire is?
8. How should the crew respond, how will they respond?
9. Can the sensor give an indication of the indicate danger level?
10. What capability is required for post-fire sensing (toxicity & corrosion)?
<u>General</u>
11. Will current systems/procedures work?
12. What are the risks outside of the crew cabin?
13. What is the effect of partial gravity on fire signature and detector response?

Research Questions

1. What are we looking for?
 - a. Target and high-risk fire definitions
 - b. Fire signatures
 - c. Threshold settings and background levels
 - d. What aren't we looking for?
2. When and how do we respond?
 - a. Levels of response/automation
 - b. Nuisance levels (impact on human response)
 - c. Human factors
3. How do we design and place detectors?
 - a. Technology/modality
 - b. Air flow in modules
 - c. Automation (detection and response)
 - d. Sampling

- e. Integration into ISS
 - f. Requirements
 - g. Risk Assessment
 - h. Annunciation technique
4. What post-fire detection is needed?
 5. What fire detection/protection systems are required for uninhabited regions of spacecraft?
 6. How are the fire signatures and detector response different in partial-gravity environments?

Of these research questions identified above, the first three were considered as the highest priority. The group also realized that technology exists to address these questions but had yet to be applied to this task. To address “What are we looking for?” The working group felt that the identification of a target or high-risk fire and the determination of fire signatures was the most immediate, near-term research that should be accomplished. In research question 2, all three sub-areas, *i.e.*, evaluation of the level of response and degree of automation that should be used to respond to a fire, the elimination of nuisance alarms, and other human factors related to the response of the crew to a fire were identified as potential near-term research areas.

Enabling Technologies

The greatest enabling technology for improved smoke and fire detection are the development of small, robust sensors that can detect very small amounts of a wide variety of fire signatures. This includes sensors that measure CO, CO₂, HCl, hydrocarbons, and smoke. These sensors can be made in several forms including solid-state MEMS sensors, and various gas absorption techniques. Each method has its advantages and disadvantages but they are still under development. Concurrent development of these systems is being done so that their response to an actual fire can be adequately evaluated.

Many of these technologies will allow a fire or smoke detector to be considerably smaller and use less power than existing instruments. This could allow a distributed network of detectors operated by a distributed intelligence system. A system of this type composed of different types of detectors could have a very low incidence of nuisance alarms, more rapidly locate the fire, and even dispense suppressant to a specified location.

In the course of these discussions, the group realized the dichotomy between physical factors and human factors in fire and smoke detection. Human factors were given less consideration by the group not because of its relative unimportance but because the group felt that their expertise did not allow them to adequately address these issues.

Summary and Conclusions

There was general agreement that current detection systems are based upon inadequate knowledge of the types of fire signatures for spacecraft materials, the effect of low gravity on fire signatures, and the transport of fire precursors within a spacecraft. Current systems have been designed using current knowledge but are generally unverified in a zero-g environment. Because existing systems only respond to smoke, they are susceptible to dust and the risk of nuisance alarms is significant. Each alarm requires valuable crew time to respond and evaluate the alarm. Repeated nuisance alarms over time could increase the crew's response time. The existing systems also have a poor track record in detecting small transients that could indicate a fire precursor. There is also no data with which to predict performance during larger events.

Detection in large cabin volumes and standoffs is a concern because of the sparsely located detectors within the open cabin volumes. Ventilation systems within a volume will eventually draw air through a detector but the transport of smoke is not evaluated.

Further improvements in detection will require implementation of hybrid detection systems consisting of sensors for species and particles. Which species these sensors should look for and what combination of sensors should be placed in what locations will have to be determined by future tests. Finally, there are ignition sources other than electrical sources that must receive consideration. Spontaneous ignition is a potential risk and detection in waste systems may not be adequate.

Fire Prevention and Material Flammability

Moderators: Professor James T'ien, Case Western Reserve University
Dr. Dennis E. Griffin, NASA Marshall Space Flight Center

This working group consisted of 24 participants (see List of Attendees). The group began by identifying outstanding issues related to fire prevention and material flammability. They focused primarily on issues related to ISS and Shuttle systems because these systems are well-defined with respect to materials used, testing procedures, etc. The issues identified by the group are as follows:

1. Fire scenarios for ISS/Shuttle
2. Testing/screening methods
3. Development of new materials
4. Flammability at elevated oxygen levels (>30%)
5. ISRU processes and storage

Within each of these issues, the group recommended research areas and identified the highest priority research that should be conducted. Desired outcomes from the research were also identified. The information for each of the issues will be discussed in the following sections.

Issue 1: Fire Scenarios for ISS/Shuttle

The discussion centered on the most likely ignition mechanisms for manned spacecraft compartment fires. The following is a list of potential fire sources and scenarios in manned spacecraft for which the group felt there was a need for investigation. Particularly, they were concerned about determining the potential for and mitigation of fires from each of these sources. They are listed below in no particular order of priority:

1. Pressurized gaseous oxygen systems
High pressure oxygen systems (up to 6000 psia) exist that are subject to numerous ignition mechanisms, including "flow friction," compression heating, particle impact, contamination/kindling chain reactions, mechanical impact, friction, etc.
2. Solid Fuel Oxygen Generator (SFOG)
SFOG units have been responsible for two recorded fire events on Mir.
3. Overheating of electrical cable
Overheating of electrical cables and components (pyrolysis events) have been reasonably common during the manned space program. On average, such an event occurs once every ten missions.
4. Fire events caused by electrical short circuits
Short circuits have been responsible for the Apollo 204 and Apollo 13 fires. Also, does foreign object debris from a short circuit represent a fire hazard.
5. Effect of work-arounds/mods
The effect of work-arounds or other modifications that can occur especially in long duration mission should be evaluated. Can these significantly alter the potential for fire?

6. Aging electrical wire
Wear-induced failures in aging electrical systems can be a problem. There have been some occurrences of this recently in the Shuttle Orbiter and SRB.
7. Auto-ignition of waste storage
It is unknown whether waste might be susceptible to autoignition in low-gravity and, if so, under what conditions can this occur.

The working group noted that other possibilities exist that have not been considered here including fire and ignition hazards associated with propulsion systems, pyrotechnics, fuels cells and electrolysis systems, etc. One must be careful to not limit consideration of all possibilities when designing fire detection and suppression systems and experiments.

Of these potential fire scenarios, the highest research priority was to investigate ignition mechanisms and flammability for pressurized oxygen systems.

The outcome of research in the area of fire scenarios should lead to improvements in understanding and aid in mitigation of potential fire scenarios. This would occur through additional crew training on awareness and considerations for fire safety. The group also recommended that researchers take advantage of lessons learned from AWIGG (Aircraft Wiring and Inert Gas Generator) working group.

Issue 2: Testing/Screening Methods

The following is a list of recommendations for research that would improve and/or augment existing materials flammability screening methods:

1. Augment existing go/no go criteria with a quantitative test method which provides ranking or indication of flammability margin, e.g. LOI or radiation panel. This would provide more information to the standard Test 1 acceptance criteria to aid in more informed materials selections.
2. More understanding on relationship between 1-g test methods to microgravity performance. Due to the limited amount of microgravity data, this would allow for a better understanding of more appropriate material selection decisions.
3. Need to understand the implications of non-flaming and smoldering combustion in microgravity with respect to ISS engineering materials. Current NASA standard flammability test techniques do not take smoldering combustion into account so this data would fill this apparent gap.
4. There is a need for additional microgravity data on the effects of oxygen and flow on ignition, combustion and flame propagation for real engineering materials. This data is required to enable rational design analysis
5. Very little data is available on combustion behavior in partial gravity yet this information is required for future exploratory missions. There is a need to obtain such data, or possibly appropriate theoretical predictions or scaling analysis, from microgravity data.
6. A better understanding of the relationship between flame spread across thermally thick and thin materials must be established. Since the ability to obtain data using thermally thin samples is much better than for thermally-thick samples, a method or scaling relationship to accurately extrapolate thin data to more realistic thick spacecraft engineering materials would be very desirable.
7. There is a definite need for long duration microgravity experimental data. A facility to carry out long duration partial and microgravity combustion experiment is essential.
8. Currently NASA's materials selection criteria are based on flammability and not on the resulting toxicity of the combustion event. Research is needed to understand the toxicity and fire hazards associated with the pyrolysis of combustion products and production of aerosols. If necessary, this information should be factored into materials selection criteria, pre-fire events and post-fire response. (Need: Moderate)

Of these research areas, all were considered to be high priority except for item number 8.

Issue 3: New Materials Need to be Studied

The members of the working group recognized that future spacecraft were likely to be composed of different materials than those used in past and current spacecraft. Research topics within this area dealt with the need for additional or improved flammability investigations for these materials.

1. Flammability of Inflatable Structures (Moderate)
Inflatable structures may be used for interplanetary transportation system structures, e.g. TransHab-type concepts, due to launch vehicle space constraints. Information on flammability of these materials is required.
2. Non-Flammable Foam Packing Material (High)
Currently, flammable foam materials are widely used for ISS stowage and packaging. A nonflammable replacement would greatly benefit a short-term need.
3. Flame-Retardant Clothing (Moderate)
More comfortable flame retardant fabric or fabric treatments for crew clothing is required, especially during long term missions. Current cotton clothing is, of course, highly flammable and not suitable for fire fighting.
4. Alternative wire insulation (High)
An insulation material with the good properties (lightweight, flexible, high cut-through resistance) of polyimide and fluorocarbon constructions and none of the bad properties (poor tear resistance, cold flow, stiff) is needed.
5. Advanced composites (Moderate)
Advanced composites are becoming more common and are extensively used in ISS for rack structures and are even being considered for oxygen tanks. In consideration of the potential for smoldering combustion, their inherent flammability in enriched oxygen, and because of the obvious advantages they offer in terms of weight and strength, these materials merit further flammability investigations for spacecraft applications.

The working group emphasized that we may need to take advantage of FAA established data for advanced materials.

Issue 4: New Research Considerations

1. Since future interplanetary missions will be weight limited, gaseous N₂ may become a limited resource, hence microgravity experiments at oxygen concentrations greater than 30% should be considered.

Issue 5: ISRU processes and storage

This discussion dealt with in-situ high temperature/high pressure production processes that are being investigated to utilize lunar and planetary resources for providing life support fuel resources (e.g. oxygen, methane, CO, etc.)

1. Education and training of researchers
People doing this research may have not considered the possibilities of fire or explosion in the experimentation. Training and recognition of potential hazards is available in courses offered by ASTM, etc. (also see item #2 below)
2. Understanding of hazards analysis techniques
3. Improve understanding of flow friction as an ignition source
Flow friction involves a fluid leaking through a small orifice and has been thought to be the cause of several recent oxygen system fires. However, this ignition mechanism is not well understood. (Refer to Issue 1 research recommendations)

4. Supplement particle impact database
The data base for particle impact ignition information is very limited in terms of particulate sizes, types, velocities and temperatures. (Refer to Issue 1 research recommendations)

Issue 6: Risk assessment

This discussion involved the aspect of analyses for preventing fires and quantifying fire risk.

1. Probabilistic Risk Assessments
Gain a better understanding of available probabilistic risk assessment and simulation tools.
2. Aircraft, Submarine, and Ship Analogies
Understand what is done in the submarine industry.
3. Determine implications of limited microgravity data sets
What are the confidence level considerations for repeatability of microgravity data/experiments?
What are the implications when considering design of experiments (DOE) and the usefulness of limited sets of data?

Fire and Post-Fire Response

Moderators: Dr. Robert Friedman, NASA Glenn Research Center (retired)
Mr. J. Michael Bennett, Wright-Patterson AFB

This working group had 21 participants representing the government, various research organizations, and academia (see List of Attendees). The working sessions began with presentations on current research covering spacecraft fire response. Following these presentations, there was a general discussion about overall research needs in spacecraft fire safety and how many of these needs impacted topics in fire and post-fire response. The group then agreed to include topics that provided initial conditions for a fire response in their scope of research.

Current Technology Issues

First, the working group identified fundamental issues that can benefit greatly from new or increased information. This lack of knowledge hinders the ability of the fire-protection community to improve fire-protection capabilities. Examples of these basic needs include knowledge, measurements, predictions or correlations of the following:

1. Rate of fire spread anticipated in space platforms under realistic fire scenarios
2. Rate of extinguishing agent transport from the reservoirs to the site of the fire, and the phenomena that influence it
3. Actual effectiveness and limits of performance of the existing on-board carbon dioxide fire extinguishing systems
4. Performance and capabilities of the foam fire extinguishing systems currently employed by the Russians in space
5. Current NASA policy that may permit or preclude consideration of alternative fire extinguishing agents to carbon dioxide
6. Types of combustion by-products emitted by the fires and the extinguishing agents applied to them in spacecraft
7. Fundamental understanding of the influence of low gravity (reduced gravity and microgravity) on the extinguishment process and
8. Knowledge of the escape and evacuation mechanisms available to crew members

Research Areas

Next, the team discussed the major research areas and enabling technologies that can address the identified key issues. These discussions defined the areas of study for improvement and advancement of spacecraft fire and post-fire response techniques. The research is presented in the following list.

1. Experimental Determination of Flow in Compartments

The precise definition and characterization of the flow field in compartments where fires may occur, or where agent or by-products may flow, is of primary and fundamental concern for the fire-characterization process. For the ISS, the compartments are defined, in terms of increasing size, as the rack, module, and inter-module. Experimental data of the flow fields must be obtained in the appropriate low-gravity environment. Both scalar velocity and momentum data of the flows must be obtained. This activity should incorporate general flow fields in major zones and also local point sources of airflow variance due to the presence of inlet or outlet ducts, exhausts, etc.

2. CFD Representation of Flow in Compartments

This activity is a corollary to activity #1, which constructs a computational fluid dynamics (CFD) model to correspond to the experimental model being developed. This numerical model will be a tool of great assistance in later characterizing the fire-establishment and -propagation process. These two activities should interact with and jointly refine each other.

3. Digital Compartment Configuration Documentation

This effort entails the collection and development of engineering data on spacecraft compartment configurations, dimensions and components. These will be used as tools in defining fire-zone locations, conditions and geometries. The operating conditions, fuel sources and states (solid, liquid, gas), and other features pertinent to fire-protection analysis will be documented. Such data ideally are to be stored in digital formats for use in computer codes and models.

4. Proposal of Fire Scenarios

The goal of this activity is to identify likely fire locations, size, and growth or spread phenomena on-board spacecraft of interest. Such fire designations should incorporate pertinent aspects of smoldering or flaming conditions, as applicable. The presence or lack of sooting should also be noted and represented. This activity should also support the initiation of an updated fault-tree analysis (of issues related to fire safety) for platforms such as the International Space Station.

5. Characterization of Fire Event

Modeling specifically for a fire event starts with the experimental and numerical verification of the fire conditions. This will establish the phenomena of fire growth and spread in low-gravity conditions on a realistic scale. (Note the distinction between fire growth, a safety issue, and flame growth, a research and possibly safety issue.)

6. Development of Fire-Response Concepts

This activity starts with a review and assessment of the current fire-response systems to establish baseline protection. This leads to the proposal and development of new technologies to mitigate fire events. The innovative approaches will be based on the operating experience in space (as available) and the application of new data. The broad range of opportunities covers both passive and active fire mitigation. Passive responses are those of fire isolation, containment, power and flow shutdown, and the like. Active responses are those of conventional extinguishment-agent discharge and compartment venting. Partial evacuation followed by agent discharge is suggested as a very efficient method of combating a difficult fire, a technique worthy of further consideration.

7. Agent Transport in Low Gravity

An effective means of agent delivery in low gravity has never been determined. Experimental and numerical studies can characterize the transport phenomena from the discharge outlets to the fire site. The results can hold promise for improved specifications for extinguishing applications, covering gaseous and mixed phase agents.

8. Fire-Related Emissions

Emissions and their toxic effects are relevant to the assessment of fire response. By-products from the fire event can include not only pyrolysis and combustion products, but also those from suppressant decomposition.

9. Extinguishing Agent Performance in Low Gravity

There is almost a complete lack of information on the performance of extinguishing agents in microgravity and other reduced gravity environments. Performance includes the efficiency (quantity required) of extinguishment, the sustaining power (time of application), and other criteria. Research must cover a range of current and potential future agents, including gases, liquids, powders, and mixed phases.

10. Agent Distribution

In addition to the determination of extinguishing agent performance, necessary research must include the investigation and assessment of the spatial distribution of agents. These data will serve to optimize flow rates, predict the thermodynamic state of the agent, and establish the range of agent application. The scope of this research must include fixed and portable extinguishing systems, centralized and distributed systems, local and general applications, and streaming and flooding discharge.

11. Agent/Fire Interaction

This necessary research covers the behavior of the suppressant entering and within the combustion zone, raising the issue of the determination of such transport issues as diffusion. It is almost certain that gravity will affect this interaction, and models and verifying experiments are necessary for low-gravity predictions.

12. Post-Fire Sampling and Characterization

Existing rules include criteria for determining that a fire is “out” for discontinuing fire response and reentry into the affected zone. These regulations are based on ground experience exclusively. Low-gravity research is essential for the definition of the end of a fire, to assure safe entry, conserve extinguishing agent, and prevent re-ignition. Predictions from research should establish improved atmospheric sampling techniques and diagnostics for these criteria.

13. Obscuration Mitigation

Both flaming and smoldering fire may generate smoke, quickly filling the confined volume of a spacecraft. Smoke may be both a hazard and a nuisance, but the major concern is the obscuration, impeding entry, control, or escape. Predictive data are important, covering the special environments of the low-gravity spacecraft. Research can lead to mitigating technology, including crew equipment to accommodate the obscured environment (smoke hoods, for example).

As evidenced by the above list, fire response requires input from the topics areas addressed by the other two working groups. For example, to properly respond to a fire, you have to first know what is burning (material flammability) and how long it has been burning (material flammability, time between initiation and detection). This implies knowing the specifics about material configuration, locations of

ignition sources, flow conditions, etc. The working group decided that this information is essential to determining a proper fire response and should be included in their analysis as part of determining the initial conditions to any fire response. Because of the short time allotted for this analysis, the working group did not further combine or prioritize their thirteen research topics. However, these topics are not unrelated and can be categorized into three general areas as follows:

Specifications of the Conditions Prior to the Response

To assess a fire response strategy, information about the expected type, size, and location of the fire is required. The research topics that address this general theme are:

1. Digital Compartment Configuration Documentation
2. Evaluation of Potential Fire Locations and Scenarios
3. Experimental Determination of Flow in Compartments
4. CFD Representation of Flow in Compartments
5. Characterization of Fire Events

The computational and experimental determination of flow in a compartment is required to understand the initial conditions of the flow field where a fire may occur and the regions that would be affected by the discharge of a suppressant. Also, details of the flow field are required to determine the rate of flame spread and the path of smoke transport. From this, the time from fire initiation to detection can be estimated. Knowing the type of fire, the possible ignition source, flame spread rate, and time to detection, an estimate of the size of the fire what the automated and crew response procedures begin can be obtained.

Evaluation of Fire Suppressants

Once a fire has been detected and an alarm has sounded, the automated and/or crew fire response begins. There are different types of responses and the ability to determine their relative effectiveness for various fire scenarios is an important step in minimizing equipment damage and reducing the amount of clean-up required. The research areas that address this theme are listed below:

1. Agent Transport in Low Gravity
2. Extinguishing Agent Performance in Low Gravity
–Agent/Fire Interaction
3. Gaseous and Particulate Emissions from Fires and Suppressants

Effectiveness of Fire Response Strategies

Knowing the effectiveness and behavior of individual suppressant agents, various response strategies and be proposed and evaluated. The research areas required for this theme include:

1. Development of Fire-Response Concepts
–Obscuration Mitigation
2. Agent Distribution Requirements and Behavior
3. Post-Fire Sampling and Characterization

Summary and Conclusions

Even though the working group did not specifically prioritize the research topics, the categories listed above imply a sequence of research areas required for the development of effective fire response strategies for manned spacecraft. An area that was repeatedly emphasized by the working group during its discussions was that an appropriate response could be defined only as well as the “initial conditions” of the fire were known. This includes knowing the material being burned, the location and size of the fire, and the ambient conditions (O_2 concentration and velocity, for example). Some of this is addressed by

research identified by the other two working groups. The areas that are not addressed, such as knowing the ambient conditions when a fire starts constitute high-priority research areas specific to fire response.

Spacecraft Fire Safety Research Plan

Upon obtaining the above lists and prioritizations from experts in various aspects of fire safety, it is important to meld the recommendations into a coherent research plan. As a result of this input, a research roadmap for spacecraft fire safety was prepared and is shown in Table 2. The tasks are divided into the three general areas mirroring the focus of the working groups, *i.e.*, fire prevention and material flammability, smoke and fire detection, and fire suppression. Work items and overall objectives were identified. While the roadmap shows research efforts over a ten-year period, the first tasks in each area are of the highest priority and work in these areas should be initiated immediately. Research in many of these areas has, in fact, begun since the workshop and the findings of these studies will be presented in future reports and workshops. Continuing research efforts will build on this initial work.

Many of the research areas identified in Table 2 are drawn directly from the recommendations and research priorities identified by the working groups during the workshop. Others have been refined from these recommendations based on results from on-going research. Of course, these research areas and topics will continue to evolve as plans are implemented and results are obtained to ensure that the most relevant and critical areas are continuously addressed.

Table 2. Spacecraft Fire Safety Research Roadmap

Technical Area	Time Frame		
	2001 - 2004	2004 - 2007	2007 - 2010
Flammability of Practical Materials	<ul style="list-style-type: none"> - Evaluate the potential for and behavior of deep seated fires in non-1g environments - Determine potential for autoignition and explosion of high-P gaseous oxygen 		Flammability measurements and correlation from normal-g to μg; new validated test methods for material ranking
	<ul style="list-style-type: none"> - Determine flammability and flame spread of plastic and composite materials in partial-g for variations in flow and imposed heat flux - Improved test methods to rank materials 	<ul style="list-style-type: none"> - Determine limiting O_2 and flow for flame propagation on practical materials in μg and partial-g - Determine the effects of sub-limit in-situ propellant concentrations in standard and enriched O_2 atmospheres on practical material flammability 	
Fire Signatures and Detection	<ul style="list-style-type: none"> - Develop component-level sensors for fire detection - Define and validate method to establish pre-fire and fire signatures of practical materials in 1g 	<ul style="list-style-type: none"> - Develop and demonstrate integrated sensor (chemical/smoke) - Establish pre-fire and fire signatures of practical materials in low g 	Data base for fire signatures and demonstration of new detection systems
Fire Suppression and Post-Fire Response	<ul style="list-style-type: none"> - Evaluate in-situ fire extinguishants - Develop model of flame growth and stability in practical configurations to extend applicability of data base and to guide design of new systems 		Experimental validation of fire suppressant performance, analysis and models of fire suppressant strategies in μg and partial-g
	<ul style="list-style-type: none"> - Integrate understanding of extinguishment strategy and flame behavior in non-1g environments through analysis and modeling - Fundamental and system-level trade-off studies of flame-suppression techniques 	<ul style="list-style-type: none"> - Analyze and test physical dispersion of suppressant and techniques for extinguishment - Test and validate flame suppression methods in enriched O_2 and exotic atmospheres 	

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Appendix—Plenary Presentations

Five presentations were delivered during the opening session of the workshop and are included in this appendix. The titles of the presentations and the speakers were as follows:

1. *Research Needs in Fire Safety for the Human Exploration and Utilization of Space*
Speaker: Dr. Gary A. Ruff, Spacecraft Fire Safety Project Scientist,
NASA Glenn Research Center
2. *Spacecraft Fire Safety: A Human Space Flight Program Perspective*
Speaker: Dr. Michael D. Pedley, ISS Materials and Process Manager,
NASA Johnson Space Center
3. *Control of Materials Flammability Hazards*
Speaker: Dr. Dennis E. Griffin, Chemistry Group Leader, Materials, Processes, and
Manufacturing Department, NASA Marshall Space Flight Center
4. *Overview of ISS U.S. Fire Detection and Suppression System*
Speaker: Alana Whitaker, ISS ECLS Subsystem Manager, Fire Detection and Suppression
Systems, NASA Johnson Space Center
5. *An Introduction to Mars ISPP Technologies*
Speaker: Dr. Dale E. Lueck, Systems Engineering and Analysis Branch, Spaceport Engineering
and Technology, NASA Kennedy Space Center

Research Needs in Fire Safety for the Human Exploration and Utilization of Space

Dr. Gary A. Ruff
Spacecraft Fire Safety Project Scientist
NASA Glenn Research Center


National Aeronautics and Space
Administration
John H. Glenn Research Center





Workshop on
Research Needs in Fire Safety
for the
Human Exploration and Utilization
of Space

Hosted by
NASA John H. Glenn Research Center
and the
National Center for Microgravity Research in Fluids and Combustion

Sheraton Airport Hotel
Cleveland, Ohio
June 25 - 26, 2001


National Aeronautics and Space
Administration
John H. Glenn Research Center

Background



- **Last Spacecraft Fire Safety Workshop was held August 20-21, 1986**





National Aeronautics and Space
Administration
John H. Glenn Research Center

Background

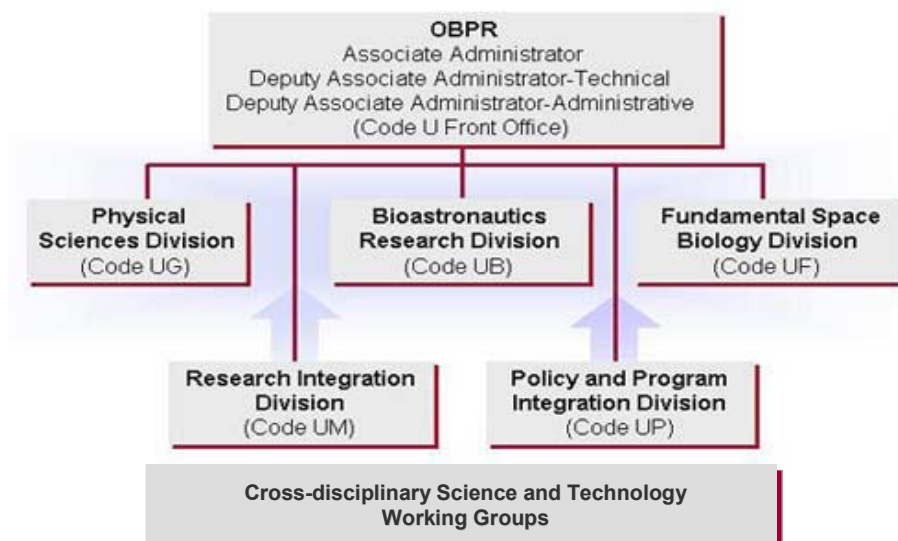


- **Last Spacecraft Fire Safety Workshop was held August 20-21, 1986**
 - Challenger accident 8 months earlier
 - Space Station designs underway
- **107 people, 5 break-out forums**
 - Fire detection and ignition
 - Fire extinguishment
 - Human responses to combustion products and inert atmospheres
 - Spacecraft materials and configurations
 - Selection of spacecraft atmospheres
- **Objectives**
 - Review current knowledge in fire safety
 - Assess the needs relevant to spacecraft
- **Microgravity combustion research conducted since 1986 has impacted fire safety practices on STS and ISS**



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Office of Biological and Physical Research



- **In mid-1999, the Space and Life Sciences Directorate at Johnson Space Center was challenged to develop a new paradigm for NASA human life sciences**
 - Space Medicine
 - Space Biomedical Research and Countermeasures
 - Advanced Human Support Technology
- **A new thrust - *Bioastronautics* - was formulated with a budget augmentation request**
- **Objective:**
 - Expanded extramural community participation through the National Space Biomedical Research Institute
 - Initiated the detailed planning and implementation of Bioastronautics
 - *An Integrated Approach to Ensure Healthy and Safe Human Space Travel*
 - *Assist in the Solution of Earth-based Problems*

- **Builds upon previous and ongoing work**
 - A significant amount of fundamental knowledge has been created through ground and flight research
 - Apply this knowledge base to applications and solutions which will provide safer human operations in space
- **Utilizes new research resources**
 - ISS/STS research opportunities
 - Ground analogs
- **Leverages new and unique capabilities**
 - Scientific community to focus on NASA issues
 - Transfer knowledge to Earth based problems
 - Cooperate with other Federal Agencies
 - Develop new technologies
 - smart medical systems
 - biologically-inspired technologies
 - fire protection

- **Substantially improve spacecraft fire safety within six years**
 - \$1M per year for four years (initial funding level)
 - Grant-based through NRAs and directed research
- **Fire safety practices and procedures**
 - ISS and Shuttle operations
 - Prolonged human-crew missions in Earth orbit and beyond
 - Lunar and/or Martian habitats
 - In-situ resource utilization
 - Propellant manufacture and storage

- **Identify research needed for fire safety of STS, ISS and their payloads**
- **Identify fire safety concerns for prolonged human-crew missions in Earth orbit and beyond**
- **Anticipate research for future Lunar/Martian habitats**

Approach

- **Plenary session to overview current operations and issues in fire protection in space**
- **Working groups to review current research and identify needs in the areas of**
 - Fire prevention and material flammability
 - Smoke and fire detection
 - Fire and post-fire response

Plenary Speakers



- **Dennis Griffin**
 - Group Leader, Chemistry Group
Materials, Processes, and Manufacturing Department
NASA Marshall Space Flight Center
- **Michael D. Pedley**
 - ISS Materials and Processes Manager
NASA Johnson Space Center
- **Alana A. Whitaker**
 - ISS Environmental Control and Life Support Systems
Fire Detection and Suppression Department
NASA Johnson Space Center
- **Dale E. Lueck**
 - Systems Engineering and Analysis Branch
Spaceport Engineering and Technology
NASA Kennedy Space Center

Working Groups



- **Fire Prevention and Material Flammability (O'Hare Room)**
 - James T'ien, Case Western Reserve University
 - Dennis Griffin, NASA Marshall Space Flight Center
- **Smoke and Fire Detection (Dulles Room)**
 - David L. Urban, NASA Glenn Research Center
 - Thomas Cleary, National Institute of Standards and Technology
- **Fire and Post-Fire Response (Hartsfield Room)**
 - Robert Friedman, NASA Glenn Research Center
 - J. Michael Bennett, Wright-Patterson Air Force Base
- **Sessions will begin with introductions and short presentations of current research**
 - Begin discussions of mission-driven fire protection systems within these areas
 - Recognize current knowledge and identify unknowns
 - Define research needed to fill gaps
 - Prioritize by short and long term, if applicable



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Schedule



Monday, June 25

Event	7:00 AM	8:00 AM	8:30 AM	9:00 AM	9:30 AM	10:00 AM	10:15 AM	10:45 AM
Plenary (Grand Ballroom)	Registration/ Continental Breakfast (Grand Ballroom)	Welcome Ruff, Ostrach	Materials Testing and Certification Griffin NASA MSFC	Spacecraft Fire Safety: A Human Space Flight Program Perspective Pedley NASA JSC	ISS Fire Protection and the ECLSS System Whitaker NASA JSC	Break (Grand Ballroom)	In-Situ Propellant Manufacture and Storage Lueck NASA KSC	Charge to Working Groups Ruff
Fire Prevention and Material Flammability (O'Hare Room)	11:00 AM Moderators: T'ien, Griffin Presentations: Torero, Fernandez-Pello Olson	Lunch (Lambert Room)	1:30 PM Working Session	3:30 PM Break (Grand Ballroom)	4:00 PM Working Session	6:00 PM Cash Bar (Lambert Room)	6:30 PM Dinner (Lambert Room)	
Smoke and Fire Detection (Dulles Room)	Moderators: Urban, Cleary Presentations: Urban, Hunter, Young		Working Session		Working Session			
Fire and Post-Fire Response (Hartsfield Room)	Moderators: Friedman, Bennett Presentations: Ross, Takahashi, Abbud-Madrid		Working Session		Working Session			



National Aeronautics and Space
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Schedule



Tuesday, June 26

Event	7:00 AM	8:00 AM	9:00 AM	9:45 AM	10:30 AM	10:45 AM	11:30 AM	11:45 AM
Plenary (Grand Ballroom)	Continental Breakfast (Grand Ballroom)		Fire Prevention and Materials Summary	Smoke and Fire Detection Summary	Break (Grand Ballroom)	Fire and Post-Fire Summary	Closing Ruff	Lunch/Completion of Written Summaries (Working Group Leaders) (Lounge)
Fire Prevention and Material Flammability (O'Hare Room)		Working Session Wrap-up						
Smoke and Fire Detection (Dulles Room)		Working Session Wrap-up						
Fire and Post-Fire Response (Hartsfield Room)		Working Session Wrap-up						

Summary Presentations



General Topic



- **Current level of understanding**
- **Desired improvement or level of knowledge required**
 - If possible,
 - Near-term
 - Long-term
- **Recommendations for research within this topic**
- **Other Considerations**
 - Enabling technologies
 - Impact on current procedures or future designs
 - Technology transfer/technology teaming opportunities
 - Who is the User?
 - Desired format

Written Report



- **Introduction**
 - Conduct of the group
 - Decision/discussion process
- **Current Technology Issues**
 - Issue 1
 - Knowns and unknowns
 - Issue 2
- **Research Areas**
 - Major Areas
 - Near-term
 - Mid-term
 - Enabling technologies
 - Technology teaming possibilities
 - Format of information desired by user

Dr. Michael D. Pedley
ISS Materials and Process Manager
NASA Johnson Space Center



Research Needs in Fire Safety for the Human Exploration and Utilization of Space


SPACECRAFT FIRE SAFETY

A HUMAN SPACE FLIGHT PROGRAM PERSPECTIVE

Michael D. Pedley
ISS Materials and Processes Manager
NASA Johnson Space Center


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Research Needs in Fire Safety for the Human Exploration and Utilization of Space

TYPICAL MANNED SPACECRAFT MATERIALS



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TYPICAL MANNED SPACECRAFT MATERIALS

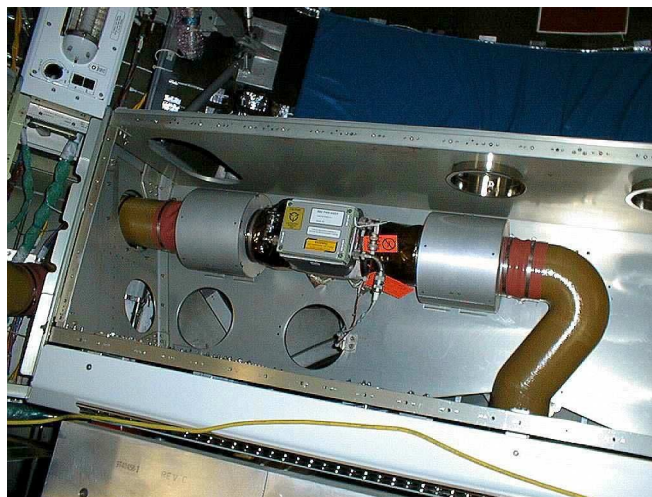


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TYPICAL MANNED SPACECRAFT MATERIALS



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TYPICAL FLAMMABLE HARDWARE PROTECTION



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MATERIALS FLAMMABILITY

- Current ground-based testing conservative but not intolerably restrictive for Shuttle/ISS environments – adequate supply of nonflammable materials for vehicle design to 30% oxygen environment
- Long-term need to quantify “conservative”
 - Relax ISS flammability requirements for payloads, clothing, portable equipment accordingly
 - Future manned space exploration missions extremely weight limited – very desirable to minimize use of nitrogen as consumable by returning to Apollo/Skylab oxygen concentrations

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FIRE RETARDANTS

- **Need a good and easy fire retardant treatment for fabrics (cotton, paper, synthetics)**
 - No significant changes in weight/feel of material,
 - Impervious to washing, dry cleaning
 - Odorless
- **Have to compete with current practice of allowing 100% cotton outer clothing (flammable)**
 - Commercially available fire retardants tried with little enthusiasm from crew
 - stiff, dry-clean only, slight odor



NONFLAMMABLE FOAM CUSHION MATERIAL

- **No good nonflammable foam cushion material**
 - Current choices are Pyrell fire-retardant polyurethane (flammable and life-limited) and Minicell polyethylene foam (more flammable but not life-limited)
 - Both weigh about 2 lb/cu. ft. and are very inexpensive
- **Desired cushion material would have following properties**
 - Nonflammable to at least 30% oxygen
 - Lightweight – preferably appreciably less than 2 lb/cu. ft.
 - Not life-limited – life 30 years +
 - Minimal compression set
 - High resilience, tear resistance
 - Negligible particulate formation
 - Open cell for vacuum compatibility
 - Very inexpensive
 - Easy to cut into complex shapes



NONFLAMMABLE FOAM CUSHION MATERIAL **-- EXISTING CANDIDATES**

- **Polyimide Foams (Solimide)**
 - Very lightweight (0.5 lb/cu. ft.), nonflammable in 30% oxygen, not life-limited, open cell
 - Very poor compression set, significant particulate generation, poor “feel”
 - Difficult to cut without generating considerable particulate
 - Very expensive
- **Melamine Foams**
 - Very lightweight (0.5 lb/cu. ft.), nonflammable in 30% oxygen, not life-limited, open cell, reasonable compression set
 - Minimal particulate generation but appreciable fine dust
 - Poor resilience, very poor tear resistance
 - Very difficult to cut complex shapes or thin slices
 - Very inexpensive
- **Silicone Foams**
 - Expensive, very heavy (at least 6 lb/cu. ft. for adequate resilience)



ELECTRICAL WIRE AND CABLE

- **Critical component from fire safety standpoint, because electrical power is only really credible ignition source (excepting solid-fuel oxygen generators)**
- **Key features**
 - Nonflammable to 40% oxygen, resists arc-tracking
 - High resistance to mechanical damage (abrasion, nicks, cuts)
 - High flexibility
 - Lightweight and capable of operating at high temperatures (at least 200 °C)
- **No perfect construction**
 - Teflon is heavy and has poor damage resistance
 - Kapton is stiff, has very poor arc-tracking resistance, is easily damaged by nicks, and may degrade in humid environments
 - Tefzel is flammable in enriched oxygen, has limited life above 150 °C and modest damage resistance
 - Teflon-polyimide hybrids currently best compromise for most applications but some aspects inferior to Kapton and others inferior to Teflon



RUSSIAN SOLID-FUEL OXYGEN GENERATOR (SFOG)



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GOX IGNITION MECHANISMS

- Two important areas of limited understanding with respect to materials ignition and combustion in oxygen systems
- In recent years, several oxygen system fires have been attributed to a phenomenon christened (possibly erroneously) as “flow friction”
 - Occurs only at high pressures (> 2500 psia)
 - Occurs in pressurized static systems (all other known ignition mechanisms are tied to motion – rapid pressurization, particle impact, friction)
 - Appears to result from leakage through a seal
 - Ignition mechanism not understood, so cannot be controlled by design/materials selection
- Limited studies of particle impact ignition have shown that high flow velocities are required and that metallic particles are probably worse than nonmetals – but we don’t know in any detail:
 - Velocity effects for different particulate contaminants
 - Effects of particle size and quantity
 - Effectiveness of filters as protection (as functions of filter size and filter material)
 - True hazards from gas streams exiting valve seats/orifices at sonic velocity

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FIRE DETECTION

- **Need capability to distinguish between pyrolysis event and true self-supporting combustion**
 - **Pyrolysis events relatively commonplace and inevitable (electrical shorts, component failures, arcing/arc tracking)**
 - **No true fires on orbit, excepting SFOG, combustion experiments**
- **Needs to have high reliability, no false positives**
- **Solve conundrum of**
 - **Air flow needed for to transport smoke, combustion products to traditional sensors for fire detection**
 - **Air flow worst thing for microgravity fires**



FIRE SUPPRESSION

- **Fire suppression capability always for backup only, but needs to be effective backup**
- **Issues with Halon-type extinguishers include:**
 - **ECLSS compatibility**
 - **Extinguishant toxicity**
 - **Effectiveness at elevated oxygen concentrations**
 - **Environmental**
- **Issues with carbon dioxide (ISS baseline) include:**
 - **Application (where is base of flame?)**
 - **Induced forced convection (will carbon dioxide application extinguish a microgravity fire or stir it up?)**
 - **Mixing (obtaining adequate concentrations in racks)**
- **Issues with water-based suppressants (includes Russian segment ISS baseline) include:**
 - **Compatibility with electrical systems**
 - **Clean up**
 - **Use in racks (application to fire source, clean-up)**

Dr. Dennis E. Griffin
Chemistry Group Leader
Materials, Processes, and Manufacturing Department
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MSFC Materials,
Processes, &
Manufacturing
Department



Control of Materials Flammability Hazards

Dennis E. Griffin
Chemistry Group Leader
NASA/Marshall Space Flight Center
Materials, Processes, and Manufacturing Department

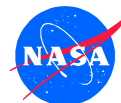
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Department

Control of Materials Flammability Hazards



- Fire is one of many potentially catastrophic hazards associated with materials used in the operation of manned spacecraft
- Appropriate materials selection and control of flammable materials is an important element of NASA's approach to fire control
- Major lesson learned from the Apollo 204 fire in 1966 was ignition sources can be minimized but never completely eliminated
- Spacecraft fire control is based on minimizing potential ignition sources and "eliminating materials that can propagate fire"
 - This means controlling quantity and configuration of flammable materials to eliminate potential fire propagation paths and ensure any fire would be small, localized, isolated and would self-extinguish without harm to the crew
- Fire extinguishers are always provided on manned spacecraft but are not considered as part of the fire control process

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Control of Materials Flammability Hazards (continued)



- Ground-based flammability testing is conservative but has not proven to be unusually restrictive for materials in manned spacecraft environments
 - Adequate sources of nonflammable materials for vehicle design
- Many solutions have been developed for controlling the configuration of flammable materials and materials in commercial “off-the-shelf” (COTS) hardware so that they can be used safely in manned spacecraft
- NSTS 22648, “*Flammability Configuration Analysis for Spacecraft Applications*,” describes these design solutions so customers can design safe and cost-effective flight hardware
- Current processes for controlling materials flammability hazards have successfully assured space flight materials and systems do not constitute an uncontrolled fire hazard
- Materials control processes include requirements, guidelines, testing, data bases, data requirement submittals, design analyses, deviation evaluation, hazard mitigation, verification, approval and certification

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Spacecraft Fire Safety Workshop

Dennis Griffin 3

Flammability Requirements



- All flight hardware used in NASA manned space programs must comply with the flammability requirements of NASA-STD-6001, “*Flammability, Odor, Offgassing, and Compatibility Requirements and Test Procedures for Materials in Environments That Support Combustion*”
- Establishes NASA program requirements for evaluation, testing and selection of materials to preclude unsafe conditions related to flammability in the following environments:
 - Habitable flight compartments (internal)
 - Locations outside habitable areas (external)
 - Ground Support Equipment (GSE) and specified test facilities
 - Vented and sealed containers
 - Liquid and gaseous oxygen (LOX/GOX)
 - Breathing gases
- NASA-STD-6001 describes required flammability tests and requires a system flammability evaluation for materials that fail these tests

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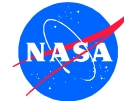
Dennis Griffin 4

Flammability Requirements (continued)



- NASA-STD-6001 contains several materials flammability and ignition tests:
 - Test 1 - Upward Flame Propagation (fundamental test for solid materials)
 - Test 2 - Heat and Visible Smoke Release Rates (cone calorimeter)
 - Test 3 - Flash Point of Liquids (ASTM D 93 Pensky-Martens closed tester)
 - Test 5 - Electrical Connector Potting & Conformal Coating Flammability (deleted)
 - Test 4 - Electrical Wire Insulation Flammability (15° inclined @ 125°C/ overload)
 - Test 8 - Flammability Test for Materials in Vented or Sealed Containers
 - Test 10 - Simulated Panel or Major Assembly Flammability (configuration Test 1)
 - Test 11 - Simulated Crew Bay Configuration Flammability Verification (deleted)
 - Test 13 - Mechanical Impact for Materials in Ambient/Pressurized LOX/GOX
 - Test 14 - Pressurized Gaseous Oxygen (GOX) Pneumatic Impact for Nonmetals
 - Test 17 - Upward Flammability of Materials in GOX (only for pressurized O₂ sys.)
 - Test 18 - Arc Tracking (for electrical wire insulation - not true flammability test)

Flammability Requirements and System Evaluations



- Nonflammable – a material that self-extinguishes within 6" when ignited and does not propagate a flame by transfer of burning debris (for at least 3 standard sized samples)
- Standard chemical ignition source – energy 750 ± 50 cal., temperature $2000 \pm 160^\circ\text{F}$, burning duration 25 ± 5 sec., flame height 2.5 ± 0.25 "
- "Worst-case" anticipated use environment (most hazardous pressure, temperature, material thickness, and fluid exposure conditions) must be used in the testing and evaluation process
- Materials shown to meet the acceptance criteria of the required test(s) are acceptable for further consideration in design
- Systems containing materials that have not been tested or do not meet the criteria of the required test(s) must be verified acceptable in the use configuration by analysis or testing
- Fundamental requirements is for overall system to be safe from a flammability standpoint
- Test methods exist to provide data needed to support systems evaluation

Flammability Requirements and System Evaluations (continued)



- An acceptable alternative to flammability testing is to assume material is flammable and demonstrate by analysis that the material configuration cannot propagate fire (e.g. for COTS hardware and electronic equipment)
- These requirements are implemented through various NASA program and Materials and Processes (M&P) requirements documents:
 - JSC SE-R-0006/MSFC-STD-506, *General M&P Standard (Shuttle)*
 - SSP 30233, *Space Station Requirements for M&P (ISS)*
 - NSTS 1700.7, *Safety Policy & Requirements for Payloads Using the Space Transportation System* and (same requirements in the) *ISS Addendum*
- NSTS 1700.7 tailors the NASA-STD-6001 requirements by exempting payload materials used in small quantities (less than 0.1 lb. or 10 square inches in manned crew environments and less than 1 lb. and/or 12 linear inches for external materials)
- Hardware containing materials that do not meet flammability requirements require Board approval with acceptance rationale and system evaluation documented in Materials Usage Agreements (MUAs) or Hazard Reports

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System Evaluations and Environments



- Systems flammability evaluations or oxygen hazards analyses are required consistent with the hazards assessment guidelines and requirement of:
 - NSTS 22648, *Flammability Configuration Analysis for Spacecraft Applications*
 - NASA TM 104823, *Guide for Oxygen Hazards Analyses on Comp. and Systems*
 - NSS 1740.15, *Standard for Oxygen and Oxygen Systems, Guidelines for Design*
- Standard rationale codes (for Class III MUAs) are available for the most common acceptable configurations containing flammable materials
- Approval of hazard assessments documented in M&P Certification
- Materials flammability depends strongly on the oxygen concentration in the environment to which the materials will be exposed (the effect of pressure is much smaller and can be ignored at crew cabin pressures < 1 Atm)
- Past NASA programs used much higher oxygen concentrations than the current 30% maximum for ISS/Shuttle (100% for Apollo and 70% for Skylab)
- Configurations found to be acceptable under higher oxygen concentrations are considered acceptable for lower oxygen concentrations

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System Evaluations



- When a flammability assessment results in an unacceptable configuration reduction of flammability hazards is necessary to correct the problems
- Primary methods used by NASA to reduce flammability hazards are:
 - Minimize or limit the use of flammable materials by replacement with nonflammable materials
 - Eliminate or restrict propagation paths
 - Covering flammable material with a nonflammable material
 - Separation of flammable materials
 - Isolate flammable materials from ignition sources or eliminate ignition sources
- When results of flammability configuration analysis are inconclusive the hardware configuration may be tested for flammability to determine acceptability
- Alternatively the hardware organization may choose to assume the configuration is flammable and implement appropriate measures to eliminate the flammability hazard

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System Evaluations (continued)



- To conduct a flammability configuration assessment - **Evaluate the overall hardware configuration:**
 - If the hardware is a closed box without vents or power, the materials inside will not contribute to the fire hazard unless the box is constructed from flammable materials – the box acts as a fire barrier
 - If the only electrical power within the box is from batteries, the maximum short-circuit power draw is nearly always too low to act as an ignition source
 - NASA testing during the Apollo era showed that solid materials cannot be ignited by electrical powers below 25 watts
- **Evaluate the way in which the hardware will be used:**
 - Hardware that is normally stowed in a fireproof container (stowage locker, many NASA provided stowage bags and ISS crew transfer bags) and exposed to the cabin environment for short periods during use may comply with stowage policy:
 - Max dimensions 10 in. and unstowed less than 1 day/week
 - Unstowed less than 1 hour/day
 - Contingency use only

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System Evaluations (continued)



- Maximum dimension <6 in. and always stowed when not in actual use
- Used only when covered by crew clothing
- Exposed surface area < 1 sq. ft. and always worn by crew when unstowed
- A full flammability analysis is required for hardware that is permanently mounted in a rack or a locker space
- **Identify the major materials to be assessed**
 - Amounts greater than 0.1 pounds (or 6 linear inches maximum dimension and/or 10 square inches maximum area) in crew-habitable compartments
 - Amounts greater than 1.0 pounds (or 12 linear inches) in other compartments
 - Metallic panels and structures are nonflammable in Shuttle/ISS environment (even magnesium and titanium) and need not be considered
 - Metallic screens may be flammable and must be addressed
 - Inorganic materials (ceramics) are also nonflammable in Shuttle/ISS environments and need not be considered
 - Adhesives (sandwiched between two surfaces) and materials covered overcoated by nonflammable materials need not be considered

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System Evaluations and Flammability Data



- Flammability characteristics of materials can be determined by consulting the NASA/MSFC Materials and Processes Technical Information System (MAPTIS) at http://map1.msfc.nasa.gov/WWW_Root/html/page7.html
- An A-rating in MAPTIS for test conditions that are the same as the use conditions means the material is acceptable in unlimited quantities
- Any other rating means the material quantity/exposure must be controlled
- Note the following key factors when using MAPTIS flammability data:
 - Oxygen concentration - MAPTIS flammability data obtained at higher oxygen concentrations than the use concentration are always conservative (unpowered and painted metal boxes, or hardware stowed/transferred in a standard locker, Shuttle container or crew transfer bag for external use are acceptable)
 - Material thickness – generally, flammability decreases with increasing thickness, so the thickness associated with the MAPTIS rating should be the same as the use thickness of the material, or it is acceptable if a thinner version of the same material is rated A for flammability

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System Evaluations and Flammability Data (continued)



- Coatings on substrates – thin coatings bonded or sprayed on metallic substrates are generally not flammable because the substrate acts as a heat sink, coating flammability always decreases with increasing substrate thickness, so a coating is always acceptable if it is A-rated for flammability on a thinner substrate, if the coating is <2 mils thick and the metal substrate is ≥ 20 mils thick the coating is acceptable, nonmetallic substrates are not effective as heat sinks
- Determine fire propagation paths
 - Determine whether the externally exposed materials represent fire propagation paths exceeding 6" in crew compartments and 12" in other areas, propagation from one flammable material application to the next is not acceptable, and must be limited by fire breaks or positive action to control the hazard
- Evaluate the ability of container to contain fire
 - Sealed containers have no vents and are verified to a max. of 1×10^{-4} cm³/sec
 - Contains no oxygen or inert gas an internal fire will not be initiated
 - Contains air and nonflammable wall ≥ 60 mils thick fire will be contained
 - Internal void space limited to less than 30% of total volume acceptable

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System Evaluations (continued)



- Vented containers have active vents and associated cooling airflow
 - Vent area <1% of total surface area and vents covered with a fine metal (stainless steel or nickel, not Al, Ti or Mg) screen will contain fire
 - Carefully evaluate/test and reduce hazard by:
 - Minimize number and size of vents (avoid chimney effect)
 - Cover vents with fine CRES or Ni screen
 - Minimize free volume by adding nonflammable packaging materials, e.g. polyimide foam
 - If forced air flow not required, cover all vents and evaluate as intermediate
 - Relation between flow rate and flammability complex
 - At low flow rates flammable materials burn more vigorously with increasing flow rate (decreasing effectiveness of the container)
 - At high flow rate airflow will prevent stable flames (blowing out fire)
 - Intermediate flow rates are worse case and are configuration and microgravity dependent

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System Evaluations (continued)



- Intermediate containers have no active vents or cooling airflow
 - NASA-provided stowage lockers and bags are treated as containers that can act as barriers to external fires
 - Many commercial electronics items may be addressed by stowage policy or can be obtained with metallic or nonflammable polycarbonate case and with internal components packed closely such that void space is of no concern
 - Internal ignition of small commercial items powered by alkaline batteries is not considered credible
 - Potential for ignition from external sources can be eliminated with nonflammable case or by covering the case with a nonflammable material

Processes to Control Materials Flammability Hazards



- **Elements of effective materials flammability control have successfully precluded uncontrolled fires on orbit:**
- Requirements - NASA-STD-6001 implemented by program requirements
- Guidelines - NSTS 22648, MSFC-PROC-1301, NSS 1740.15, etc.
- Testing – active program for new materials, applications & configurations
- Data bases - MAPTIS provides 85,000 test reports on >32,000 materials
 - Used to publish MSFC-HDBK-527/JSC 09604, *Materials Selection Lists for Space Hardware Systems*, all materials have unique NASA Material Code
- Data requirement submittals – Type 1 Approval, MCPs, MIULs and MUAs
 - Materials Control Plans – Describes how requirements will be implemented
 - Materials Identification Usage Lists – Identifies where specific materials are used, quantities, environments, application, thicknesses, cure, applicable test data, etc.
 - Materials Usage Agreements – used to approve materials that fail to meet requirements, describes application and hazard assessment with technical acceptance rationale for evaluation of deviation
 - Engineering Drawings

Processes to Control Materials Flammability Hazards (continued)



- Design review/approval – M&P approval signature required on all engineering documentation
- Design analysis – formal hazards analysis, inspections, walk-throughs
- Hazard mitigation – numerous techniques developed and documented
- Oversight/Insight – M&P approval signature and representation required for milestone design reviews (SRRs, PDRs, CDRs, DCRs), Safety Review Boards/Panels, Certification of Flight Readiness Reviews (CoFRs)
- Verification – data submittal, assessment and closure for generic flammability hazard, reconcile as-designed versus as-built configuration
- Materials and Processes (M&P) organization responsible for preparing and approving certification that materials meet flammability requirements for CoFR and Safety Panel
- Reciprocal Materials Agreements
 - JSC, MSFC, JPL, GRC, GSFC maintain Intercenter Materials Agreements
 - NASA, ESA, NASDA and RSA maintain Interagency Materials Agreements

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Flammability Reduction Methods



- Commercial items with flammable outer surfaces (ABS, PVC, polyethylene, and/or polyamides) may be wrapped in nonflammable tape
 - 3 mil aluminum tape (L-T-80) will protect most plastics, foams and cardboard
 - Nonflammable fiberglass tape with silicone adhesive will provide same protection if each rotation or wrap overlaps the previous one by 50%
- For long-term applications and aesthetics, flammable surfaces may be coated with nonflammable barrier such as Fluorel ® (expensive, complex, fair durability)
- Common case materials for commercial items are generally extremely flammable ABS or normally acceptable polycarbonate (up to 30%) or metal
- Electrically powered items with internal flammable materials can usually be treated or filled with a suitable material (nonflammable glass-filled-epoxy potting compound) to provide protection from internal ignition sources

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Wire and Cable



- Most aerospace-grade electrical wire insulation is nonflammable in Shuttle/ISS environments
- Limitations are usually driven by such factors as flexibility and cut-through resistance:
 - Teflon (MIL-W-22759, MIL-C-27500, or equivalent) – good general-purpose wire with high flexibility but poor cut-through resistance
 - Polyimide (MIL-W-81381) – no longer used except in flat circuits because of propensity to arc track
 - Teflon-Polyimide Hybrids (MIL-W-22759, MIL-C-27500, or equivalent) – good general-purpose wire with lower flexibility than Teflon but higher cut-through resistance
 - Tefzel (MIL-W-22759, MIL-C-27500, or equivalent) – suitable for external applications but flammable in enriched oxygen with performance similar to hybrid
 - ISS also uses a custom silicone-insulated construction in power circuits (SSQ 21652) that is nonflammable in ISS environments and exceptionally flexible

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Wire and Cable (continued)



- COTS hardware typically has electrical wiring with PVC, polyethylene, or chloroprene insulations which are flammable in all Shuttle/ISS environments
- Their use is generally discouraged and may be used only when demonstrated to be acceptable in configuration by flammability analysis
- Commercial wiring inside electronics boxes and low-power signal wiring outside such boxes can usually be accepted by this method
- External power cables nearly always need to be replaced or protected from ignition
- Flammable insulation is acceptable on wires in external payloads that are not powered (including during ground testing) until in vacuum

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Wire, Cable and Electrical Accessories



- Methods for protecting flammable cables include:
 - Covering with braided Teflon sleeve, such as Goretex ® sleeving
 - Wrapping with nonflammable fiberglass-backed-silicone adhesive tape
 - Covering with sleeve of 7.2 oz/yd² natural Nomex HT-9040 fabric, beta cloth, polybenzimidazole (PBI), or other nonflammable fabrics
 - Covering by heat shrinking polyvinylidene fluoride or Teflon sleeve onto cable
- Wire and cable accessories such as cable markers, spacers, and cable ties should not contribute to fire propagation paths
- Polyvinylidene fluoride/fluoroelastomeric cable markers are generally used
- Other types of cable marker material may be acceptable if used in small discrete amounts or covered with a clear Teflon TFE or FEP sleeve
- Most types of spacers are usually acceptable because of heat sink effects
- Acceptable lacing cords are Teflon TFE, Teflon TFE/fiberglass, or Nomex

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Electrical Accessories Hoses and Tubes



- Acceptable cable ties can be made from ETFE or ECTFE fluoropolymers
- If flammable cable tie wraps are used on nonflammable cables they should be spaced at least 2 inches apart to prevent fire propagation
- In air and moderately-enriched oxygen environments (up to 40 percent oxygen) the shell of a metal shell electrical connector prevents fire propagation from the nonmetallic materials used inside the connector to other nonmetallic materials, regardless of the material inside the connector
- Flammability configuration analysis is required for nonmetallic shell connectors
- Acceptability of the nonmetallic materials used inside the connector depends on the flammability of the shell material and its ability to act as a fire barrier
- External tubes or hoses (such as a vacuum cleaner hose) made from flammable materials may be replaced with a nonflammable material or covered with a fire barrier material

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Hoses and Tubes Hook and Loop Fasteners



- Clear TFE or FEP Teflon tubes and hoses are readily available to replace flammable materials
- If flammable tubes or hoses must be used, the exterior can be protected by a covering of 7.2 oz/yd² natural Nomex HT-9040, PBI, Beta cloth, or other nonflammable fabric
- In these cases potential for ignition of the tube walls from inside must be addressed
- Although some hook-and-loop fastener materials are less flammable than others, all common types are flammable in spacecraft habitable areas
- To prevent long flame propagation paths, the following usage limits are generally applied to hook and loop fasteners in habitable areas:
 - Maximum size: 4 square inches, individually or in pieces
 - Maximum length: 4 inches
 - Minimum separation distance: 2 inches in any direction from another piece
- NASA normally uses nylon fasteners in habitable areas for greater durability and Nomex in EVA operations for good low-temperature performance

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Stowage Bags and Lockers



- Metal stowage lockers that do not contain ignition sources are acceptable
- Material selection criteria for nonmetallic stowage lockers must be based on fire containment capability and should be supported by test data
- Acceptable stowage bags may be constructed from the following fabrics:
 - Beta cloth - acceptable for stowage of potentially flammable materials but has low durability and a tendency to shed glass fibers
 - Natural Nomex HT-9040 fabric weighing at least 7.2 ounces/square yard
 - Lighter weights of natural Nomex HT-9040 are acceptable in double layers
 - Navy blue single-layer Nomex weighing 6.5 ounces/square yard treated with ammonia dihydrogen phosphate fire retardant
 - Used on the Shuttle but discouraged for ISS because the fabric cannot be wiped down without removing the fire retardant
 - PBI and other flame-retardant fabrics (see MAPTIS)
- These containers can have flammable items stowed inside them provided they do not contain ignition sources and are not susceptible to spontaneous ignition or chemical reaction

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Thermal Control Blankets



- Thermal control blankets are the most widely used potentially flammable external materials
- Blankets typically contain 12 to 40 layers of film (0.0005 to 0.002 inches in thickness) separated by some type of scrim cloth
- Blanket materials are usually constructed of metal-coated polyethylene terephthalate or polyimide film with an organic separator scrim
- The inner and outer layers are generally heavier than the internal layers for durability
- Outer layer has controlled optical properties and is usually polyimide, silver-Teflon, or Beta cloth
- Acceptable thermal control blankets are typically constructed as follows:
 - The outer layer is made of nonflammable material such as polyimide film (at least 1.5 mil thick), metal foil, silver-Teflon, or Beta cloth
 - Internal layers can be a combination of flammable films or scrims
 - Edges are hemmed or suitably finished so that the inner flammable layers are protected and Atomic Oxygen is a consideration for long- term LEO exposure

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Fiber Reinforced Laminates



- Fiber-reinforced laminates are used as structural materials
- Laminates may be flammable if used in thickness < 0.125 inches
- Flammability characteristics of thin laminates should be verified by test or the laminates should be protected
- Flammable laminates may be used in external payloads provided that ignition sources (electrical wires, heaters, etc.) are not located within 6 inches of the laminates
- Otherwise firebreaks should be placed on the exposed surfaces of these laminates at 12 inch intervals, e.g. Aluminum tape 3 mils thick X 3 inches wide (Federal Standard L-T-80)

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Alana Whitaker
ISS ECLS Subsystem Manager
Fire Detection and Suppression Systems
NASA Johnson Space Center

Overview of ISS US Fire Detection and Suppression System

6/25/01

Alana Whitaker

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Outline

- Intro to Fire Detection and Suppression (FDS)
- Description of (FDS) Subsystems
 - Portable Fire Extinguishers (PFE)
 - PFE Testing
 - Smoke Detectors (SD)
 - Ventilation and Air Monitoring/Supply Systems
 - Portable Breathing Apparatus (PBA)
- FDS System Component Location and Status
- FDS System Capabilities

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Outline (cont.)

- FDS Automatic and Manual Response
- Post Fire Atmosphere Restoration and Air Quality Assessment
- FDS Research Needs

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Intro to FDS on ISS

- Fire Detection and Suppression (FDS) includes:
 - Detection of smoke
 - Isolation of fires
 - The means to extinguish fires
 - The means to recover from fires

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Portable Fire Extinguisher (PFE)



PFE w/Cover (config. on orbit)

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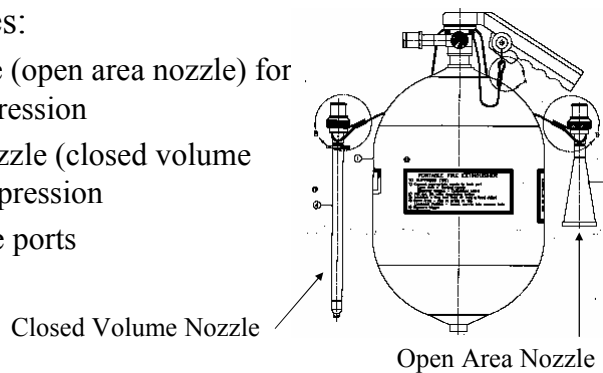
PFE w/o Cover

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Portable Fire Extinguisher (PFE)

- PFE Characteristics
 - Contains 6 lbs CO₂ at 850psi
 - Discharges in 45 sec.
 - Has two nozzles:
 - Conical Nozzle (open area nozzle) for open area suppression
 - Cylindrical Nozzle (closed volume nozzle) for suppression in closeout fire ports



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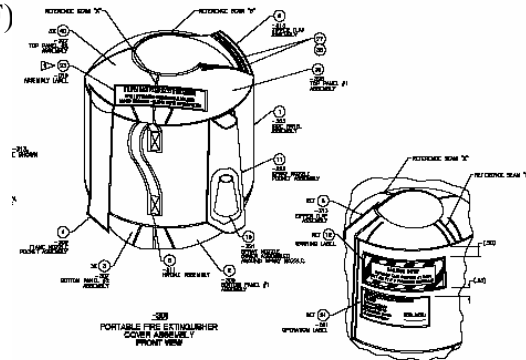
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PFE Cover

- PFE Cover Characteristics

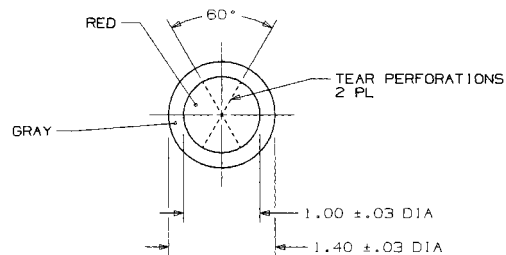
- Made of Nomex
- Fits snugly to PFE
- Keeps PFE within allowable touch temp. limits during discharge (w/o Cover, PFE reaches 0 deg. F and nozzle -32 deg. F)



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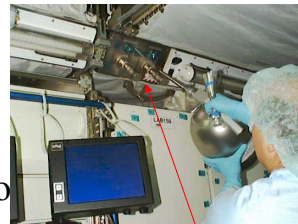
Fire Suppression Ports

- 1" or 0.5" diameter perforated access ports in racks and standoffs for the cylindrical nozzle (enclosed area nozzle) to suppress fires
- O₂ concentration in a rack is reduced to < 10.5% within 1 min of suppression.

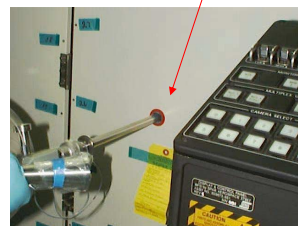


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Suppression port nozzle inserted
into suppression port



Fire Suppression Testing

- Enclosed Volume Tests (cylindrical nozzle)
 - All CO₂ sensors show > 50% concentration for volumes 60ft³ or less
 - Good mix in enclosed volumes
- Open Volume Tests (conical nozzle)
 - Fire is suppressed by a combination of blowing the fire out (3 lb mass in first 10 sec) and supplying CO₂.

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Smoke Detector



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Smoke Detector

- **Photoelectric Smoke Detector**

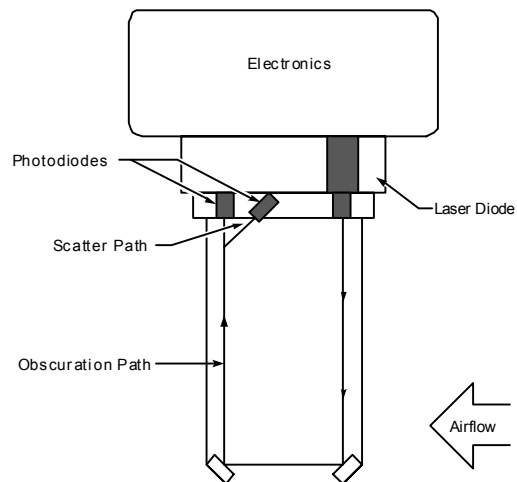
- Based on smoke particles scattering a light beam
- Light from a laser source is reflected by mirrors back to a photodiode (obscuration).
- Scattered light is measured by a second photodiode (scattering)
- Alarms are based on the voltage level generated by the scattering photodiode.

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Smoke Detector Principle



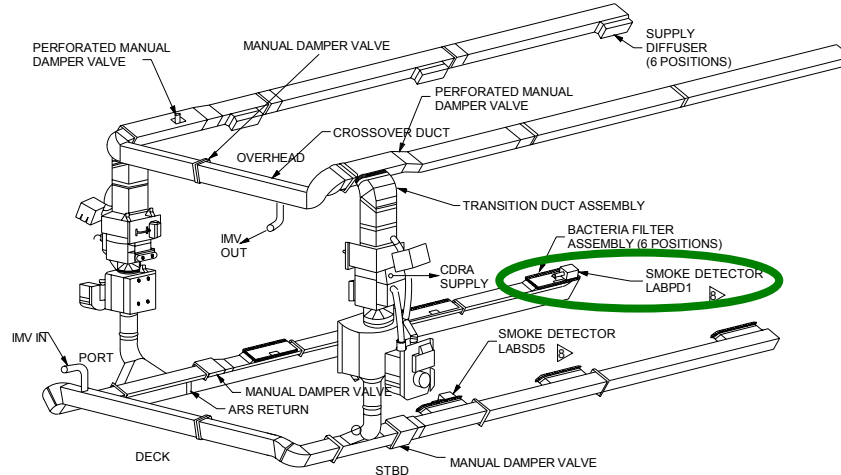
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Smoke Detectors in Ventilation

- Smoke Detectors are located on the ventilation filter intake ducts.



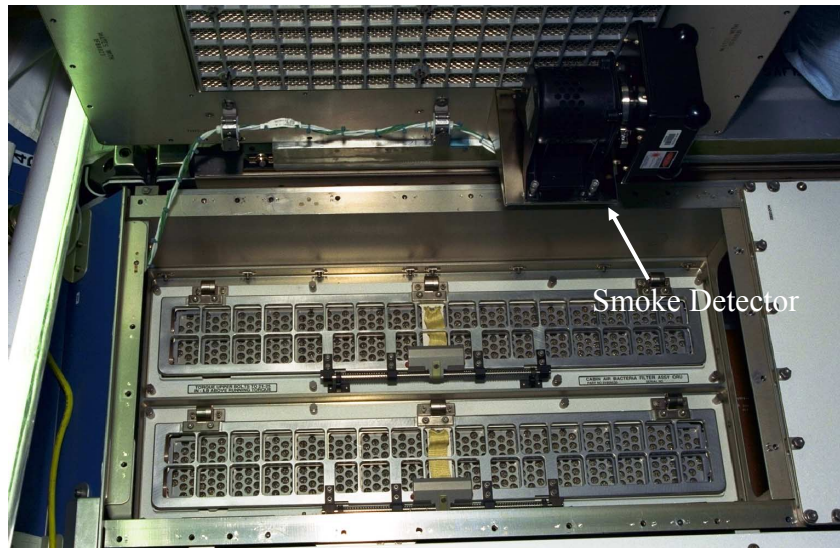
Lab Cabin Air Temperature and Humidity Control Assembly with Smoke Detectors

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Smoke Detectors in Ventilation



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Air Monitoring/Supply System

- Air components/concentrations are monitored by the Major Constituent Analyzer (MCA) in the LAB.
 - Air samples are taken from each module and routed to the sensor (mass spec.) in the MCA.
 - MCA gives percent compositions. (Typical O₂ levels on ISS are slightly less than 24%.)
- Metabolic O₂ and N₂ are supplied from Orbiter, Service Module, and Progress

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Total and Oxygen Partial Pressure Control Not In Campout Mode

- Pressure control when Not in Campout Mode (nominal) is done with closed-loop control
 - Total Pressure
 - The PCPs will be taking constant (1 Hz) total pressures
 - If the total pressure drops below 14.25 psia the Nitrogen Isolation Valve in the primary PCP will open
 - When the total pressure \geq 14.3 psia the Nitrogen Isolation Valve in the primary PCP will close
 - Oxygen Partial Pressure
 - The MCA will be making constant readings of the Station atmosphere
 - If the oxygen partial pressure drops below 3.00 psia the Oxygen Isolation Valve in the primary PCP will be opened
 - When the oxygen partial pressure \geq 3.05 psia the Oxygen Isolation Valve in the primary PCP will close

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Total and Oxygen Partial Pressure Control In Campout Mode

- While in Campout Mode, the ppO₂ in the Airlock will be controlled by the following:
 - If ppO₂ < 2.7 psia in the Airlock, the Airlock PCA will open the PCP OIV for 4 minutes +/- 10 seconds
 - If the ppO₂ > 2.85 psia in the Airlock, the Airlock PCA will open the PCP NIV for 2 minutes +/- 2 seconds
 - If either the PCP NIV or OIV was opened, wait 11 minutes after the valve closes
 - Repeat
- Total pressure control is via manual operation of the Depress Pump
- The rest of Station will continue to control total and oxygen partial pressures in the standard method

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Portable Breathing Apparatus (PBA)



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Portable Breathing Apparatus (PBA)

- PBA is composed of:
 - Mask
 - 15 minute O₂ bottle
 - 30' hose
- Provides O₂ to crew in emergency situations
 - Post-fire clean-up
 - Environmental contamination
 - Depressurization

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FDS System Component Location

- Node 1 – 2 area Smoke Detectors (SD), 1 (PBA), 1 (PFE)
 - Currently on orbit
 - PFE and PBA are nominal (have not been used)
 - SD#1 is powered, enabled, and nominal
 - SD#2 is powered and disabled
- Lab – 2 area SD, 2 system rack SD (AR rack, CHeCS rack), up to 13 experiment rack SD (3 experiment rack SD at 7A), 2 PBA, 2 PFE
 - Currently on orbit
 - PFEs and PBAs are nominal (have not been used)
 - 4 SDs (2 area and 2 rack) are powered, enabled, and nominal
 - 1 payload SD is powered, enabled, and nominal
 - 2 payload SDs operate intermittently based on payload operations

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FDS System Component Location

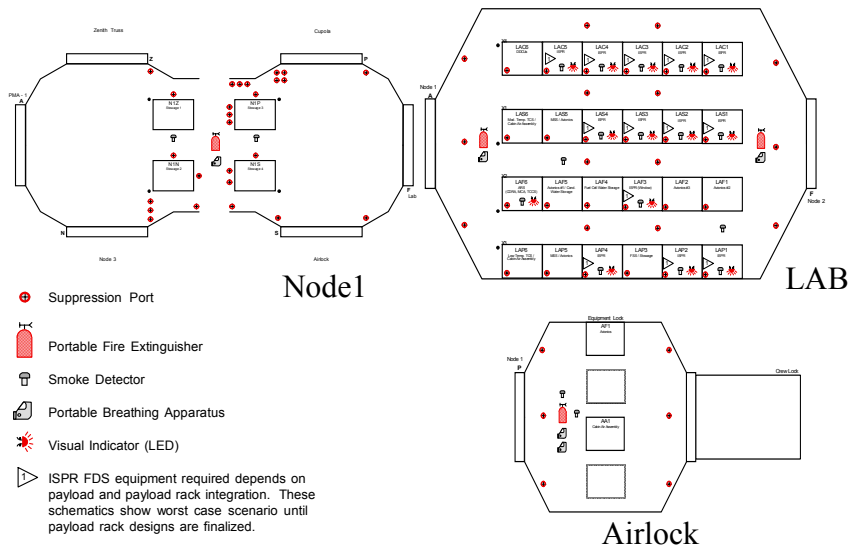
- A/L – 1 area SD, 1 duct SD, 2 Pre-breathe Hose Assemblies (PHA), 3 O2 bottles, 1 PHA spares kit, 1 PFE
- MPLM – 1 duct SD, 1 PFE, 1 PBA (PBA & PFE stored in Node1 when MPLM is not attached)

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FDS System Component Location



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FDS System Capabilities

- Node 1, Lab, A/L, & MPLM FDS
 - Fire emergency alarm received if any single SD FIRE status flag is set equal to “FIRE”
 - Scatter must exceed the fire threshold two consecutive times, the detector then initiates an active Built In Test (BIT), and the scatter must still be exceeding the threshold after the BIT to set the status flag equal to “FIRE.”
 - Location may be determined by laptop.

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FDS Automatic and Manual Response (Overview)

- In case of fire or smoke
 - The crew can manually push the fire alarm or the Smoke Detectors can automatically initiate the fire alarm to perform the following functions:
 - 1) Remove power to racks-to isolate ignition sources
 - 2) Isolate module by shutting off ventilation (close IMV valves, sample delivery systems, cabin fans)-to stop air flow within module and exchange between modules
 - 3) Inhibit introduction of O₂ and N₂ into module (inhibit pressure control assembly in LAB)

Crew can use PFE at their discretion

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Post Fire Atmosphere Restoration

- Gaseous Contaminants removed by the following:
 - **SM - Micropurification Unit(БМП)**
 - Removes 19 different gaseous contaminants using a catalytic oxidizer (ambient) and expendable & regenerative charcoal beds.
 - **FGB - Harmful Impurities Filter (ФВГ)**
 - Removes gaseous trace impurities (particles of 0.5 to 300 μ m to a level of 0.15 mg/m³).
 - **Lab - Trace Contaminant Control Subsystem (TCCS)**
 - Removes gaseous contaminants using a catalytic oxidizer (400°C) and expendable sorbent and charcoal beds. Sorbent contains LiOH which can remove acid gases.

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Post Fire Atmosphere Restoration

- **Carbon Dioxide Removal Assembly (CDRA)**
 - Removes CO₂ from the atmosphere that was discharged from the PFE
- **Extra charcoal air filters**
 - Scrub the environment and contain 2% Pt for CO removal.
- **CO₂ Removal Kit (CRK)**
 - Consists of a portable fan assembly with a LiOH cartridge adapter.
 - Can be used with LiOH or ATCO catalyst canister for CO₂ or CO removal
- **Venting module to space**
 - Only in worst case scenario

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Post Fire Air Quality Assessment

- Air quality analysis done with the following equipment:
 - Compound-Specific Analyzer for Combustion Products (CSA-CP)
 - Carbon Dioxide Monitoring Kit (CDMK)
- Final analysis using Draeger detector tubes
- Atmospheric sampling, using GSC and AK-1 air sampling assemblies, for delivery to ground.

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FDS Research Needs

- Data to support suppressant selection
 - Suppressant
 - Effective
 - Not harm ECLSS or other equipment
 - No/low toxicity
 - Not require extensive clean up
- Microgravity research on suppression of fire
 - Experiments needed on fabrics and items on orbit likely to burn

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??Questions??



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Systems Engineering and Analysis Branch
Spaceport Engineering and Technology
NASA Kennedy Space Center

An Introduction to Mars ISPP Technologies

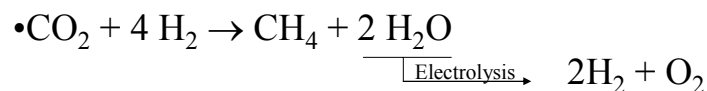
**Research Needs in Fire Safety
for the
Human Exploration and Utilization of Space**

June 25-26, 2001 Cleveland, Ohio

Dr. Dale E. Lueck NASA/John F. Kennedy Space Center

Background

- ISPP is an enabling technologies for HEDS missions to Mars.



(Sabatier Reaction with Water Electrolysis)

- Supplemental oxygen production required
 - $2 \text{CO}_2 \rightarrow 2 \text{CO} + \text{O}_2$

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A detailed 3D CAD model of a complex industrial machine, possibly a steam engine or a pump assembly. The model is rendered in a light gray, semi-transparent style, revealing internal components. It features several large cylindrical tanks or cylinders, a complex network of pipes and valves, and a central mechanism that could be a piston or a pump. The entire assembly is mounted on a base plate. The image is presented in a perspective view, highlighting the intricate design and mechanical layout of the system.

- # Sabatier Reactor Flow Chart
-
- The flow chart illustrates the Sabatier reactor system, which is a closed-loop process for producing and storing methane. The system includes the following components and flow paths:
- Sorption Pump:** Located at the top left, it maintains a high vacuum for the Sabatier reactor.
 - Go to Process Flow Sheet:** A button or label indicating the start of the process.
 - Sabatier Reactor:** The central component where the Sabatier reaction occurs, producing methane and water.
 - Hydrogen Recovery Pump:** Recovers hydrogen gas from the reactor effluent.
 - H₂O Separator:** Separates water from the hydrogen gas stream.
 - H₂O Dryer:** Removes residual water from the hydrogen gas.
 - Electrolysis:** Splits water into hydrogen and oxygen.
 - Hydrogen Storage:** Stores the recovered hydrogen gas.
 - Oxygen Storage:** Stores the oxygen gas produced by electrolysis.
 - Methane Storage:** Stores the methane produced by the Sabatier reactor.
 - Zirconia Cells:** Used for gas analysis or monitoring.
- The flow paths are as follows:
- Hydrogen gas from the **Hydrogen Recovery Pump** and **Electrolysis** is stored in **Hydrogen Storage**.
 - Oxygen gas from **Electrolysis** is stored in **Oxygen Storage**.
 - Water from the **H₂O Separator** is sent to the **Electrolysis** unit.
 - The **Electrolysis** unit produces hydrogen gas, which is then dried in the **H₂O Dryer**.
 - The dried hydrogen gas is fed into the **Sabatier Reactor**.
 - The **Sabatier Reactor** produces methane and water, which are then separated in the **H₂O Separator**.
 - The methane is stored in **Methane Storage**.
 - The water is sent to the **Electrolysis** unit.
 - The **Sorption Pump** maintains a high vacuum for the **Sabatier Reactor**.
 - The **Zirconia Cells** are used for gas analysis or monitoring.

Alternative Fuels?

- Methane requires 4 atoms of Hydrogen
- Lower hydrogen content improves ISPP weight savings ratio

	H/C	Tons H2
■ Methane	4	5.1
■ Ethane	3	4.7
■ Ethylene	2	3.4
■ Benzene	1	2.1

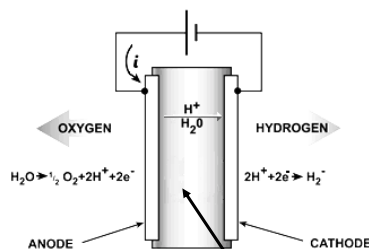
Fuels and Oxidizer

- ISPP saves weight by producing fuels on Mars (5 – 8 tons over H2 brought)
- Producing fuels other than methane is still in early development
- Producing oxygen saves 70+ tons for MAV oxidizer.
- Life support and mobile power further increases savings.

Oxygen Production

- All systems use electrolysis to produce oxygen
 - Electrolysis of water from a reactor
 - Direct electrolysis of CO₂
- Electrolytes can be water, non-aqueous liquids or solids.
- 4 e⁻ / O₂ molecule establishes current
- Operating voltage and temperature establish efficiency and materials of construction.

PEM Cell Electrolyzer Schematic



• Nafion is preferred PEM

• Platinum group metals used for electrodes, deposited on PEM

• Uses Proton Exchange Membrane (PEM) to separate H₂ and O₂

Electrolyzer Stack for Seawolf Submarine



- 100Cells/Stack (7 Cells / Inch)
- 50-kW (360 SCFH-H₂)
- High Current Density (1000 A/Ft²)
- Over 100,000 hours operation
- H₂ & O₂ at 3000 psi

Courtesy of J. Kosek, Giner, Inc.

Zirconia Solid Electrolyte Cell

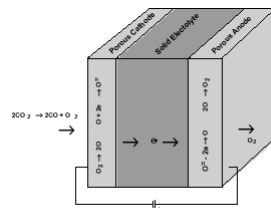


Figure 2. Principle of operation of a solid oxide electrolyzer.



Figure 3. Exploded view of an electrolyzer assembly.

Sridar, Gottmann, and Baird, AIAA Publication

Zirconia Pros and Cons

- Direct electrolysis of CO₂ with pure O₂ separated.
- Good efficiency, about 1.5 V, similar to water electrolysis.
- Very high operating temperatures, 800 - 1000°C.
 - All ceramic construction in high temp zone.
 - Fragile, easily cracked.
- Membrane failure could threaten entire output.
- Has been proposed for water vapor electrolysis

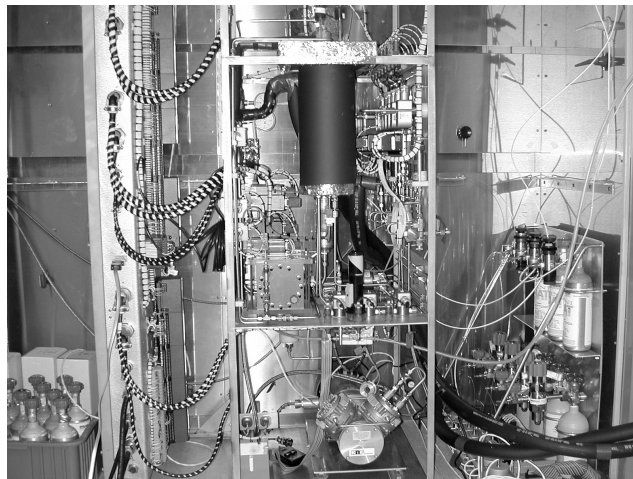
Possible Advantages for an Alternate System

- Lower temperatures
 - <700°C...use metals in construction
 - <270°C ...use polymers and elastomers
 - < 31°C ...liquid CO₂ as co-solvent
- Lower operating voltage...better efficiency
- More rugged construction, a robust assembly

Reverse Water Gas Shift (RWGS)

- $\text{CO}_2 + \text{H}_2 \leftrightarrow \text{CO} + \text{H}_2\text{O}$ (RWGS Reaction)
- Equilibrium constant is only 0.1, must remove products to drive reaction to completion.
- Reactor requires pump, permeation filter and heat exchangers to run.
- Electrolysis of water requires as much energy as zirconia.
- Rugged and low temperature, but complex and heavy.

RWGS Reactor Assembly

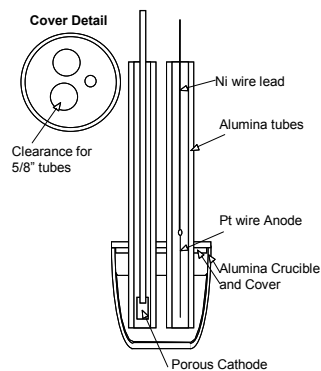


RWGS Test Bed

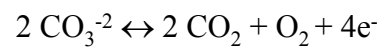


Molten Carbonate Electrolysis

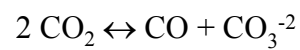
Molten Carbonate Test Cell Design



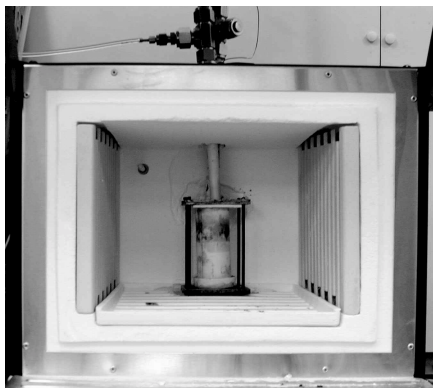
Anode Reaction



Cathode Reaction



Molten Carbonate Test Fixture



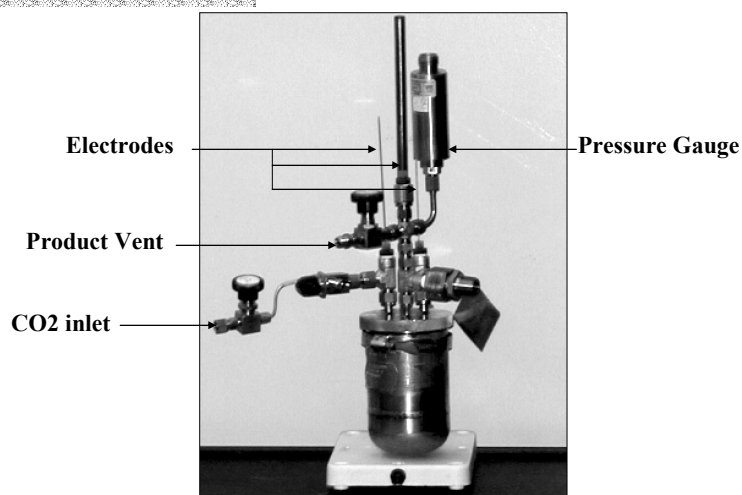
Molten Salt Results

- Li_2O in Chloride melt \rightarrow Pure oxygen at anode
 - Current decreased to zero over a few hours
 - Carbonate formation at cathode is likely
- Carbonate electrolysis at anode yields 2:1, CO_2/O_2
 - Sustained reaction for 7 days
 - Minimal loss of O_2 production
 - Temperature of operation: 550°C
 - Cell voltage: ~ 0.8 Volts
 - Platinum anode and cathode

Non-Aqueous Solvents

- Potential Advantages
 - Wide electrochemical window
 - Low temperature operation
 - CO₂ a potential co-solvent
- Solvents Surveyed & Results
 - Acetonitrile, DMSO, Propylene Carbonate
 - C-V curves show CO₂ reduction
 - No evidence for oxide or carbonate solubility
 - No oxygen generation at anode

Liquid CO₂: Electrochemical Reaction Vessel



Pro and Cons of Liquid CO₂

- Advantages:

- Very high electrode concentrations → High current density
- No porous gas cathode required → Simplified Cathode
- If carbon forms → Twice as much O₂ out/ CO₂ in

- Disadvantages:

- CO₂ at high pressure mixed with electrode products
- If carbon forms → must remove carbon periodically
- If CO forms, separation technology is critical for life support uses.
- No known cell compartment separators that would transport carbonate, and simplify product separation.

Ionic Liquids

- What are they?

- Low melting point ionic salts. By using large anions and cations, a low temperature melt with conductivity similar to molten salts can be obtained.
- Examples include pyridinium and imidazolium cations with anions such as PF₆⁻, BF₄⁻, and many others.

- Desirable Properties

- Low temperature (-100 - 300°C).
- High conductivity (low I*R losses).
- Wide electrochemical window.
- Non-volatile.
- Miscible with or high solubility for CO₂.

Hurdles for Ionic Liquids

- . Find one that carbonate is soluble in, or carbonate is the anion.

(Working with Prof. R. Rogers @Univ. of Alabama)

- Confirm CO₂ reduction, preferably to CO.
- Confirm O₂ production at anode (2:1, CO₂/O₂).
- Confirm long term stability and balanced cell reactions.
- Minimize cell voltage.
 - Electrode materials
 - Minimize I*R drop → thin electrolyte film, highly conductive.
- Construct porous support for electrolyte (similar to carbonate).
- Construct cell manifolds and multi-cell assemblies.

Mobile Oxide Ceramic Membranes

- Similar to Zirconia, but lower temperature.
- Demonstrated on NO_x electrolysis.
- Oxide ion from CO₂ reduction stabilized by Ceramic Lattice structure.
- Operating temperatures 500 - 700°C allows use of metal manifolds and seals.

Working with Prof. E. Wachsman at
Univ. of Florida to prove feasibility.

Oxygen Production Conclusions

- Oxide ions as an electrochemical intermediate are only viable in mobile oxide ceramics.
- Carbonate is formed from CO₂ reduction in molten salts, and produces a 2:1 CO₂/O₂ mixture at the anode.
- Other products of CO₂ reduction do not produce O₂ at the anode.
- Carbonate melts and mobile oxide ceramics are probably useable below 700°C for CO₂ electrolysis.
- Ionic liquids may be able to operate below 200°C if one compatible with carbonate can be found.

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 - Mike O'Neal Bill Larson Clyde Parrish
 - Bill Buttner Jan Surma Curtis Ihlefeld
- Approximately 50 workers have participated in ISRU related technologies at KSC, including biological research on plant growth chambers, Mars atmospheric test chamber, static charge experiments, ISPP and other technologies.

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Legend: Prevention - Fire Prevention and Material Flammability
Detection - Smoke and Fire Detection
Response - Fire and Post-Fire Response

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13. ABSTRACT (Maximum 200 words) The purpose of the workshop documented in this publication was to bring together personnel responsible for the design and operations of the International Space Station (ISS) and the fire protection research community to review the current knowledge in fire safety relative to spacecraft. From this review, research needs were identified that were then used to formulate a research plan with specific objectives. In this document, I have attempted to capture the very informative and lively discussions that occurred in the plenary sessions and the working groups. I hope that it will be useful to readers and serve as a significant step in assuring fire protection for the crews of current and future spacecraft.				
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